

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1800.
2.00	0.0	0.259E+00	2625.	1875.
3.00	0.0	0.718E-02	3675.	1950.
4.00	0.0	0.245E-03	4800.	2025.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1800.
2.00	0.0	0.442E+02	2550.	1875.
3.00	0.0	0.106E+02	3600.	1950.
4.00	0.0	0.312E+01	4650.	2025.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND		X-LOC (FT)	Z-LOC (FT)
		ON ENTIRE GRID (MG/L)	ON GRID (MG/L)		
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF copper FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF copper IS 0.667000E-02 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.2580000E-02 MG/L.

THE WATER QUALITY STANDARD FOR copper IS 0.3100000E-02 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 1 30.31	500.3	1575.	143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 2 30.61	500.2	1575.	159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 3 30.92	500.2	1575.	171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 4 31.23	500.2	1575.	181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 5 31.54	500.2	1575.	189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 6 31.84	500.2	1575.	195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 7 32.15	500.2	1575.	201.6	11.25	0.9467E-01	2.327	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 8 32.46	500.2	1575.	206.7	11.34	0.7957E-01	2.003	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 9 32.77	500.2	1575.	211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 10 33.07	500.2	1575.	215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(CU FT)	(CU FT)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3	1575.	2) = 1 143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2	1575.	2) = 2 159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2	1575.	2) = 3 171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2	1575.	2) = 4 181.1	10.80	0.1911	7.461	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2	1575.	2) = 5 189.1	10.99	0.1448	5.884	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2	1575.	2) = 6 195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2	1575.	2) = 7 201.6	11.25	0.9467E-01	4.083	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2	1575.	2) = 8 206.7	11.34	0.7957E-01	3.512	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2	1575.	2) = 9 211.1	11.42	0.6810E-01	3.066	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2	1575.	2) = 10 215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.31	500.3	1575.	143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 30.61	500.2	1575.	159.3	10.08	0.4471	6.960	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 30.92	500.2	1575.	171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 31.23	500.2	1575.	181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 31.54	500.2	1575.	189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 31.84	500.2	1575.	195.8	11.13	0.1152	2.190	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 32.15	500.2	1575.	201.6	11.25	0.9467E-01	1.849	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 32.46	500.2	1575.	206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 32.77	500.2	1575.	211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 33.07	500.2	1575.	215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 1 30.31	500.3	1575.	143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 2 30.61	500.2	1575.	159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 3 30.92	500.2	1575.	171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 4 31.23	500.2	1575.	181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 5 31.54	500.2	1575.	189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 6 31.84	500.2	1575.	195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 7 32.15	500.2	1575.	201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 8 32.46	500.2	1575.	206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 9 32.77	500.2	1575.	211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 10 33.07	500.2	1575.	215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	X-LOCATION 500.2	Z-LOCATION 1575.	5) = 1 215.1	10.07	3.431	8453.	3784.	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME... MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 144.63

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7091.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.868

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7178.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.601

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7212.4

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .00001)

Table with 31 columns (M N= 2 to 31) and 31 rows (2 to 59). The table shows numerical values for silt accumulation, with some cells containing '+' signs and others being zero. The values generally decrease as the column index increases, with the highest values in the first few columns.

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564. 1650.	3.674	0.0000E+00	466.9	0.0000E+00	13.50	0.100000E-01
2	1564. 1650.	0.9189	0.0000E+00	491.6	0.0000E+00	13.50	0.100000E-01
3	1564. 1650.	0.6027	0.0000E+00	509.9	0.0000E+00	13.50	0.100000E-01
4	1564. 1650.	0.4163	0.0000E+00	524.4	0.0000E+00	13.50	0.100000E-01
5	1564. 1650.	0.3492	0.0000E+00	536.2	0.0000E+00	13.50	0.100000E-01
6	1563. 1650.	0.2863	0.0000E+00	546.1	0.0000E+00	13.50	0.100000E-01
7	1563. 1650.	0.2448	0.0000E+00	554.5	0.0000E+00	13.50	0.100000E-01
8	1563. 1650.	0.2099	0.0000E+00	561.8	0.0000E+00	13.50	0.100000E-01
9	1563. 1650.	0.1815	0.0000E+00	568.2	0.0000E+00	13.50	0.100000E-01
10	1563. 1650.	16.72	0.0000E+00	573.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.6253
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9256
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6010
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.4

MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637. 1726.	0.2492	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2637. 1726.	0.6233E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2637. 1726.	0.4089E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2636. 1726.	0.2824E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2636. 1726.	0.2369E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2636. 1726.	0.1942E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2636. 1726.	0.1660E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2636. 1726.	0.1424E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2636. 1726.	0.1231E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2636. 1726.	1.134	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65294
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26630
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10861
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	0	0	0	0	0	0	0	0	0	0	00000
24	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	0	0	0	0	0	0	0	0	0	00000
26	+	+	+	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	0	0	0	0	0	0	0	0	00000
28	+	+	+	+	0	0	0	0	0	0	0	00000
29	+	+	+	+	0	0	0	0	0	0	0	00000
30	+	+	+	+	+	0	0	0	0	0	0	00000
31	+	+	+	+	+	0	0	0	0	0	0	00000
32	+	+	+	+	+	0	0	0	0	0	00000
33	+	+	+	+	+	+	0	0	0	0	00000
34	+	+	+	+	+	+	0	0	0	00000
35	+	+	+	+	+	+	0	0	00000
36	+	+	+	+	+	+	+	0	00000
37	+	+	+	+	+	+	+	0	00000
38	+	+	+	+	+	+	+	0	00000
39	+	+	+	+	+	+	+	0	00000
40	+	+	+	+	+	+	+	0	00000
41	+	+	+	+	+	+	+	0	00000
42	+	+	+	+	+	+	+	+	00000
43	+	+	+	+	+	+	+	+	00000
44	+	+	+	+	+	+	+	+	00000
45	+	+	+	+	+	+	+	+	00000
46	+	+	+	+	+	+	+	+	00000
47	+	+	+	+	+	+	+	+	00000
48	+	+	+	+	+	+	+	+00000
49	+	+	+	+	+	+	+	+00000
50	+	+	+	+	+	+	+	+00000
51	+	+	+	+	+	+	+	+	00000
52	+	+	+	+	+	+	+	+	00000
53	+	+	+	+	+	+	+	+	00000
54	+	+	+	+	+	+	+	+	00000
55	+	+	+	+	+	+	+	+	00000
56	+	+	+	+	+	+	+	+	00000
57	+	+	+	+	+	+	+	+	00000
58	+	+	+	00000
59	+	+	00000
60	+	0	0	00000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3710. 1801.	0.1691E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	3710. 1801.	0.4229E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	3709. 1801.	0.2774E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	3709. 1801.	0.1916E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	3709. 1801.	0.1607E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	3709. 1801.	0.1317E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	3709. 1801.	0.1126E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	3709. 1801.	0.9658E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	3709. 1801.	0.8352E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	3709. 1801.	0.7693E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44293E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18065E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73674E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.1147E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2869E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	4782.	1877.	0.1882E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	4782.	1877.	0.1300E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	4782.	1877.	0.1090E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	4782.	1877.	0.8937E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	4782.	1877.	0.7641E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	4782.	1877.	0.6552E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	4782.	1877.	0.5666E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	4782.	1877.	0.5219E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1419.2

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1858.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 611.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2665.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 484.33

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2793.5

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .00001)

Table with columns M N= 2 to 31 and rows 2 to 59. The table displays numerical values for each grid square, with many cells containing 0.0000. Non-zero values appear starting from row 8, column 15, and increase significantly through rows 12-29, representing the bottom accumulation of clay. The values are distributed across columns 15 to 29.

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1548. 1649.	134.9	0.0000E+00	466.9	0.0000E+00	13.50	0.200000E-02
2	1564. 1650.	4.086	0.0000E+00	491.6	0.0000E+00	13.50	0.200000E-02
3	1564. 1650.	2.691	0.0000E+00	509.9	0.0000E+00	13.50	0.200000E-02
4	1564. 1650.	1.960	0.0000E+00	524.4	0.0000E+00	13.50	0.200000E-02
5	1564. 1650.	1.544	0.0000E+00	536.2	0.0000E+00	13.50	0.200000E-02
6	1563. 1650.	1.266	0.0000E+00	546.1	0.0000E+00	13.50	0.200000E-02
7	1563. 1650.	1.070	0.0000E+00	554.5	0.0000E+00	13.50	0.200000E-02
8	1563. 1650.	0.9198	0.0000E+00	561.8	0.0000E+00	13.50	0.200000E-02
9	1563. 1650.	0.8021	0.0000E+00	568.2	0.0000E+00	13.50	0.200000E-02
10	1433. 1641.	335.1	0.0000E+00	573.9	0.1115	13.39	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 405.31
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2872.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 339.19
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2938.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 283.85
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2993.9

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2621.	1724.	79.04	0.0000E+00	915.3	0.0000E+00	13.50	0.200000E-02
2	2637.	1726.	2.395	0.0000E+00	946.7	0.0000E+00	13.50	0.200000E-02
3	2637.	1726.	1.577	0.0000E+00	969.8	0.0000E+00	13.50	0.200000E-02
4	2636.	1726.	1.149	0.0000E+00	987.9	0.0000E+00	13.50	0.200000E-02
5	2636.	1726.	0.9049	0.0000E+00	1003.	0.0000E+00	13.50	0.200000E-02
6	2636.	1726.	0.7418	0.0000E+00	1015.	0.0000E+00	13.50	0.200000E-02
7	2636.	1726.	0.6271	0.0000E+00	1026.	0.0000E+00	13.50	0.200000E-02
8	2636.	1726.	0.5391	0.0000E+00	1035.	0.0000E+00	13.50	0.200000E-02
9	2636.	1726.	0.4701	0.0000E+00	1043.	0.0000E+00	13.50	0.200000E-02
10	2505.	1716.	196.4	0.0000E+00	1050.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 237.55
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3040.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 198.79
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3079.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 166.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3111.4

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 10800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows (3 0000 to 59 0000). The table shows numerical values for clay accumulation, with some cells containing '+' signs indicating specific values or trends. The values generally increase from top to bottom and from left to right.

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	0	0	0	0	0	0	0	0	0	0	0
19	+	+	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	0	0	0	0	0	0	0	0	0	0
21	+	+	+	+	0	0	0	0	0	0	0	0	0
22	+	+	+	+	0	0	0	0	0	0	0	0
23	+	+	+	+	+	0	0	0	0	0	0
24	.01	+	+	+	+	+	0	0	0	0	0
25	.02	+	+	+	+	+	+	0	0	0	0
26	.02	.01	+	+	+	+	+	0	0	0	0
27	.03	.01	+	+	+	+	+	+	0	0	0
28	.04	.02	.01	+	+	+	+	+	+	0	0
29	.05	.02	.01	+	+	+	+	+	+0000
30	.07	.03	.01	+	+	+	+	+	+	+0000
31	.08	.04	.02	.01	+	+	+	+	+	+0000
32	.09	.05	.03	.01	+	+	+	+	+	+0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+0000
35	.13	.08	.05	.02	.01	+	+	+	+	+	+0000
36	.15	.09	.05	.03	.02	.01	+	+	+	+	+	+0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+0000
38	.17	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.17	.12	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.0000
40	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.0000
41	.18	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.0000
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
43	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
44	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
45	.17	.13	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	.	+0000
46	.17	.12	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	.	+0000
47	.16	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
48	.14	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
49	.13	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
50	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
51	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
52	.09	.07	.05	.04	.02	.02	.01	.	+	+	+	+	+	+	+	.	+0000
53	.08	.06	.04	.03	.02	.01	.01	.	+	+	+	+	+	+	+	.	+0000
54	.06	.05	.04	.03	.02	.01	.01	.	+	+	+	+	+	+	+	.	+0000
55	.05	.04	.03	.02	.01	.01	.	+	+	+	+	+	+	+	+	.	.0000
56	.04	.03	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	.	.0000
57	.03	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	.	.0000
58	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	.	.	.0000
59	.01	.01	.01	.	+	+	+	+	+	+	+	+	+	+	.	.	.0000
60	.01	.01	.	+	+	+	+	+	+	+	+	+	+0000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	3694.	1800.	46.32	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	3710.	1801.	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	3709.	1801.	0.9242	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	3709.	1801.	0.6733	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	3709.	1801.	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	3709.	1801.	0.4348	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	3709.	1801.	0.3675	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	3709.	1801.	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	3709.	1801.	0.2755	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	3578.	1792.	115.1	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 139.22
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3138.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 116.51
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3160.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 97.504
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3179.3

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	.09	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	00000
43	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	00000
44	.17	.15	.14	.12	.10	.09	.08	.06	.05	.04	.03	.02	.02	0	0	0	00000
45	.22	.20	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	.02	0	0	0	00000
46	.29	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	00000
47	.36	.33	.30	.26	.23	.20	.17	.14	.11	.09	.07	.06	.04	0	0	0	00000
48	.46	.42	.37	.33	.29	.25	.21	.17	.14	.11	.09	.07	.05	0	0	0	00000
49	.57	.51	.46	.41	.36	.31	.26	.22	.18	.14	.11	.09	.07	0	0	0	00000
50	.69	.63	.56	.50	.43	.37	.32	.26	.22	.17	.14	.11	.08	0	0	0	00000
51	.83	.76	.68	.60	.52	.45	.38	.32	.26	.21	.17	.13	.10	0	0	0	00000
52	.99	.90	.81	.71	.62	.53	.45	.38	.31	.25	.20	.16	.12	0	0	0	00000
53	1.1	1.0	.94	.83	.73	.62	.53	.44	.36	.29	.23	.18	.14	0	0	0	00000
54	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.21	.16	0	0	0	00000
55	1.5	1.3	1.2	1.0	.95	.82	.69	.58	.48	.39	.31	.24	.19	0	0	0	00000
56	1.7	1.5	1.3	1.2	1.0	.92	.78	.65	.53	.43	.34	.27	.21	0	0	0	00000
57	1.8	1.7	1.5	1.3	1.1	1.0	.86	.72	.59	.48	.38	.30	.23	0	0	0	00000
58	2.0	1.8	1.6	1.4	1.2	1.1	.94	.78	.64	.52	.42	.33	.25	0	0	0	00000
59	2.2	2.0	1.8	1.5	1.3	1.1	1.0	.84	.69	.56	.45	.35	.27	0	0	0	00000
60	2.3	2.1	1.9	1.6	1.4	1.2	1.0	.89	.73	.59	.47	.37	.29	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	0	0	0	0	0	0	0	0	0	0	0
19	+	+	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	0	0	0	0	0	0	0	0	0	0
21	+	+	+	+	0	0	0	0	0	0	0	0	0
22	+	+	+	+	0	0	0	0	0	0	0	0
23	+	+	+	+	+	0	0	0	0	0	0
24	.01	+	+	+	+	+	0	0	0	0	0
25	.02	+	+	+	+	+	+	0	0	0	0
26	.02	.01	+	+	+	+	+	0
27	.03	.01	+	+	+	+	+	+0000
28	.04	.02	.01	+	+	+	+	+	+0000
29	.05	.02	.01	+	+	+	+	+	+	+0000
30	.07	.03	.01	+	+	+	+	+	+	+0000
31	.08	.04	.02	.01	+	+	+	+	+	+0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	.	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	.	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	.	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	.	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	.	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	.	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	.	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	.	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	.	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	.	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	.	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	.	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	.	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	.	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	.	+0000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM		MASS FROM DISPOSAL	ENTRAINED MASS	CLOUD X-Z DIAMETER	DEPTH OF TOP OF CLOUD	CLOUD VERT. THICKNESS	SOLIDS FALL VELOCITY
	TOP OF GRID	LEFT OF GRID	(CU FT)	(CU FT)	(FT)	(FT)	(FT)	(FPS)
1	4767.	1876.	27.15	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.8226	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	4782.	1877.	0.5417	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	4782.	1877.	0.3946	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	4782.	1877.	0.3108	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	4782.	1877.	0.2548	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	4782.	1877.	0.2154	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	4782.	1877.	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	4782.	1877.	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	4651.	1868.	67.47	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	0	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	0	00000
25	.02	+	+	+	+	+	+	0	0	0	00000
26	.02	.01	+	+	+	+	+	00000
27	.03	.01	+	+	+	+	+	+00000
28	.04	.02	.01	+	+	+	+	+	+00000
29	.05	.02	.01	+	+	+	+	+	+	+00000
30	.07	.03	.01	+	+	+	+	+	+	+00000
31	.08	.04	.02	.01	+	+	+	+	+	+00000
32	.09	.05	.03	.01	+	+	+	+	+	+	+00000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+00000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+00000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.00000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.00000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.00000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+00000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+00000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+00000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+00000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+00000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+00000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+00000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+00000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF copper

SUMMARY OF copper DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.7

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	847.9	1600.	0.1048E+06	0.1001E+06	318.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.7

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1206.	1625.	0.1871E+06	0.1825E+06	439.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.7

CONCENTRATIONS ABOVE BACKGROUND OF copper (MG/L) IN THE CLOUD 3600.00 SECONDS AFTER DUMP

0.00 FT BELOW THE WATER SURFACE

...MULTIPLY DISPLAYED VALUES BY 0.1000E-04 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows (2 to 57). Row 2 contains a long string of zeros. Rows 3-14 contain zeros. Row 15 starts with a period and plus signs. Row 16 starts with a period and plus signs and decimal values. Rows 17-57 contain various numerical values representing concentrations.

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1563.	1650.	0.3217E+06	0.3170E+06	573.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.7

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1921.	1675.	0.5097E+06	0.5050E+06	721.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.8

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2278.	1700.	0.7605E+06	0.7559E+06	880.0	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4668.8

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2636.	1726.	0.1084E+07	0.1079E+07	1050.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.5

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2994.	1751.	0.1488E+07	0.1484E+07	1230.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.5

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3351.	1776.	0.1984E+07	0.1980E+07	1420.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.5

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.2581E+07	0.2576E+07	1619.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.2

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4066.	1826.	0.3287E+07	0.3283E+07	1827.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.2

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4424.	1852.	0.4114E+07	0.4109E+07	2043.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4662.0

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.08	.07	.06	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	00000
45	.10	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	.01	0	0	0	00000
46	.14	.13	.11	.10	.09	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	00000
47	.18	.16	.15	.13	.11	.10	.08	.07	.06	.05	.04	.03	.02	0	0	0	00000
48	.23	.21	.19	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	00000
49	.29	.26	.24	.21	.18	.16	.13	.11	.09	.07	.06	.05	.04	0	0	0	00000
50	.35	.32	.29	.26	.23	.20	.17	.14	.11	.09	.07	.06	.04	0	0	0	00000
51	.43	.39	.36	.32	.28	.24	.20	.17	.14	.11	.09	.07	.06	0	0	0	00000
52	.52	.47	.43	.38	.33	.29	.24	.21	.17	.14	.11	.09	.07	0	0	0	00000
53	.62	.56	.51	.45	.40	.34	.29	.24	.20	.16	.13	.10	.08	0	0	0	00000
54	.72	.66	.59	.53	.46	.40	.34	.29	.24	.19	.16	.12	.10	0	0	0	00000
55	.83	.76	.68	.61	.53	.46	.39	.33	.27	.22	.18	.14	.11	0	0	0	00000
56	.94	.86	.78	.69	.61	.52	.45	.38	.31	.25	.20	.16	.13	0	0	0	00000
57	1.0	.96	.87	.77	.68	.59	.50	.42	.35	.29	.23	.18	.14	0	0	0	00000
58	1.1	1.0	.96	.86	.75	.65	.55	.47	.39	.32	.25	.20	.16	0	0	0	00000
59	1.2	1.1	1.0	.93	.82	.71	.60	.51	.42	.34	.28	.22	.17	0	0	0	00000
60	1.3	1.2	1.1	1.0	.88	.76	.65	.55	.45	.37	.30	.24	.19	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.30	.28	.25	.22	.19	.17	.14	.12	.10	.08	.06	.05	.04	0	0	0	00000
45	.40	.37	.33	.29	.26	.22	.19	.16	.13	.11	.08	.07	.05	0	0	0	00000
46	.52	.48	.43	.38	.34	.29	.25	.21	.17	.14	.11	.09	.07	0	0	0	00000
47	.67	.62	.56	.49	.43	.37	.32	.27	.22	.18	.15	.11	.09	0	0	0	00000
48	.86	.78	.71	.63	.55	.48	.41	.34	.28	.23	.19	.15	.11	0	0	0	00000
49	1.0	.98	.88	.79	.69	.60	.51	.43	.35	.29	.23	.18	.14	0	0	0	00000
50	1.3	1.2	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	0	0	0	00000
51	1.6	1.4	1.3	1.1	1.0	.90	.77	.64	.53	.44	.35	.28	.22	0	0	0	00000
52	1.9	1.7	1.5	1.4	1.2	1.0	.92	.77	.64	.53	.42	.34	.26	0	0	0	00000
53	2.2	2.0	1.8	1.6	1.4	1.2	1.0	.92	.76	.62	.50	.40	.31	0	0	0	00000
54	2.6	2.4	2.2	1.9	1.7	1.4	1.2	1.0	.89	.73	.59	.47	.37	0	0	0	00000
55	3.0	2.8	2.5	2.2	1.9	1.7	1.4	1.2	1.0	.84	.68	.54	.42	0	0	0	00000
56	3.4	3.1	2.8	2.5	2.2	1.9	1.6	1.4	1.1	.95	.77	.61	.48	0	0	0	00000
57	3.9	3.5	3.2	2.8	2.5	2.1	1.8	1.5	1.3	1.0	.86	.69	.54	0	0	0	00000
58	4.3	3.9	3.5	3.1	2.7	2.4	2.0	1.7	1.4	1.1	.95	.76	.60	0	0	0	00000
59	4.7	4.3	3.8	3.4	3.0	2.6	2.2	1.8	1.5	1.2	1.0	.83	.65	0	0	0	00000
60	5.0	4.6	4.1	3.7	3.2	2.8	2.4	2.0	1.6	1.3	1.1	.89	.70	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	.02	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
34	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
35	.04	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
36	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
37	.04	.03	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
38	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	00000
39	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	00000
40	.06	.04	.02	.01	.01	+	+	+	+	0	0	0	0	0	0	0	00000
41	.06	.04	.02	.02	.01	+	+	+	+	+	0	0	0	0	0	0	00000
42	.06	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0	0	00000
43	.06	.05	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	00000
44	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
45	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0	0	0	00000
46	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0	0	0	00000
47	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	00000
48	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	00000
49	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0	0	0	00000
50	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0	0	0	00000
51	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0	0	0	00000
52	.07	.06	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	0	0	0	00000
53	.07	.05	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	00000
54	.07	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	00000
55	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	00000
56	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	00000
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	00000
58	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	+	+	+	0	0	0	00000
59	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	+	0	0	0	00000
60	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	+	0	0	0	00000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.5070E+07	0.5065E+07	2268.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

M N= 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48
2 00
3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
14 . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
15 . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
16 . . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
17 . . . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
18 . . . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
19 + . . . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
20 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
21 + + . . . 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
22 + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
23 + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
24 + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
25 + + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
26 + + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
27 + + + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
28 + + + + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
29 + + + + + + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
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32 .01 + + + + + + + +0000
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36 .01 .01 + + + + + + + +0000
37 .01 .01 + + + + + + + +0000
38 .01 .01 + + + + + + + +0000
39 .01 .01 + + + + + + + +0000
40 .01 .01 + + + + + + + +0000
41 .02 .01 .01 + + + + + + + +0000
42 .02 .01 .01 + + + + + + + +0000
43 .02 .01 .01 + + + + + + + +0000
44 .02 .01 .01 + + + + + + + +0000
45 .02 .01 .01 + + + + + + + +0000
46 .02 .01 .01 + + + + + + + +0000
47 .02 .01 .01 + + + + + + + +0000
48 .02 .01 .01 + + + + + + + +0000
49 .02 .01 .01 .01 + + + + + + + +0000
50 .02 .01 .01 .01 + + + + + + + +0000
51 .02 .01 .01 .01 + + + + + + + +0000
52 .01 .01 .01 .01 + + + + + + + +0000
53 .01 .01 .01 .01 + + + + + + + +0000
54 .01 .01 .01 .01 + + + + + + + +0000
55 .01 .01 .01 .01 + + + + + + + +0000
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57 .01 .01 .01 + + + + + + + +0000
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59 .01 .01 .01 + + + + + + + +0000
60 .01 .01 .01 + + + + + + + +0000

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.263E+00	2625.	1725.
3.00	0.0	0.735E-02	3675.	1800.
4.00	0.0	0.252E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.255E+03	1500.	1650.
2.00	0.0	0.467E+02	2550.	1725.
3.00	0.0	0.114E+02	3600.	1800.
4.00	0.0	0.336E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR copper

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE		X-LOC (FT)	Z-LOC (FT)
		BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)		
0.33	0.0	0.971E-04	0.268E-02	825.	1575.
0.67	0.0	0.535E-04	0.263E-02	1200.	1650.
1.00	0.0	0.319E-04	0.261E-02	1575.	1650.
1.33	0.0	0.199E-04	0.260E-02	1950.	1650.
1.67	0.0	0.135E-04	0.259E-02	2250.	1725.
2.00	0.0	0.957E-05	0.259E-02	2625.	1725.
2.33	0.0	0.695E-05	0.259E-02	3000.	1725.
2.67	0.0	0.521E-05	0.259E-02	3375.	1800.
3.00	0.0	0.401E-05	0.258E-02	3675.	1800.
3.33	0.0	0.315E-05	0.258E-02	4050.	1800.
3.67	0.0	0.252E-05	0.258E-02	4425.	1875.
4.00	0.0	0.205E-05	0.258E-02	4800.	1875.
0.33	6.8	0.359E-03	0.294E-02	825.	1575.
0.67	6.8	0.198E-03	0.278E-02	1200.	1650.
1.00	6.8	0.118E-03	0.270E-02	1575.	1650.
1.33	6.8	0.737E-04	0.265E-02	1950.	1650.
1.67	6.8	0.498E-04	0.263E-02	2250.	1725.
2.00	6.8	0.354E-04	0.262E-02	2625.	1725.
2.33	6.8	0.257E-04	0.261E-02	3000.	1725.
2.67	6.8	0.193E-04	0.260E-02	3375.	1800.
3.00	6.8	0.148E-04	0.259E-02	3675.	1800.
3.33	6.8	0.116E-04	0.259E-02	4050.	1800.
3.67	6.8	0.932E-05	0.259E-02	4425.	1875.
4.00	6.8	0.757E-05	0.259E-02	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

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UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME                 SNAPSHOT                 ACCUMULATED                 3
3      ( SEC )             AREA(SQ FT)         L(FT)          W(FT)         AREA(SQ FT)         L(FT)          W(FT)         3
3
3      1200.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      2400.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      3600.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      4800.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      6000.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      7200.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      8400.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3      9600.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3     10800.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3     12000.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3     13200.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3     14400.0             0.000000E+00       0.            0.            0.000000E+00       0.            0.            3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
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*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF copper FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF copper IS 0.115000E-02 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.2580000E-02 MG/L.

THE WATER QUALITY STANDARD FOR copper IS 0.3100000E-02 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	1) = 197.4	10.91	0.2177	34.30	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	1) = 224.8	11.43	0.1157	20.28	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	1) = 232.3	11.55	0.9997E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	2) = 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	2) = 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	2) = 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	2) = 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	2) = 185.6	10.61	0.2974	8.984	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	2) = 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	2) = 207.6	11.12	0.1689	5.614	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	2) = 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	2) = 224.8	11.43	0.1157	4.102	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	2) = 232.3	11.55	0.9997E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	2) = 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.56	500.1	1575.	113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 31.13	499.8	1575.	134.8	8.477	1.036	9.913	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 31.69	499.6	1575.	154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 32.25	499.5	1575.	171.6	10.18	0.4327	5.259	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 32.82	499.5	1575.	185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 33.38	499.5	1575.	197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 33.94	499.5	1575.	207.6	11.12	0.1689	2.428	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 34.51	499.5	1575.	216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 35.07	499.5	1575.	224.8	11.43	0.1157	1.773	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 35.63	499.5	1575.	232.3	11.55	0.9997E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 11 35.72	499.5	1575.	233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	4) = 1 233.4	9.779	3.721	6427.	5928.	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 167.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5902.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.559
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6002.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.553
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6042.0

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	2.333	0.0000E+00	419.0	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	1.539	0.0000E+00	453.4	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	1.101	0.0000E+00	484.4	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.7476	0.0000E+00	510.1	0.0000E+00	13.50	0.100000E-01
5	1563.	1650.	0.5443	0.0000E+00	531.0	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.4158	0.0000E+00	548.3	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.3351	0.0000E+00	563.0	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.2858	0.0000E+00	576.0	0.0000E+00	13.50	0.100000E-01
9	1562.	1650.	0.2452	0.0000E+00	587.6	0.0000E+00	13.50	0.100000E-01
10	1562.	1650.	0.2115	0.0000E+00	598.2	0.0000E+00	13.50	0.100000E-01
11	1562.	1650.	19.79	0.0000E+00	599.8	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.237
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6058.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.5829
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6065.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.8691
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.7

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 7200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns labeled M N= 2 through 31 and rows 2 through 59. The table contains numerical data representing silt accumulation, with some cells containing '+' signs and others containing decimal values. The values generally increase from row 2 to row 59.

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	2637.	1726.	0.1583	0.0000E+00	853.9	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.1044	0.0000E+00	898.1	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.7469E-01	0.0000E+00	937.5	0.0000E+00	13.50	0.100000E-01
4	2636.	1726.	0.5071E-01	0.0000E+00	970.0	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.3693E-01	0.0000E+00	996.2	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.2821E-01	0.0000E+00	1018.	0.0000E+00	13.50	0.100000E-01
7	2635.	1725.	0.2273E-01	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01
8	2635.	1725.	0.1939E-01	0.0000E+00	1052.	0.0000E+00	13.50	0.100000E-01
9	2635.	1725.	0.1663E-01	0.0000E+00	1067.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1435E-01	0.0000E+00	1080.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.343	0.0000E+00	1082.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76229
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31089
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12679
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
 MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.1074E-01	0.0000E+00	1389.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.7081E-02	0.0000E+00	1441.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.5067E-02	0.0000E+00	1487.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3440E-02	0.0000E+00	1526.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2505E-02	0.0000E+00	1556.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1913E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1542E-02	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01
8	3708.	1801.	0.1315E-02	0.0000E+00	1622.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1128E-02	0.0000E+00	1638.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.9735E-03	0.0000E+00	1654.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.9109E-01	0.0000E+00	1656.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.51711E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21090E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.86012E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.6

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.7283E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.4803E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3437E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2334E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1699E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1298E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1046E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.8922E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7655E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6604E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.6179E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1232.1

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1392.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 435.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2189.1

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	112.6	0.0000E+00	419.0	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	5.895	0.0000E+00	453.4	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	4.298	0.0000E+00	484.4	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	3.093	0.0000E+00	510.1	0.0000E+00	13.50	0.200000E-02
5	1563.	1650.	2.260	0.0000E+00	531.0	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	1.742	0.0000E+00	548.3	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	1.388	0.0000E+00	563.0	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	1.183	0.0000E+00	576.0	0.0000E+00	13.50	0.200000E-02
9	1562.	1650.	1.025	0.0000E+00	587.6	0.0000E+00	13.50	0.200000E-02
10	1562.	1650.	0.9074	0.0000E+00	598.2	0.0000E+00	13.50	0.200000E-02
11	1438.	1641.	300.8	0.0000E+00	599.8	0.3251E-01	13.47	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 364.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2260.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2319.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 255.11
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2369.3

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 7200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns M N= 2 through 31. Rows 2 through 59 contain numerical values representing clay accumulation, with some cells being zero and others containing decimal values. The values generally increase from row 2 to row 59, with some fluctuations.

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	66.02	0.0000E+00	853.9	0.0000E+00	13.50	0.200000E-02
2	2636.	1726.	3.455	0.0000E+00	898.1	0.0000E+00	13.50	0.200000E-02
3	2636.	1726.	2.519	0.0000E+00	937.5	0.0000E+00	13.50	0.200000E-02
4	2636.	1726.	1.813	0.0000E+00	970.0	0.0000E+00	13.50	0.200000E-02
5	2635.	1726.	1.324	0.0000E+00	996.2	0.0000E+00	13.50	0.200000E-02
6	2635.	1726.	1.021	0.0000E+00	1018.	0.0000E+00	13.50	0.200000E-02
7	2635.	1725.	0.8135	0.0000E+00	1036.	0.0000E+00	13.50	0.200000E-02
8	2635.	1725.	0.6936	0.0000E+00	1052.	0.0000E+00	13.50	0.200000E-02
9	2635.	1725.	0.6010	0.0000E+00	1067.	0.0000E+00	13.50	0.200000E-02
10	2634.	1725.	0.5318	0.0000E+00	1080.	0.0000E+00	13.50	0.200000E-02
11	2511.	1717.	176.3	0.0000E+00	1082.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2410.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.67
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2445.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2474.9

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	+	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	0	0	0	0	0	0	0	00000
22	+	+	+	+	+	0	0	0	0	0	0	00000
23	.01	+	+	+	+	+	0	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	0	00000
25	.02	+	+	+	+	+	+	0	0	0	00000
26	.02	.01	+	+	+	+	+	+	0	00000
27	.03	.01	+	+	+	+	+	+	00000
28	.04	.02	.01	+	+	+	+	+	+0000
29	.05	.03	.01	+	+	+	+	+	+	+0000
30	.06	.03	.01	.01	+	+	+	+	+	+0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+0000
32	.09	.05	.02	.01	+	+	+	+	+	+	+0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
40	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.16	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.16	.12	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.03	.02	.01	.	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
54	.06	.04	.03	.02	.02	.01	.	+	+	+	+	+	+	+	+	+	+0000
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
56	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.0000
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	38.69	0.0000E+00	1389.	0.0000E+00	13.50	0.200000E-02
2	3709.	1801.	2.025	0.0000E+00	1441.	0.0000E+00	13.50	0.200000E-02
3	3709.	1801.	1.476	0.0000E+00	1487.	0.0000E+00	13.50	0.200000E-02
4	3708.	1801.	1.062	0.0000E+00	1526.	0.0000E+00	13.50	0.200000E-02
5	3708.	1801.	0.7763	0.0000E+00	1556.	0.0000E+00	13.50	0.200000E-02
6	3708.	1801.	0.5983	0.0000E+00	1582.	0.0000E+00	13.50	0.200000E-02
7	3708.	1801.	0.4768	0.0000E+00	1603.	0.0000E+00	13.50	0.200000E-02
8	3708.	1801.	0.4065	0.0000E+00	1622.	0.0000E+00	13.50	0.200000E-02
9	3707.	1801.	0.3522	0.0000E+00	1638.	0.0000E+00	13.50	0.200000E-02
10	3707.	1801.	0.3117	0.0000E+00	1654.	0.0000E+00	13.50	0.200000E-02
11	3583.	1792.	103.3	0.0000E+00	1656.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 125.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2499.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.71
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2519.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.632
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2535.8

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	00000
43	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	00000
44	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	00000
45	.20	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	00000
46	.25	.23	.21	.18	.16	.14	.12	.10	.08	.06	.05	.04	.03	0	0	0	00000
47	.32	.29	.26	.23	.20	.18	.15	.12	.10	.08	.07	.05	.04	0	0	0	00000
48	.40	.37	.33	.29	.26	.22	.19	.16	.13	.10	.08	.07	.05	0	0	0	00000
49	.50	.45	.41	.36	.32	.27	.23	.19	.16	.13	.10	.08	.06	0	0	0	00000
50	.61	.55	.50	.44	.38	.33	.28	.23	.19	.16	.13	.10	.08	0	0	0	00000
51	.73	.66	.60	.53	.46	.40	.34	.28	.23	.19	.15	.12	.09	0	0	0	00000
52	.86	.79	.71	.63	.55	.47	.40	.33	.28	.22	.18	.14	.11	0	0	0	00000
53	1.0	.92	.83	.73	.64	.55	.47	.39	.32	.26	.21	.17	.13	0	0	0	00000
54	1.1	1.0	.96	.85	.74	.63	.54	.45	.37	.30	.24	.19	.15	0	0	0	00000
55	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.22	.17	0	0	0	00000
56	1.5	1.3	1.2	1.0	.94	.81	.69	.57	.47	.38	.31	.24	.19	0	0	0	00000
57	1.6	1.5	1.3	1.2	1.0	.90	.76	.64	.52	.43	.34	.27	.21	0	0	0	00000
58	1.8	1.6	1.4	1.3	1.1	.98	.83	.69	.57	.46	.37	.29	.23	0	0	0	00000
59	1.9	1.7	1.6	1.4	1.2	1.0	.89	.75	.61	.50	.40	.31	.24	0	0	0	00000
60	2.0	1.8	1.7	1.5	1.3	1.1	.95	.79	.65	.53	.42	.33	.26	0	0	0	00000

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows (3 0000 to 59 0000). The table contains numerical values representing clay accumulation, with some cells containing '+' signs to indicate specific values or trends. The values generally increase from left to right and bottom to top.

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	+	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	0	0	0	0	0	0	0	00000
22	+	+	+	+	+	0	0	0	0	0	00000
23	.01	+	+	+	+	+	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	00000
25	.02	+	+	+	+	+	+	0	0	00000
26	.02	.01	+	+	+	+	+	+	+	00000
27	.03	.01	+	+	+	+	+	+	+00000
28	.04	.02	.01	+	+	+	+	+	+	+00000
29	.05	.03	.01	+	+	+	+	+	+	+00000
30	.06	.03	.01	.01	+	+	+	+	+	+	+00000
31	.08	.04	.02	.01	+	+	+	+	+	+	+00000
32	.09	.05	.03	.01	+	+	+	+	+	+	+00000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+00000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.00000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.	.00000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.00000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+00000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+00000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+00000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+00000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+00000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+00000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+00000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+00000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+00000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	22.68	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8653	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6227	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2795	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2382	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2064	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	4656.	1868.	60.57	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	+	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	0	0	0	0	0	0	0	00000
22	+	+	+	+	+	0	0	0	0	0	00000
23	.01	+	+	+	+	+	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	00000
25	.02	+	+	+	+	+	+	0	0	00000
26	.02	.01	+	+	+	+	+	+	00000
27	.03	.01	+	+	+	+	+	+00000
28	.04	.02	.01	+	+	+	+	+	+00000
29	.05	.03	.01	+	+	+	+	+	+	+00000
30	.06	.03	.01	.01	+	+	+	+	+	+00000
31	.08	.04	.02	.01	+	+	+	+	+	+00000
32	.09	.05	.03	.01	+	+	+	+	+	+00000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+00000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.00000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.	.00000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.00000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+00000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+00000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+00000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+00000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+00000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+00000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+00000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+00000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+00000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+00000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+00000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+00000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+00000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+00000

BEGIN LONG TERM SIMULATION OF FATE OF copper

SUMMARY OF copper DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 498.17

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.4	1599.	0.1142E+06	0.1137E+06	339.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.39

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	0.2028E+06	0.2023E+06	462.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.38

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1562.	1650.	0.3464E+06	0.3459E+06	599.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.38

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	0.5452E+06	0.5447E+06	749.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.38

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	0.8085E+06	0.8080E+06	910.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.38

CONCENTRATIONS ABOVE BACKGROUND OF copper (MG/L) IN THE CLOUD 7200.00 SECONDS AFTER DUMP

0.00 FT BELOW THE WATER SURFACE

Table with 31 columns (M N= 2 to 31) and 31 rows. Header: ...MULTIPLY DISPLAYED VALUES BY 0.1000E-06 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001). Data values range from 0 to 0.20.

CONCENTRATIONS ABOVE BACKGROUND OF copper (MG/L) IN THE CLOUD 7200.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

Table with columns for M N= (2-31) and rows for concentration values. Legend: 0.1000E-05 (MULTIPLY DISPLAYED VALUES BY), (LEGEND... + = .LT. .01, . = .LT. .0001, 0 = .LT. .000001). Values are 0 for most rows, increasing to 0.07 for row 56.

M N= 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48
2 000
3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
12 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
17 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
24 + + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
25 .01 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
26 .02 .01 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
27 .04 .02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
28 .07 .04 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
29 .11 .06 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
30 .16 .09 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
31 .23 .13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
32 .30 .18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
33 .38 .22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
34 .44 .26 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
35 .49 .29 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
36 .51 .30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
37 .50 .30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
38 .46 .27 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
39 .40 .24 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
40 .32 .19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
41 .25 .15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
42 .18 .10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
43 .12 .07 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
44 .07 .04 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
45 .04 .02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
46 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
47 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
48 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
49 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
51 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
52 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
53 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
54 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
55 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
56 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
57 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
58 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
59 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000
60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 00000

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	0.1146E+07	0.1145E+07	1082.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.38

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2992.	1751.	0.1566E+07	0.1566E+07	1264.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.50

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3350.	1776.	0.2080E+07	0.2079E+07	1455.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.50

CONCENTRATIONS ABOVE BACKGROUND OF copper (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-05 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 56 rows (2 to 56). Values range from 0 to 0.96, showing an increasing trend across both rows and columns.

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3707.	1801.	0.2696E+07	0.2695E+07	1656.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.50

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4065.	1826.	0.3424E+07	0.3423E+07	1865.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.50

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4422.	1851.	0.4273E+07	0.4272E+07	2083.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 497.50

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.09	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	00000
45	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	00000
46	.16	.14	.13	.12	.10	.09	.07	.06	.05	.04	.03	.03	.02	0	0	0	00000
47	.20	.19	.17	.15	.13	.11	.10	.08	.07	.05	.04	.03	.03	0	0	0	00000
48	.26	.23	.21	.19	.17	.14	.12	.10	.09	.07	.06	.04	.03	0	0	0	00000
49	.32	.29	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	00000
50	.39	.36	.32	.29	.25	.22	.19	.16	.13	.11	.09	.07	.05	0	0	0	00000
51	.47	.43	.39	.35	.31	.27	.23	.19	.16	.13	.11	.08	.07	0	0	0	00000
52	.56	.52	.47	.42	.37	.32	.27	.23	.19	.16	.13	.10	.08	0	0	0	00000
53	.66	.61	.55	.49	.43	.38	.32	.27	.23	.19	.15	.12	.09	0	0	0	00000
54	.77	.71	.64	.57	.50	.44	.37	.32	.26	.22	.18	.14	.11	0	0	0	00000
55	.88	.81	.73	.65	.58	.50	.43	.36	.30	.25	.20	.16	.13	0	0	0	00000
56	1.0	.92	.83	.74	.65	.57	.49	.41	.34	.28	.23	.18	.14	0	0	0	00000
57	1.1	1.0	.93	.83	.73	.63	.54	.46	.38	.32	.26	.21	.16	0	0	0	00000
58	1.2	1.1	1.0	.91	.80	.70	.60	.51	.42	.35	.28	.23	.18	0	0	0	00000
59	1.3	1.2	1.1	.99	.87	.76	.65	.55	.46	.38	.31	.25	.19	0	0	0	00000
60	1.4	1.3	1.1	1.0	.93	.81	.70	.59	.49	.41	.33	.26	.21	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.35	.32	.29	.26	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	00000
45	.46	.42	.38	.34	.30	.26	.22	.19	.16	.13	.10	.08	.06	0	0	0	00000
46	.60	.55	.49	.44	.39	.34	.29	.24	.20	.17	.14	.11	.08	0	0	0	00000
47	.76	.70	.63	.56	.50	.43	.37	.31	.26	.21	.17	.14	.11	0	0	0	00000
48	.96	.88	.79	.71	.62	.54	.47	.39	.33	.27	.22	.18	.14	0	0	0	00000
49	1.1	1.0	.99	.88	.78	.67	.58	.49	.41	.34	.27	.22	.17	0	0	0	00000
50	1.4	1.3	1.2	1.0	.95	.83	.71	.60	.50	.41	.34	.27	.21	0	0	0	00000
51	1.7	1.6	1.4	1.3	1.1	1.0	.86	.73	.61	.50	.41	.33	.26	0	0	0	00000
52	2.0	1.9	1.7	1.5	1.3	1.1	1.0	.87	.72	.60	.49	.39	.31	0	0	0	00000
53	2.4	2.2	2.0	1.8	1.6	1.4	1.2	1.0	.85	.70	.57	.46	.36	0	0	0	00000
54	2.8	2.6	2.3	2.1	1.8	1.6	1.4	1.1	.99	.82	.66	.53	.42	0	0	0	00000
55	3.2	3.0	2.7	2.4	2.1	1.8	1.6	1.3	1.1	.94	.76	.61	.48	0	0	0	00000
56	3.7	3.4	3.0	2.7	2.4	2.1	1.8	1.5	1.2	1.0	.86	.69	.55	0	0	0	00000
57	4.1	3.7	3.4	3.0	2.7	2.3	2.0	1.7	1.4	1.1	.96	.77	.61	0	0	0	00000
58	4.5	4.1	3.7	3.3	2.9	2.5	2.2	1.8	1.5	1.3	1.0	.85	.67	0	0	0	00000
59	4.9	4.5	4.1	3.6	3.2	2.8	2.4	2.0	1.7	1.4	1.1	.92	.73	0	0	0	00000
60	5.2	4.8	4.4	3.9	3.4	3.0	2.5	2.1	1.8	1.5	1.2	.99	.78	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.02	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.03	.02	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
35	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.05	.03	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.05	.03	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.05	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.06	.04	.03	.01	.01	+	+	+	0	0	0	0	0	0	0	0	0
40	.06	.04	.03	.01	.01	+	+	+	0	0	0	0	0	0	0	0	0
41	.07	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0	0	0
42	.06	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0	0	0
43	.07	.05	.04	.02	.02	.01	+	+	+	+	0	0	0	0	0	0	0
44	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
45	.07	.06	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
46	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
47	.07	.05	.04	.03	.02	.02	.01	+	+	+	+	+	0	0	0	0	0
48	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	0	0
49	.07	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0	0
50	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	0	0	0	0	0
51	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	0	0	0	0	0
52	.07	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0	0
53	.07	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0	0
54	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	0	0	0	0	0
55	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	0	0	0	0	0
56	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	0	0	0	0	0
57	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0
58	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0
59	.06	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0
60	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4780.	1877.	0.5253E+07	0.5253E+07	2310.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.152E+02	1575.	1650.
2.00	0.0	0.299E+00	2625.	1725.
3.00	0.0	0.840E-02	3675.	1800.
4.00	0.0	0.289E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.419E+02	2550.	1725.
3.00	0.0	0.102E+02	3675.	1800.
4.00	0.0	0.302E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR copper

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE		X-LOC (FT)	Z-LOC (FT)
		BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)		
0.33	0.0	0.923E-05	0.259E-02	825.	1575.
0.67	0.0	0.515E-05	0.259E-02	1200.	1650.
1.00	0.0	0.311E-05	0.258E-02	1575.	1650.
1.33	0.0	0.197E-05	0.258E-02	1950.	1650.
1.67	0.0	0.134E-05	0.258E-02	2250.	1725.
2.00	0.0	0.960E-06	0.258E-02	2625.	1725.
2.33	0.0	0.702E-06	0.258E-02	3000.	1725.
2.67	0.0	0.529E-06	0.258E-02	3375.	1800.
3.00	0.0	0.409E-06	0.258E-02	3675.	1800.
3.33	0.0	0.323E-06	0.258E-02	4050.	1800.
3.67	0.0	0.259E-06	0.258E-02	4425.	1875.
4.00	0.0	0.211E-06	0.258E-02	4800.	1875.
0.33	6.8	0.341E-04	0.261E-02	825.	1575.
0.67	6.8	0.190E-04	0.260E-02	1200.	1650.
1.00	6.8	0.115E-04	0.259E-02	1575.	1650.
1.33	6.8	0.727E-05	0.259E-02	1950.	1650.
1.67	6.8	0.496E-05	0.258E-02	2250.	1725.
2.00	6.8	0.355E-05	0.258E-02	2625.	1725.
2.33	6.8	0.259E-05	0.258E-02	3000.	1725.
2.67	6.8	0.196E-05	0.258E-02	3375.	1800.
3.00	6.8	0.151E-05	0.258E-02	3675.	1800.
3.33	6.8	0.119E-05	0.258E-02	4050.	1800.
3.67	6.8	0.956E-06	0.258E-02	4425.	1875.
4.00	6.8	0.778E-06	0.258E-02	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME (SEC)	SNAPSHOT			ACCUMULATED		
	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF copper FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF copper IS 0.340000E-02 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.2580000E-02 MG/L.

THE WATER QUALITY STANDARD FOR copper IS 0.3100000E-02 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	1) = 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	1) = 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	1) = 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	1) = 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	1) = 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	1) = 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	1) = 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	1) = 201.4	11.31	0.1341	8.588	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	1) = 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	1) = 214.3	11.55	0.9280E-01	6.297	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	1) = 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	2) = 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	2) = 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	2) = 144.6	9.538	0.6070	13.14	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	2) = 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	2) = 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	2) = 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	2) = 193.7	11.14	0.1709	4.997	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	2) = 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	2) = 208.2	11.44	0.1096	3.434	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	2) = 214.3	11.55	0.9280E-01	2.986	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	2) = 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.57	500.0	1575.	114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 31.13	499.7	1575.	128.4	8.827	0.7117	5.741	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 31.70	499.5	1575.	144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 32.27	499.4	1575.	160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 32.83	499.3	1575.	173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 33.40	499.3	1575.	184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 33.97	499.3	1575.	193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 34.53	499.3	1575.	201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 35.10	499.3	1575.	208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 35.67	499.3	1575.	214.3	11.55	0.9280E-01	1.260	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 11 35.69	499.3	1575.	214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	4) = 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	4) = 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	4) = 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	4) = 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	4) = 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	4) = 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	4) = 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	4) = 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	4) = 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	4) = 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	4) = 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	5) = 1 214.5	10.08	3.420	5498.	3720.	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 128.12

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4904.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 51.587

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4981.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 21.039

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5011.7

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	1.250	0.0000E+00	420.7	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	0.9148	0.0000E+00	443.1	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	0.8659	0.0000E+00	468.8	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.6671	0.0000E+00	492.8	0.0000E+00	13.50	0.100000E-01
5	1562.	1650.	0.5040	0.0000E+00	512.9	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.3810	0.0000E+00	529.3	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.2980	0.0000E+00	542.7	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.2459	0.0000E+00	554.0	0.0000E+00	13.50	0.100000E-01
9	1562.	1650.	0.2051	0.0000E+00	563.8	0.0000E+00	13.50	0.100000E-01
10	1561.	1650.	0.1706	0.0000E+00	572.5	0.0000E+00	13.50	0.100000E-01
11	1561.	1650.	15.54	0.0000E+00	572.8	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 8.5805
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5024.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.4994
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.4272
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.8483E-01	0.0000E+00	856.1	0.0000E+00	0.100000E-01
2	2636.	1726.	0.6206E-01	0.0000E+00	884.9	0.0000E+00	0.100000E-01
3	2636.	1726.	0.5874E-01	0.0000E+00	917.7	0.0000E+00	0.100000E-01
4	2635.	1726.	0.4525E-01	0.0000E+00	948.2	0.0000E+00	0.100000E-01
5	2635.	1726.	0.3419E-01	0.0000E+00	973.5	0.0000E+00	0.100000E-01
6	2635.	1726.	0.2584E-01	0.0000E+00	994.1	0.0000E+00	0.100000E-01
7	2635.	1726.	0.2022E-01	0.0000E+00	1011.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.1668E-01	0.0000E+00	1025.	0.0000E+00	0.100000E-01
9	2634.	1725.	0.1391E-01	0.0000E+00	1037.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1157E-01	0.0000E+00	1048.	0.0000E+00	0.100000E-01
11	2634.	1725.	1.054	0.0000E+00	1048.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.58207
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.23739
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.96817E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.5754E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.4210E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.3985E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3070E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2319E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1753E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1371E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1132E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.9436E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.7852E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7149E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.39486E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.16104E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65677E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM		MASS FROM DISPOSAL	ENTRAINED MASS	CLOUD X-Z DIAMETER	DEPTH OF TOP OF CLOUD	CLOUD VERT. THICKNESS	SOLIDS FALL VELOCITY
	TOP OF GRID	LEFT OF GRID	(CU FT)	(CU FT)	(FT)	(FT)	(FT)	(FPS)
1	4782.	1877.	0.3904E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2856E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.2703E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2082E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1573E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1189E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.9304E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.7677E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.6401E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.5326E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4850E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 938.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1183.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.09

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1694.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 343.50

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1778.7

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows. The table contains numerical values and symbols (+, =) representing the bottom accumulation of clay over time and grid squares. Values are zero for most grid squares, with non-zero values appearing in a diagonal pattern from (2,2) to (31,31).

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	96.43	0.0000E+00	420.7	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	3.412	0.0000E+00	443.1	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	3.268	0.0000E+00	468.8	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	2.684	0.0000E+00	492.8	0.0000E+00	13.50	0.200000E-02
5	1562.	1650.	2.040	0.0000E+00	512.9	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	1.556	0.0000E+00	529.3	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	1.188	0.0000E+00	542.7	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	0.9942	0.0000E+00	554.0	0.0000E+00	13.50	0.200000E-02
9	1562.	1650.	0.8375	0.0000E+00	563.8	0.0000E+00	13.50	0.200000E-02
10	1561.	1650.	0.7256	0.0000E+00	572.5	0.0000E+00	13.50	0.200000E-02
11	1435.	1641.	230.4	0.0000E+00	572.8	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 287.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 240.57
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1881.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 201.32
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1920.9

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	56.52	0.0000E+00	856.1	0.0000E+00	13.50	0.200000E-02
2	2636.	1726.	2.000	0.0000E+00	884.9	0.0000E+00	13.50	0.200000E-02
3	2636.	1726.	1.915	0.0000E+00	917.7	0.0000E+00	13.50	0.200000E-02
4	2635.	1726.	1.573	0.0000E+00	948.2	0.0000E+00	13.50	0.200000E-02
5	2635.	1726.	1.195	0.0000E+00	973.5	0.0000E+00	13.50	0.200000E-02
6	2635.	1726.	0.9122	0.0000E+00	994.1	0.0000E+00	13.50	0.200000E-02
7	2635.	1726.	0.6960	0.0000E+00	1011.	0.0000E+00	13.50	0.200000E-02
8	2635.	1725.	0.5827	0.0000E+00	1025.	0.0000E+00	13.50	0.200000E-02
9	2634.	1725.	0.4908	0.0000E+00	1037.	0.0000E+00	13.50	0.200000E-02
10	2634.	1725.	0.4253	0.0000E+00	1048.	0.0000E+00	13.50	0.200000E-02
11	2508.	1717.	135.0	0.0000E+00	1048.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 168.48
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1953.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1981.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 117.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2004.2

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	33.12	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.9218	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7006	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5347	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4079	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	3707. 1801.	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.2877	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	3581. 1792.	79.13	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 98.744
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2023.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 82.635
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2039.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 69.155
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2052.3

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0
44	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
45	.15	.13	.12	.10	.09	.08	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
46	.19	.17	.15	.14	.12	.10	.08	.07	.06	.04	.04	.03	.02	0	0	0	0
47	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
48	.31	.28	.25	.22	.19	.16	.14	.11	.09	.07	.06	.05	.03	0	0	0	0
49	.38	.35	.31	.27	.24	.20	.17	.14	.12	.09	.07	.06	.04	0	0	0	0
50	.47	.43	.38	.34	.29	.25	.21	.17	.14	.12	.09	.07	.05	0	0	0	0
51	.57	.52	.46	.41	.35	.30	.25	.21	.17	.14	.11	.09	.07	0	0	0	0
52	.68	.61	.55	.49	.42	.36	.30	.25	.21	.17	.13	.10	.08	0	0	0	0
53	.80	.72	.65	.57	.50	.42	.36	.30	.24	.20	.16	.12	.09	0	0	0	0
54	.93	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	.11	0	0	0	0
55	1.0	.96	.86	.76	.66	.56	.47	.39	.32	.26	.21	.16	.12	0	0	0	0
56	1.1	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
57	1.3	1.2	1.0	.95	.82	.70	.59	.49	.40	.32	.26	.20	.16	0	0	0	0
58	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.36	.28	.22	.17	0	0	0	0
59	1.5	1.4	1.2	1.1	.97	.83	.70	.58	.48	.38	.30	.24	.18	0	0	0	0
60	1.6	1.5	1.3	1.1	1.0	.88	.74	.62	.51	.41	.32	.25	.19	0	0	0	0

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	0	0	0	0	0	0	00000
24	+	+	+	+	+	0	0	0	0	0	00000
25	.01	+	+	+	+	+	0	0	00000
26	.01	+	+	+	+	+	0	00000
27	.02	.01	+	+	+	+	00000
28	.03	.01	+	+	+	+	+	+0000
29	.03	.01	+	+	+	+	+	+	+0000
30	.04	.02	.01	+	+	+	+	+	+0000
31	.05	.03	.01	+	+	+	+	+	+0000
32	.06	.03	.01	.01	+	+	+	+	+	+0000
33	.07	.04	.02	.01	+	+	+	+	+	+	+0000
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+0000
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+0000
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+0000
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	+0000
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	+0000
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+0000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	19.41	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.6580	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4106	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.2391	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2002	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1686	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	4654.	1868.	46.38	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	0	0	0	0	0	0	00000
24	+	+	+	+	+	0	0	0	0	0	00000
25	.01	+	+	+	+	+	0	0	0	00000
26	.01	+	+	+	+	+	0	0	00000
27	.02	.01	+	+	+	+	00000
28	.03	.01	+	+	+	+	+	+0000
29	.03	.01	+	+	+	+	+	+	+0000
30	.04	.02	.01	+	+	+	+	+	+	+0000
31	.05	.03	.01	+	+	+	+	+	+	+0000
32	.06	.03	.01	.01	+	+	+	+	+	+0000
33	.07	.04	.02	.01	+	+	+	+	+	+	+0000
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+0000
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+0000
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+0000
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	+0000
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	+0000
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+0000
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+0000

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BOTTOM ACCUMULATION OF Clumps (CU FT/GRID SQUARE) , 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 10.00 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns M N= 2 to 31 and rows 2 to 59. Row 2 is a long string of zeros. Rows 3-59 contain numerical values for each column, with some non-zero values appearing in the first 20 columns of the first 10 rows.

BEGIN LONG TERM SIMULATION OF FATE OF copper

SUMMARY OF copper DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1778.0

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.3	1599.	0.1013E+06	0.9953E+05	317.4	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1777.2

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	0.1834E+06	0.1816E+06	438.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1777.2

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1561.	1650.	0.3176E+06	0.3158E+06	572.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1778.8

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	0.5052E+06	0.5034E+06	719.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1778.8

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	0.7555E+06	0.7537E+06	878.7	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1778.8

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	0.1078E+07	0.1076E+07	1048.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1772.5

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2992.	1751.	0.1482E+07	0.1480E+07	1228.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1772.6

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3349.	1776.	0.1977E+07	0.1975E+07	1418.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1772.8

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3707.	1801.	0.2573E+07	0.2571E+07	1617.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1760.5

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4065.	1826.	0.3279E+07	0.3277E+07	1825.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1760.5

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4422.	1851.	0.4104E+07	0.4103E+07	2041.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1761.0

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.31	.28	.25	.23	.20	.17	.14	.12	.10	.08	.06	.05	.04	0	0	0	00000
45	.41	.38	.34	.30	.26	.23	.19	.16	.13	.11	.09	.07	.05	0	0	0	00000
46	.54	.49	.44	.39	.34	.30	.25	.21	.18	.14	.11	.09	.07	0	0	0	00000
47	.69	.63	.57	.51	.44	.38	.33	.27	.23	.19	.15	.12	.09	0	0	0	00000
48	.88	.80	.72	.64	.56	.49	.42	.35	.29	.24	.19	.15	.12	0	0	0	00000
49	1.1	1.0	.91	.81	.71	.61	.52	.44	.36	.30	.24	.19	.15	0	0	0	00000
50	1.3	1.2	1.1	.99	.87	.75	.64	.54	.45	.37	.30	.23	.18	0	0	0	00000
51	1.6	1.5	1.3	1.2	1.0	.92	.78	.66	.55	.45	.36	.29	.22	0	0	0	00000
52	1.9	1.8	1.6	1.4	1.2	1.1	.94	.79	.66	.54	.43	.34	.27	0	0	0	00000
53	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.94	.78	.64	.51	.41	.32	0	0	0	00000
54	2.7	2.5	2.2	2.0	1.7	1.5	1.3	1.1	.91	.74	.60	.48	.37	0	0	0	00000
55	3.1	2.8	2.6	2.3	2.0	1.7	1.5	1.2	1.0	.86	.69	.55	.43	0	0	0	00000
56	3.5	3.2	2.9	2.6	2.3	2.0	1.7	1.4	1.1	.97	.79	.63	.49	0	0	0	00000
57	4.0	3.6	3.3	2.9	2.5	2.2	1.9	1.6	1.3	1.0	.88	.70	.55	0	0	0	00000
58	4.4	4.0	3.6	3.2	2.8	2.4	2.1	1.7	1.4	1.2	.97	.78	.61	0	0	0	00000
59	4.8	4.4	3.9	3.5	3.1	2.6	2.3	1.9	1.6	1.3	1.0	.85	.66	0	0	0	00000
60	5.1	4.7	4.2	3.8	3.3	2.8	2.4	2.0	1.7	1.4	1.1	.91	.71	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	00000
45	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	00000
46	.20	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	00000
47	.25	.23	.21	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	0	0	0	00000
48	.32	.29	.26	.23	.21	.18	.15	.13	.10	.08	.07	.05	.04	0	0	0	00000
49	.40	.37	.33	.29	.26	.22	.19	.16	.13	.11	.09	.07	.05	0	0	0	00000
50	.50	.46	.41	.36	.32	.28	.23	.20	.16	.13	.11	.08	.06	0	0	0	00000
51	.61	.55	.50	.44	.39	.34	.29	.24	.20	.16	.13	.10	.08	0	0	0	00000
52	.73	.67	.60	.53	.47	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	00000
53	.86	.79	.71	.63	.55	.48	.41	.34	.28	.23	.19	.15	.12	0	0	0	00000
54	1.0	.92	.83	.74	.65	.56	.48	.40	.33	.27	.22	.17	.14	0	0	0	00000
55	1.1	1.0	.96	.85	.75	.65	.55	.46	.38	.31	.25	.20	.16	0	0	0	00000
56	1.3	1.2	1.0	.97	.85	.73	.63	.53	.44	.36	.29	.23	.18	0	0	0	00000
57	1.4	1.3	1.2	1.0	.95	.82	.70	.59	.49	.40	.32	.26	.20	0	0	0	00000
58	1.6	1.4	1.3	1.2	1.0	.91	.78	.65	.54	.44	.36	.28	.22	0	0	0	00000
59	1.7	1.6	1.4	1.3	1.1	.99	.85	.71	.59	.48	.39	.31	.24	0	0	0	00000
60	1.9	1.7	1.5	1.4	1.2	1.0	.91	.77	.63	.52	.42	.33	.26	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
33	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
35	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	00000
36	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	00000
37	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	00000
38	.02	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
39	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
40	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
41	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	00000
42	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	00000
43	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	00000
44	.02	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	00000
45	.02	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	00000
46	.02	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	00000
47	.02	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	00000
48	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
49	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
50	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
51	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
52	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
53	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
54	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
55	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
56	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
57	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
58	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
59	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
60	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4780.	1877.	0.5059E+07	0.5057E+07	2266.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.122E+02	1575.	1650.
2.00	0.0	0.236E+00	2625.	1725.
3.00	0.0	0.659E-02	3675.	1800.
4.00	0.0	0.226E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.200E+03	1500.	1650.
2.00	0.0	0.346E+02	2550.	1725.
3.00	0.0	0.834E+01	3675.	1800.
4.00	0.0	0.246E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR copper

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE		X-LOC (FT)	Z-LOC (FT)
		BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)		
0.33	0.0	0.374E-04	0.262E-02	825.	1575.
0.67	0.0	0.205E-04	0.260E-02	1200.	1650.
1.00	0.0	0.122E-04	0.259E-02	1575.	1650.
1.33	0.0	0.761E-05	0.259E-02	1950.	1650.
1.67	0.0	0.515E-05	0.259E-02	2250.	1725.
2.00	0.0	0.366E-05	0.258E-02	2625.	1725.
2.33	0.0	0.265E-05	0.258E-02	3000.	1725.
2.67	0.0	0.198E-05	0.258E-02	3375.	1800.
3.00	0.0	0.153E-05	0.258E-02	3675.	1800.
3.33	0.0	0.119E-05	0.258E-02	4050.	1800.
3.67	0.0	0.954E-06	0.258E-02	4425.	1875.
4.00	0.0	0.775E-06	0.258E-02	4800.	1875.
0.33	6.8	0.138E-03	0.272E-02	825.	1575.
0.67	6.8	0.756E-04	0.266E-02	1200.	1650.
1.00	6.8	0.451E-04	0.263E-02	1575.	1650.
1.33	6.8	0.281E-04	0.261E-02	1950.	1650.
1.67	6.8	0.190E-04	0.260E-02	2250.	1725.
2.00	6.8	0.135E-04	0.259E-02	2625.	1725.
2.33	6.8	0.978E-05	0.259E-02	3000.	1725.
2.67	6.8	0.733E-05	0.259E-02	3375.	1800.
3.00	6.8	0.565E-05	0.259E-02	3675.	1800.
3.33	6.8	0.441E-05	0.258E-02	4050.	1800.
3.67	6.8	0.353E-05	0.258E-02	4425.	1875.
4.00	6.8	0.286E-05	0.258E-02	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

3	3							3
	TIME	SNAPSHOT			ACCUMULATED			
3	(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	3
3	1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3	14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	3
3								3

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF copper FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF copper IS 0.665000E-02 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.2580000E-02 MG/L.

THE WATER QUALITY STANDARD FOR copper IS 0.3100000E-02 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	1) = 109.2	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	1) = 130.9	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	1) = 152.5	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	1) = 171.5	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	1) = 187.3	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	1) = 200.5	10.89	0.2393	53.70	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	1) = 211.8	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	1) = 221.7	11.31	0.1469	35.76	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	1) = 230.7	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	1) = 238.9	11.58	0.1054	27.19	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	1) = 239.2	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	2) = 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	2) = 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	2) = 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	2) = 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	2) = 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	2) = 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	2) = 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	2) = 221.7	11.31	0.1469	0.4822	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	2) = 230.7	11.46	0.1227	0.4153	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	2) = 238.9	11.58	0.1054	0.3668	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	2) = 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.59	500.0	1575.	109.2	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 31.19	499.8	1575.	130.9	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 31.78	499.6	1575.	152.5	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 32.38	499.5	1575.	171.5	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 32.97	499.5	1575.	187.3	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 33.56	499.5	1575.	200.5	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 34.16	499.5	1575.	211.8	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 34.75	499.5	1575.	221.7	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 35.35	499.5	1575.	230.7	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 35.94	499.5	1575.	238.9	11.58	0.1054	0.1514	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 11 35.96	499.5	1575.	239.2	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	X-LOCATION 499.5	Z-LOCATION 1575.	4) = 1 239.2	9.685	3.815	8474.	6684.	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.411
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 493.19

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 38.912
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 549.69

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 15.870
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 572.73

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	1.488	0.0000E+00	411.8	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	0.1670	0.0000E+00	447.2	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	0.1244	0.0000E+00	481.0	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.8470E-01	0.0000E+00	509.8	0.0000E+00	13.50	0.100000E-01
5	1562.	1650.	0.6077E-01	0.0000E+00	533.4	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.4553E-01	0.0000E+00	552.7	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.3587E-01	0.0000E+00	569.0	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	13.50	0.100000E-01
9	1562.	1650.	0.2516E-01	0.0000E+00	596.0	0.0000E+00	13.50	0.100000E-01
10	1562.	1650.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	13.50	0.100000E-01
11	1562.	1650.	13.79	0.0000E+00	607.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.4723
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 582.12

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.6397
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.96

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.0766
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.52
 MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 7200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns M N= 2 to 31 and rows 2 to 59. Row 2 is a long string of zeros. Rows 3-59 show numerical values and '+' symbols representing silt accumulation. Values increase significantly in the first 20 rows and then stabilize.

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1009	0.0000E+00	844.6	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.8436E-02	0.0000E+00	933.3	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.5746E-02	0.0000E+00	969.7	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.4122E-02	0.0000E+00	999.2	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	13.50	0.100000E-01
7	2635.	1725.	0.2433E-02	0.0000E+00	1044.	0.0000E+00	13.50	0.100000E-01
8	2635.	1725.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	13.50	0.100000E-01
9	2635.	1725.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	0.9353	0.0000E+00	1092.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.43906
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.16

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17907
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.42

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73030E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.52

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
24	+	+	+	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	0	0	0	0	0	0	0	0	00000
26	+	+	+	+	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	0	0	0	0	0	0	0	00000
28	+	+	+	+	0	0	0	0	0	0	0	00000
29	+	+	+	+	+	0	0	0	0	0	0	00000
30	+	+	+	+	+	0	0	0	0	0	0	00000
31	+	+	+	+	+	0	0	0	0	0	00000
32	+	+	+	+	+	+	0	0	0	0	00000
33	+	+	+	+	+	+	0	0	0	00000
34	+	+	+	+	+	+	0	0	0	00000
35	+	+	+	+	+	+	0	0	00000
36	+	+	+	+	+	+	+	0	00000
37	+	+	+	+	+	+	+	0	00000
38	+	+	+	+	+	+	+	00000
39	+	+	+	+	+	+	+	00000
40	+	+	+	+	+	+	+	00000
41	+	+	+	+	+	+	+	00000
42	+	+	+	+	+	+	+	00000
43	+	+	+	+	+	+	+	00000
44	+	+	+	+	+	+	+	00000
45	+	+	+	+	+	+	+	00000
46	+	+	+	+	+	+	+0000
47	+	+	+	+	+	+	+0000
48	+	+	+	+	+	+	+0000
49	+	+	+	+	+	+	+0000
50	+	+	+	+	+	+	+0000
51	+	+	+	+	+	+	+0000
52	+	+	+	+	+	+	+	00000
53	+	+	+	+	+	+	+	00000
54	+	+	+	+	+	+	+	00000
55	+	+	+	+	+	+	+	00000
56	+	+	+	+	+	+	+	00000
57	+	+	+	+	+	+	+	00000
58	+	+	00000
59	+	00000
60	0	0	0	00000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	0.6846E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	3709. 1801.	0.7684E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	3709. 1801.	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	3708. 1801.	0.3898E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	3708. 1801.	0.2796E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	3708. 1801.	0.2095E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	3708. 1801.	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	3708. 1801.	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	3707. 1801.	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	3707. 1801.	0.1004E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	3707. 1801.	0.6345E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.29784E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.57

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12147E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.49541E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.59

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4644E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3882E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2644E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1421E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7853E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6808E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4304E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns labeled M N= 2 through 31 and rows numbered 2 through 59. The table contains numerical values and symbols (+) representing silt accumulation. Values increase from 0 in the top row to approximately 0.01 in the bottom row, with a '0' symbol appearing in the first row.

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.871

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.29

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.710

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 136.65

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 106.35

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns M N= 2 to 31 and rows 2 to 59. The table contains numerical values representing clay accumulation, with a row of zeros at the top (row 2) and values increasing from row 3 onwards. The values are mostly small, with some larger values appearing in the middle rows (e.g., row 10-17).

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	13.35	0.0000E+00	411.8	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	0.5799	0.0000E+00	447.2	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	0.4376	0.0000E+00	481.0	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	0.3164	0.0000E+00	509.8	0.0000E+00	13.50	0.200000E-02
5	1562.	1650.	0.2289	0.0000E+00	533.4	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	0.1739	0.0000E+00	552.7	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	0.1387	0.0000E+00	569.0	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	0.1153	0.0000E+00	583.3	0.0000E+00	13.50	0.200000E-02
9	1562.	1650.	0.9923E-01	0.0000E+00	596.0	0.0000E+00	13.50	0.200000E-02
10	1562.	1650.	0.8740E-01	0.0000E+00	607.5	0.0000E+00	13.50	0.200000E-02
11	1562.	1650.	121.1	0.0000E+00	607.9	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.36
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.64

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.702
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 147.30

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.090
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.91

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637. 1726.	7.825	0.0000E+00	844.6	0.0000E+00	13.50	0.200000E-02
2	2636. 1726.	0.3399	0.0000E+00	890.2	0.0000E+00	13.50	0.200000E-02
3	2636. 1726.	0.2564	0.0000E+00	933.3	0.0000E+00	13.50	0.200000E-02
4	2635. 1726.	0.1854	0.0000E+00	969.7	0.0000E+00	13.50	0.200000E-02
5	2635. 1726.	0.1342	0.0000E+00	999.2	0.0000E+00	13.50	0.200000E-02
6	2635. 1726.	0.1019	0.0000E+00	1023.	0.0000E+00	13.50	0.200000E-02
7	2635. 1725.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	13.50	0.200000E-02
8	2635. 1725.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	13.50	0.200000E-02
9	2635. 1725.	0.5816E-01	0.0000E+00	1077.	0.0000E+00	13.50	0.200000E-02
10	2634. 1725.	0.5122E-01	0.0000E+00	1091.	0.0000E+00	13.50	0.200000E-02
11	2634. 1725.	70.99	0.0000E+00	1092.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.024
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.91

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 46.940
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 196.06

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	4.586	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5973E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4763E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	3708. 1801.	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.3409E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	3707. 1801.	41.61	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.282
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.69

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.874
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.511
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 215.12

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.03	.03	.03	.02	.02	.02	.01	.01	.01	.01	+	+	+	0	0	0	0
45	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	0	0	0	0
46	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0
47	.08	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
48	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
49	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
50	.16	.14	.13	.11	.10	.09	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
51	.19	.17	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
52	.23	.21	.19	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
53	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	0
54	.32	.29	.26	.23	.20	.18	.15	.13	.10	.08	.07	.05	.04	0	0	0	0
55	.36	.33	.30	.27	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
56	.41	.38	.34	.30	.27	.23	.20	.16	.14	.11	.09	.07	.06	0	0	0	0
57	.46	.42	.38	.34	.30	.26	.22	.18	.15	.13	.10	.08	.06	0	0	0	0
58	.51	.47	.42	.37	.33	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
59	.56	.51	.46	.41	.36	.31	.26	.22	.18	.15	.12	.10	.08	0	0	0	0
60	.60	.55	.49	.44	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM		MASS FROM DISPOSAL	ENTRAINED MASS	CLOUD X-Z DIAMETER	DEPTH OF TOP OF CLOUD	CLOUD VERT. THICKNESS	SOLIDS FALL VELOCITY
	TOP OF GRID	LEFT OF GRID	(CU FT)	(CU FT)	(FT)	(FT)	(FT)	(FPS)
1	4782.	1877.	2.688	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1998E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1759E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	4780.	1877.	24.38	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31
2 000
3 0000
4 0000
5 0000
6 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 .
7 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + + + + .
8 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + .01 .01 .01 + + + .
9 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + .03 .10 .16 .14 .07 .02 + + .
10 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + .03 .17 .52 .86 .77 .38 .10 .01 + .
11 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + .01 .09 .51 1.5 2.6 2.3 1.1 .30 .04 + + .
12 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + .01 .15 .83 2.6 4.8 4.2 1.8 .49 .07 + + .
13 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + .01 .14 .75 2.3 4.2 3.7 1.6 .47 .08 .01 + + .
14 0000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 + + .01 .10 .45 1.2 2.0 1.9 1.0 .34 .08 .01 + + .
15 0000 0 0 0 0 0 0 0 0 0 0 0 0 + + .02 .10 .34 .78 1.2 1.2 .80 .37 .13 .03 + + + .
16 0000 0 0 0 0 0 0 0 0 0 0 0 0 + + + .04 .15 .43 .93 1.4 1.5 1.1 .56 .22 .06 .01 + + .
17 0000 0 0 0 0 0 0 0 0 0 0 0 + + .01 .05 .18 .52 1.1 1.7 1.9 1.3 .70 .28 .08 .02 + + + .
18 0000 0 0 0 0 0 0 0 0 0 0 + + + .01 .05 .18 .50 1.0 1.6 1.7 1.2 .68 .29 .10 .03 + + + .
19 0000 0 0 0 0 0 0 0 0 0 0 + + + .01 .05 .17 .41 .79 1.1 1.2 .98 .59 .29 .11 .04 .01 + + + .
20 0000 0 0 0 0 0 0 0 0 + + + .02 .06 .16 .36 .65 .92 1.0 .86 .57 .31 .14 .06 .02 + + + .
21 0000 0 0 0 0 0 0 0 0 + + + .02 .07 .18 .38 .65 .91 1.0 .89 .63 .37 .18 .08 .03 .01 + + + .
22 0000 0 0 0 0 0 0 0 + + + .01 .03 .08 .20 .40 .67 .94 1.0 .94 .68 .41 .21 .09 .04 .01 + + + .
23 0000 0 0 0 0 0 0 + + + + .01 .03 .09 .20 .39 .64 .88 .98 .89 .67 .42 .23 .11 .04 .01 + + + .
24 0000 0 0 0 0 0 + + + + .01 .04 .09 .19 .36 .57 .76 .85 .79 .61 .41 .23 .12 .05 .02 .01 + + + .
25 0000 0 0 0 0 + + + + .01 .04 .09 .19 .33 .50 .66 .74 .70 .57 .40 .24 .13 .07 .03 .01 + + + .
26 0000 0 0 0 + + + + + .02 .04 .10 .19 .31 .47 .61 .68 .66 .55 .40 .26 .15 .08 .04 .01 + + + .
27 0000 0 0 + + + + + .01 .02 .05 .10 .19 .31 .45 .57 .64 .63 .54 .41 .27 .16 .09 .05 .02 + + + .
28 0000 0 + + + + + .01 .02 .05 .10 .19 .30 .42 .54 .60 .60 .52 .40 .28 .17 .10 .05 .02 + + + .
29 0000 + + + + + .01 .03 .06 .11 .18 .28 .39 .49 .55 .55 .49 .39 .28 .18 .11 .06 .03 + + + .
30 0000 + + + + + .01 .03 .06 .11 .17 .26 .36 .45 .50 .50 .45 .37 .27 .19 .12 .07 .04 + + + .
31 0000 + + + + + + .01 .03 .06 .10 .17 .25 .34 .41 .46 .46 .42 .35 .27 .19 .12 .07 .04 + + + .
32 0000 + + + + + + .01 .02 .03 .06 .10 .16 .24 .31 .38 .43 .43 .40 .34 .27 .19 .13 .08 .05 + + + .
33 0000 + + + + + + .01 .02 .04 .06 .10 .16 .22 .29 .36 .40 .40 .38 .33 .26 .19 .13 .09 .05 + + + .
34 0000 + + + + + + + .01 .02 .04 .06 .10 .15 .21 .28 .33 .37 .38 .36 .31 .25 .19 .14 .09 .06 + + + .
35 0000 + + + + + + + .01 .02 .04 .06 .10 .15 .20 .26 .31 .34 .35 .33 .29 .24 .19 .14 .10 .06 + + + .
36 0000 + + + + + + + .01 .02 .04 .06 .10 .14 .19 .24 .28 .31 .32 .31 .28 .23 .19 .14 .10 .07 + + + .
37 0000 + + + + + + .01 .01 .02 .04 .06 .10 .14 .18 .22 .26 .29 .30 .29 .26 .23 .18 .14 .10 .07 + + + .
38 0000 + + + + + + + .01 .01 .02 .04 .06 .09 .13 .17 .21 .25 .27 .28 .27 .25 .22 .18 .14 .10 .07 + + + .
39 0000 + + + + + + + .01 .01 .03 .04 .06 .09 .12 .16 .20 .23 .25 .26 .25 .24 .21 .17 .14 .10 .07 + + + .
40 0000 . + + + + + + + + + + .01 .02 .03 .04 .06 .09 .12 .15 .18 .21 .23 .24 .24 .22 .20 .17 .13 .10 .08 + + + .
41 0000 + + + + + + + + + + .01 .02 .03 .04 .06 .09 .11 .14 .17 .20 .22 .23 .22 .21 .19 .16 .13 .10 .08 + + + .
42 0000 + + + + + + + + + + .01 .02 .03 .04 .06 .08 .11 .14 .16 .19 .20 .21 .21 .20 .18 .15 .13 .10 .08 + + + .
43 0000 + + + + + + + + + + .01 .02 .03 .04 .06 .08 .10 .13 .15 .17 .19 .20 .19 .19 .17 .15 .12 .10 .08 + + + .
44 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .06 .08 .10 .12 .14 .16 .18 .18 .18 .17 .16 .14 .12 .10 .08 + + + .
45 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .06 .07 .09 .11 .13 .15 .16 .17 .17 .16 .15 .13 .12 .10 .08 + + + .
46 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .05 .07 .09 .11 .13 .14 .15 .16 .16 .15 .14 .13 .11 .09 .08 + + + .
47 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .05 .07 .08 .10 .12 .13 .14 .15 .15 .14 .14 .12 .11 .09 .07 + + + .
48 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .05 .06 .08 .10 .11 .12 .13 .14 .14 .14 .13 .12 .10 .09 .07 + + + .
49 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .05 .06 .08 .09 .10 .11 .12 .13 .13 .13 .12 .11 .10 .08 .07 + + + .
50 0000 + + + + + + + + + + .01 .01 .02 .03 .04 .05 .06 .07 .08 .10 .11 .12 .12 .12 .12 .11 .10 .09 .08 .07 + + + .
51 0000 + + + + + + + + + + .01 .01 .02 .03 .03 .04 .06 .07 .08 .09 .10 .11 .11 .11 .11 .11 .11 .10 .09 .08 .07 + + + .
52 0000 + + + + + + + + + + .01 .01 .02 .03 .03 .04 .05 .06 .07 .08 .09 .10 .10 .11 .10 .10 .10 .09 .08 .07 .06 + + + .
53 0000 + + + + + + + + + + .01 .01 .02 .02 .03 .04 .05 .06 .07 .08 .09 .09 .10 .10 .10 .10 .09 .09 .08 .07 .06 + + + .
54 0000 + + + + + + + + + + .01 .01 .02 .02 .03 .04 .05 .06 .07 .07 .08 .09 .09 .09 .09 .09 .09 .08 .08 .07 .06 + + + .
55 0000 + + + + + + + + + + .01 .01 .02 .02 .03 .04 .05 .05 .06 .07 .08 .08 .08 .09 .09 .08 .08 .07 .06 .06 + + + .
56 0000 + + + + + + + + + + .01 .01 .02 .02 .03 .04 .04 .05 .06 .06 .07 .08 .08 .08 .08 .08 .08 .07 .07 .06 .05 + + + .
57 0000 + + + + + + + + + + .01 .01 .02 .02 .03 .03 .04 .05 .05 .06 .07 .07 .07 .07 .07 .07 .07 .07 .06 .06 .05 + + + .
58 0000 + + + + + + + + + + .01 .01 .01 .02 .03 .03 .04 .04 .05 .06 .06 .06 .07 .07 .07 .07 .07 .07 .06 .06 .05 .05 + + + .
59 0000 + + + + + + + + + + .01 .01 .01 .02 .02 .03 .03 .04 .05 .05 .06 .06 .06 .06 .06 .06 .06 .06 .06 .05 .04 + + + .

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
22	+	+	+	0	0	0	0	0	0	0	0	0
23	+	+	+	+	0	0	0	0	0	0	0	0
24	+	+	+	+	+	0	0	0	0	0	0	0
25	+	+	+	+	+	+	0	0	0	0	0	0
26	.01	+	+	+	+	+	0	0	0	0
27	.01	+	+	+	+	+	0	0	0	0
28	.02	.01	+	+	+	+	+	+	0
29	.02	.01	+	+	+	+	+	+0000
30	.03	.01	+	+	+	+	+	+0000
31	.04	.02	.01	+	+	+	+	+	+0000
32	.04	.02	.01	+	+	+	+	+	+0000
33	.05	.03	.01	+	+	+	+	+	+	+0000
34	.05	.03	.02	.01	+	+	+	+	+	+	+0000
35	.06	.04	.02	.01	+	+	+	+	+	+	+0000
36	.07	.04	.02	.01	.01	+	+	+	+	+	+	+0000
37	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+0000
38	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
39	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
40	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
41	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
42	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
43	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
44	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
45	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
46	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+0000
50	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
51	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
52	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
53	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
54	.08	.07	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
55	.08	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
56	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
58	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
59	.06	.05	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
60	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000

BEGIN LONG TERM SIMULATION OF FATE OF copper

SUMMARY OF copper DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1790.9

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.4	1599.	0.1199E+06	0.1181E+06	345.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	0.2105E+06	0.2088E+06	470.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1562.	1650.	0.3570E+06	0.3552E+06	607.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	0.5592E+06	0.5574E+06	758.0	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	0.8264E+06	0.8246E+06	919.5	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	0.1168E+07	0.1166E+07	1092.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1790.9

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2992.	1751.	0.1594E+07	0.1592E+07	1274.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1790.8

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3350.	1776.	0.2113E+07	0.2111E+07	1466.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3707.	1801.	0.2735E+07	0.2733E+07	1667.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4065.	1826.	0.3469E+07	0.3467E+07	1878.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4422.	1851.	0.4326E+07	0.4324E+07	2096.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1791.0

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.35	.32	.29	.26	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	00000
45	.46	.42	.38	.34	.30	.26	.22	.19	.16	.13	.10	.08	.07	0	0	0	00000
46	.59	.54	.49	.44	.39	.34	.29	.24	.20	.17	.14	.11	.09	0	0	0	00000
47	.75	.69	.63	.56	.49	.43	.37	.31	.26	.21	.17	.14	.11	0	0	0	00000
48	.94	.87	.78	.70	.62	.54	.46	.39	.33	.27	.22	.18	.14	0	0	0	00000
49	1.1	1.0	.97	.87	.77	.67	.57	.49	.41	.34	.27	.22	.17	0	0	0	00000
50	1.4	1.3	1.1	1.0	.94	.82	.70	.60	.50	.41	.33	.27	.21	0	0	0	00000
51	1.7	1.5	1.4	1.2	1.1	.99	.85	.72	.60	.50	.40	.33	.26	0	0	0	00000
52	2.0	1.8	1.7	1.5	1.3	1.1	1.0	.86	.72	.59	.48	.39	.31	0	0	0	00000
53	2.4	2.2	2.0	1.7	1.5	1.3	1.1	1.0	.84	.70	.57	.46	.36	0	0	0	00000
54	2.7	2.5	2.3	2.0	1.8	1.6	1.3	1.1	.98	.81	.66	.53	.42	0	0	0	00000
55	3.1	2.9	2.6	2.3	2.1	1.8	1.5	1.3	1.1	.92	.75	.61	.48	0	0	0	00000
56	3.6	3.3	2.9	2.6	2.3	2.0	1.7	1.5	1.2	1.0	.85	.68	.54	0	0	0	00000
57	4.0	3.6	3.3	2.9	2.6	2.3	1.9	1.6	1.4	1.1	.95	.76	.61	0	0	0	00000
58	4.4	4.0	3.6	3.2	2.9	2.5	2.1	1.8	1.5	1.2	1.0	.84	.67	0	0	0	00000
59	4.7	4.3	3.9	3.5	3.1	2.7	2.3	2.0	1.6	1.3	1.1	.91	.72	0	0	0	00000
60	5.1	4.7	4.2	3.8	3.3	2.9	2.5	2.1	1.8	1.4	1.2	.98	.77	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.13	.12	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	00000
45	.17	.15	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	00000
46	.22	.20	.18	.16	.14	.12	.10	.09	.07	.06	.05	.04	.03	0	0	0	00000
47	.27	.25	.23	.20	.18	.16	.13	.11	.09	.08	.06	.05	.04	0	0	0	00000
48	.35	.32	.29	.26	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	00000
49	.43	.39	.36	.32	.28	.24	.21	.18	.15	.12	.10	.08	.06	0	0	0	00000
50	.52	.48	.44	.39	.34	.30	.26	.22	.18	.15	.12	.10	.08	0	0	0	00000
51	.63	.58	.53	.47	.41	.36	.31	.26	.22	.18	.15	.12	.09	0	0	0	00000
52	.75	.69	.63	.56	.49	.43	.37	.31	.26	.22	.18	.14	.11	0	0	0	00000
53	.89	.81	.74	.66	.58	.51	.43	.37	.31	.25	.21	.17	.13	0	0	0	00000
54	1.0	.94	.85	.76	.67	.59	.50	.43	.36	.29	.24	.19	.15	0	0	0	00000
55	1.1	1.0	.98	.87	.77	.67	.58	.49	.41	.34	.27	.22	.17	0	0	0	00000
56	1.3	1.2	1.1	.99	.87	.76	.65	.55	.46	.38	.31	.25	.20	0	0	0	00000
57	1.4	1.3	1.2	1.1	.97	.85	.73	.62	.52	.43	.35	.28	.22	0	0	0	00000
58	1.6	1.4	1.3	1.2	1.0	.93	.80	.68	.57	.47	.38	.31	.24	0	0	0	00000
59	1.7	1.6	1.4	1.3	1.1	1.0	.87	.74	.62	.51	.41	.33	.26	0	0	0	00000
60	1.8	1.7	1.5	1.4	1.2	1.0	.93	.79	.66	.55	.44	.36	.28	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
32	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
33	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
34	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	00000
35	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
36	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
37	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
38	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
39	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
40	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	00000
41	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	00000
42	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	00000
43	.02	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	00000
44	.02	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	00000
45	.02	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	00000
46	.02	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	00000
47	.02	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	00000
48	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
49	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
50	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
51	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
52	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	00000
53	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
54	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
55	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
56	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
57	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
58	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
59	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	00000
60	.02	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	00000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4780.	1877.	0.5314E+07	0.5312E+07	2323.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM, 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows (3 0000 to 59 0000). The table displays numerical values for each cell, with many zeros and some values increasing from left to right and bottom to top. The values are small, often in the range of 0.01 to 0.72.

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.819E+01	1575.	1650.
2.00	0.0	0.164E+00	2625.	1725.
3.00	0.0	0.467E-02	3675.	1800.
4.00	0.0	0.162E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.702E+02	1575.	1650.
2.00	0.0	0.122E+02	2625.	1725.
3.00	0.0	0.299E+01	3675.	1800.
4.00	0.0	0.896E+00	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR copper

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE		X-LOC (FT)	Z-LOC (FT)
		BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)		
0.33	0.0	0.320E-04	0.261E-02	825.	1575.
0.67	0.0	0.180E-04	0.260E-02	1200.	1650.
1.00	0.0	0.109E-04	0.259E-02	1575.	1650.
1.33	0.0	0.692E-05	0.259E-02	1950.	1650.
1.67	0.0	0.474E-05	0.258E-02	2250.	1725.
2.00	0.0	0.339E-05	0.258E-02	2625.	1725.
2.33	0.0	0.249E-05	0.258E-02	3000.	1725.
2.67	0.0	0.188E-05	0.258E-02	3375.	1800.
3.00	0.0	0.145E-05	0.258E-02	3675.	1800.
3.33	0.0	0.115E-05	0.258E-02	4050.	1800.
3.67	0.0	0.920E-06	0.258E-02	4425.	1875.
4.00	0.0	0.750E-06	0.258E-02	4800.	1875.
0.33	6.8	0.118E-03	0.270E-02	825.	1575.
0.67	6.8	0.664E-04	0.265E-02	1200.	1650.
1.00	6.8	0.404E-04	0.262E-02	1575.	1650.
1.33	6.8	0.256E-04	0.261E-02	1950.	1650.
1.67	6.8	0.175E-04	0.260E-02	2250.	1725.
2.00	6.8	0.125E-04	0.259E-02	2625.	1725.
2.33	6.8	0.919E-05	0.259E-02	3000.	1725.
2.67	6.8	0.693E-05	0.259E-02	3375.	1800.
3.00	6.8	0.537E-05	0.259E-02	3675.	1800.
3.33	6.8	0.424E-05	0.258E-02	4050.	1800.
3.67	6.8	0.340E-05	0.258E-02	4425.	1875.
4.00	6.8	0.277E-05	0.258E-02	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME (SEC)	SNAPSHOT			ACCUMULATED		
	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF copper FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF copper IS 0.665000E-02 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.2580000E-02 MG/L.

THE WATER QUALITY STANDARD FOR copper IS 0.3100000E-02 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.000	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 72.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 235.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	1) = 1 123.6	9.291	0.6767E-01	140.1	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	1) = 2 137.3	9.359	0.5698	2.383	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	1) = 3 151.3	9.929	0.4586	2.134	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	1) = 4 163.7	10.39	0.3367	1.710	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	1) = 5 174.2	10.72	0.2440	1.325	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	1) = 6 182.8	10.97	0.1815	1.038	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	1) = 7 190.1	11.15	0.1404	0.8352	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	1) = 8 196.3	11.29	0.1129	0.6941	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	1) = 9 201.8	11.40	0.9417E-01	0.5948	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	1) = 10 206.8	11.50	0.8092E-01	0.5234	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	1) = 11 207.7	10.19	3.312	847.7	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(CU FT)	(CU FT)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	2) = 1 123.6	9.291	0.6767E-01	1135.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	2) = 2 137.3	9.359	0.5698	19.31	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	2) = 3 151.3	9.929	0.4586	17.29	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	2) = 4 163.7	10.39	0.3367	13.86	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	2) = 5 174.2	10.72	0.2440	10.74	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	2) = 6 182.8	10.97	0.1815	8.406	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	2) = 7 190.1	11.15	0.1404	6.765	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	2) = 8 196.3	11.29	0.1129	5.626	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	2) = 9 201.8	11.40	0.9417E-01	4.820	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	2) = 10 206.8	11.50	0.8092E-01	4.242	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	2) = 11 207.7	10.19	3.312	6869.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(CU FT)	(CU FT)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.54	500.0	1575.	123.6	9.291	0.6767E-01	446.7	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 31.09	499.7	1575.	137.3	9.359	0.5698	7.601	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 31.63	499.5	1575.	151.3	9.929	0.4586	6.806	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 32.18	499.4	1575.	163.7	10.39	0.3367	5.455	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 32.72	499.2	1575.	174.2	10.72	0.2440	4.227	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 33.27	499.1	1575.	182.8	10.97	0.1815	3.309	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 33.81	499.1	1575.	190.1	11.15	0.1404	2.663	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 34.35	499.0	1575.	196.3	11.29	0.1129	2.214	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 34.90	499.0	1575.	201.8	11.40	0.9417E-01	1.897	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 35.44	499.0	1575.	206.8	11.50	0.8092E-01	1.670	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 11 35.54	499.0	1575.	207.7	10.19	3.312	2703.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	4) = 123.6	13.50	0.1000E-02	3949.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	4) = 137.3	13.50	0.1000E-02	3128.	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	4) = 151.3	13.50	0.1000E-02	2120.	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	4) = 163.7	13.50	0.1000E-02	1343.	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	4) = 174.2	13.50	0.1000E-02	798.7	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	4) = 182.8	13.50	0.1000E-02	450.2	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	4) = 190.1	13.50	0.1000E-02	243.2	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	4) = 196.3	13.50	0.1000E-02	126.9	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	4) = 201.8	13.50	0.1000E-02	64.40	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	4) = 206.8	13.50	0.1000E-02	31.89	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	4) = 207.7	10.19	3.312	29.13	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	5) = 1 207.7	10.19	3.312	8554.	3012.	235	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.31

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7954.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 55.287

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8039.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.548

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8072.0

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1564.	1650.	1.588	0.0000E+00	435.4	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	1.229	0.0000E+00	457.2	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	1.037	0.0000E+00	479.1	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.8205	0.0000E+00	498.2	0.0000E+00	13.50	0.100000E-01
5	1562.	1650.	0.6312	0.0000E+00	513.9	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.4945	0.0000E+00	526.7	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.3970	0.0000E+00	537.4	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.3360	0.0000E+00	546.5	0.0000E+00	13.50	0.100000E-01
9	1561.	1650.	0.2856	0.0000E+00	554.5	0.0000E+00	13.50	0.100000E-01
10	1561.	1650.	0.2423	0.0000E+00	561.7	0.0000E+00	13.50	0.100000E-01
11	1561.	1650.	15.49	0.0000E+00	562.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.1960
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.7505
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5296
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.1
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1077	0.0000E+00	875.0	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.8339E-01	0.0000E+00	903.0	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.7035E-01	0.0000E+00	930.9	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.5566E-01	0.0000E+00	955.0	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.4282E-01	0.0000E+00	974.8	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.3355E-01	0.0000E+00	990.9	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2693E-01	0.0000E+00	1004.	0.0000E+00	13.50	0.100000E-01
8	2634.	1725.	0.2279E-01	0.0000E+00	1016.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1937E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1644E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.051	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.62383
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25442
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10376
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	0	0	0	0	0	0	0	0	0	0	00000
24	+	+	0	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	0	0	0	0	0	0	0	0	0	00000
26	+	+	+	0	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	0	0	0	0	0	0	0	0	00000
28	+	+	+	+	0	0	0	0	0	0	0	0	00000
29	+	+	+	+	0	0	0	0	0	0	0	00000
30	+	+	+	+	+	0	0	0	0	0	0	00000
31	+	+	+	+	+	0	0	0	0	0	0	00000
32	+	+	+	+	+	0	0	0	0	0	00000
33	+	+	+	+	+	+	0	0	0	0	00000
34	+	+	+	+	+	+	0	0	0	00000
35	+	+	+	+	+	+	0	0	00000
36	+	+	+	+	+	+	0	00000
37	+	+	+	+	+	+	+	0	00000
38	+	+	+	+	+	+	+	0	00000
39	+	+	+	+	+	+	+	0	00000
40	+	+	+	+	+	+	+	0	00000
41	+	+	+	+	+	+	+	0	00000
42	+	+	+	+	+	+	+	0	00000
43	+	+	+	+	+	+	+	00000
44	+	+	+	+	+	+	+	00000
45	+	+	+	+	+	+	+	00000
46	+	+	+	+	+	+	+	00000
47	+	+	+	+	+	+	+	00000
48	+	+	+	+	+	+	+	00000
49	+	+	+	+	+	+	+	00000
50	+	+	+	+	+	+	+	00000
51	+	+	+	+	+	+	+	00000
52	+	+	+	+	+	+	+	00000
53	+	+	+	+	+	+	+	00000
54	+	+	+	+	+	+	+	00000
55	+	+	+	+	+	00000
56	+	+	+	+	+	0	00000
57	+	+	+	+	0	00000
58	+	+	+	0	00000
59	+	+	0	0	00000
60	+	0	0	00000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	DISTANCE FROM LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.7308E-02	0.0000E+00	1414.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.5657E-02	0.0000E+00	1447.	0.0000E+00	13.50	0.100000E-01
3	3708.	1801.	0.4772E-02	0.0000E+00	1480.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3776E-02	0.0000E+00	1508.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2905E-02	0.0000E+00	1531.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2276E-02	0.0000E+00	1550.	0.0000E+00	13.50	0.100000E-01
7	3707.	1801.	0.1827E-02	0.0000E+00	1566.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1546E-02	0.0000E+00	1579.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1314E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1115E-02	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7127E-01	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.42318E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17259E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.70389E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4957E-03	0.0000E+00	2037.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.3838E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3237E-03	0.0000E+00	2111.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2561E-03	0.0000E+00	2143.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1970E-03	0.0000E+00	2169.	0.0000E+00	13.50	0.100000E-01
6	4780.	1877.	0.1544E-03	0.0000E+00	2191.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.1239E-03	0.0000E+00	2208.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.1049E-03	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.8914E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.7563E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4835E-02	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1351.5

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 562.96

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2623.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 439.38

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2746.6

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1521.	1647.	109.6	0.0000E+00	435.4	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	4.474	0.0000E+00	457.2	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	3.999	0.0000E+00	479.1	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	3.201	0.0000E+00	498.2	0.0000E+00	13.50	0.200000E-02
5	1562.	1650.	2.453	0.0000E+00	513.9	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	1.918	0.0000E+00	526.7	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	1.539	0.0000E+00	537.4	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	1.281	0.0000E+00	546.5	0.0000E+00	13.50	0.200000E-02
9	1561.	1650.	1.097	0.0000E+00	554.5	0.0000E+00	13.50	0.200000E-02
10	1561.	1650.	0.9626	0.0000E+00	561.7	0.0000E+00	13.50	0.200000E-02
11	1420.	1640.	308.8	0.0000E+00	562.9	0.2463	13.25	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 367.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2818.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 307.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2878.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 257.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2928.5

CONCENTRATIONS ABOVE BACKGROUND OF Clay (MG/L) IN THE CLOUD 7200.00 SECONDS AFTER DUMP

0.00 FT BELOW THE WATER SURFACE

Table with 31 columns (M N= 2 to 31) and 31 rows (2 to 57). Row 2 is a long string of zeros. Rows 3-23 show zeros. Row 24 starts with a '+' sign and numerical values. Rows 25-57 contain numerical data points.

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2594. 1723.	64.26	0.0000E+00	875.0	0.0000E+00	13.50	0.200000E-02
2	2636. 1726.	2.622	0.0000E+00	903.0	0.0000E+00	13.50	0.200000E-02
3	2636. 1726.	2.344	0.0000E+00	930.9	0.0000E+00	13.50	0.200000E-02
4	2635. 1726.	1.876	0.0000E+00	955.0	0.0000E+00	13.50	0.200000E-02
5	2635. 1726.	1.438	0.0000E+00	974.8	0.0000E+00	13.50	0.200000E-02
6	2635. 1726.	1.124	0.0000E+00	990.9	0.0000E+00	13.50	0.200000E-02
7	2635. 1726.	0.9021	0.0000E+00	1004.	0.0000E+00	13.50	0.200000E-02
8	2634. 1725.	0.7508	0.0000E+00	1016.	0.0000E+00	13.50	0.200000E-02
9	2634. 1725.	0.6427	0.0000E+00	1026.	0.0000E+00	13.50	0.200000E-02
10	2634. 1725.	0.5642	0.0000E+00	1035.	0.0000E+00	13.50	0.200000E-02
11	2493. 1716.	181.0	0.0000E+00	1036.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 215.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2970.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.34
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3005.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 150.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.1

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3666. 1798.	37.66	0.0000E+00	1414.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	1.537	0.0000E+00	1447.	0.0000E+00	13.50	0.200000E-02
3	3708. 1801.	1.374	0.0000E+00	1480.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	1.099	0.0000E+00	1508.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.8428	0.0000E+00	1531.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.6587	0.0000E+00	1550.	0.0000E+00	13.50	0.200000E-02
7	3707. 1801.	0.5287	0.0000E+00	1566.	0.0000E+00	13.50	0.200000E-02
8	3707. 1801.	0.4401	0.0000E+00	1579.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.3767	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.3307	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
11	3566. 1791.	106.1	0.0000E+00	1603.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.30
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3059.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.70
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3080.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.453
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3096.7

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0	00000
43	.12	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0	00000
44	.15	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0	00000
45	.20	.18	.16	.14	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0	00000
46	.26	.24	.21	.19	.16	.14	.12	.10	.08	.06	.05	.04	0	0	0	0	00000
47	.34	.31	.27	.24	.21	.18	.15	.12	.10	.08	.06	.05	0	0	0	0	00000
48	.42	.38	.34	.30	.26	.23	.19	.16	.13	.10	.08	.06	0	0	0	0	00000
49	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0	00000
50	.64	.58	.52	.46	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	0	00000
51	.78	.70	.63	.55	.48	.41	.35	.29	.24	.19	.15	.12	0	0	0	0	00000
52	.92	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	0	0	0	0	00000
53	1.0	.98	.88	.77	.67	.57	.48	.40	.33	.26	.21	.16	0	0	0	0	00000
54	1.2	1.1	1.0	.89	.77	.66	.56	.46	.38	.31	.24	.19	0	0	0	0	00000
55	1.4	1.2	1.1	1.0	.88	.75	.63	.53	.43	.35	.28	.22	0	0	0	0	00000
56	1.5	1.4	1.2	1.1	.99	.84	.71	.59	.48	.39	.31	.24	0	0	0	0	00000
57	1.7	1.6	1.4	1.2	1.0	.93	.79	.65	.53	.43	.34	.27	0	0	0	0	00000
58	1.9	1.7	1.5	1.3	1.1	1.0	.86	.71	.58	.47	.37	.29	0	0	0	0	00000
59	2.0	1.8	1.6	1.4	1.2	1.0	.92	.76	.62	.50	.40	.31	0	0	0	0	00000
60	2.1	1.9	1.7	1.5	1.3	1.1	.97	.81	.66	.53	.42	.33	0	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	0	0	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	0	0	00000
25	.01	+	+	+	+	+	0	0	0	0	00000
26	.02	.01	+	+	+	+	+	0	0	0	00000
27	.03	.01	+	+	+	+	+	+	00000
28	.04	.01	+	+	+	+	+	+0000
29	.05	.02	.01	+	+	+	+	+	+0000
30	.06	.03	.01	+	+	+	+	+	+0000
31	.07	.03	.02	.01	+	+	+	+	+	+0000
32	.08	.04	.02	.01	+	+	+	+	+	+0000
33	.09	.05	.03	.01	+	+	+	+	+	+	+0000
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM		MASS FROM DISPOSAL	ENTRAINED MASS	CLOUD X-Z DIAMETER	DEPTH OF TOP OF CLOUD	CLOUD VERT. THICKNESS	SOLIDS FALL VELOCITY
	TOP OF GRID	LEFT OF GRID	(CU FT)	(CU FT)	(FT)	(FT)	(FT)	(FPS)
1	4739.	1874.	22.07	0.0000E+00	2037.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.9008	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8050	0.0000E+00	2111.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6444	0.0000E+00	2143.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4939	0.0000E+00	2169.	0.0000E+00	13.50	0.200000E-02
6	4780.	1877.	0.3861	0.0000E+00	2191.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.3099	0.0000E+00	2208.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2579	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2208	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1938	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
11	4639.	1867.	62.17	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with 31 columns (M N= 2 to 31) and 31 rows (3 0000 to 59 0000). The table displays numerical values representing clay accumulation at various grid squares over time. The values generally increase from left to right and bottom to top, with some rows showing '+' signs indicating specific accumulation levels.

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	0	0	0	0	0	0	00000
24	.01	+	+	+	+	+	0	0	0	0	0	00000
25	.01	+	+	+	+	+	0	0	0	0	00000
26	.02	.01	+	+	+	+	+	0	0	0	00000
27	.03	.01	+	+	+	+	+	+	00000
28	.04	.01	+	+	+	+	+	+0000
29	.05	.02	.01	+	+	+	+	+	+0000
30	.06	.03	.01	+	+	+	+	+	+0000
31	.07	.03	.02	.01	+	+	+	+	+	+0000
32	.08	.04	.02	.01	+	+	+	+	+	+0000
33	.09	.05	.03	.01	+	+	+	+	+	+	+0000
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF copper

SUMMARY OF copper DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.7

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.0	1599.	0.1001E+06	0.9458E+05	309.5	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.7

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	0.1799E+06	0.1743E+06	429.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.7

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1561.	1650.	0.3106E+06	0.3051E+06	562.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.7

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	0.4941E+06	0.4886E+06	709.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2276.	1700.	0.7397E+06	0.7342E+06	867.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	0.1057E+07	0.1051E+07	1036.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2992.	1751.	0.1455E+07	0.1449E+07	1215.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3349.	1776.	0.1943E+07	0.1938E+07	1404.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3707.	1801.	0.2532E+07	0.2526E+07	1603.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4064.	1826.	0.3229E+07	0.3224E+07	1810.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5542.8

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4422.	1851.	0.4046E+07	0.4041E+07	2026.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF copper DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 5543.0

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.09	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0	00000
45	.12	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0	00000
46	.16	.15	.13	.12	.10	.09	.07	.06	.05	.04	.03	.02	0	0	0	0	00000
47	.21	.19	.17	.15	.13	.11	.10	.08	.07	.05	.04	.03	0	0	0	0	00000
48	.27	.24	.22	.19	.17	.15	.12	.10	.08	.07	.05	.04	0	0	0	0	00000
49	.34	.31	.28	.25	.21	.18	.16	.13	.11	.09	.07	.05	0	0	0	0	00000
50	.42	.38	.34	.31	.27	.23	.19	.16	.13	.11	.09	.07	0	0	0	0	00000
51	.51	.47	.42	.37	.33	.28	.24	.20	.16	.13	.11	.08	0	0	0	0	00000
52	.62	.56	.51	.45	.39	.34	.29	.24	.20	.16	.13	.10	0	0	0	0	00000
53	.73	.67	.60	.53	.47	.40	.34	.29	.24	.19	.15	.12	0	0	0	0	00000
54	.86	.78	.71	.63	.55	.47	.40	.34	.28	.23	.18	.14	0	0	0	0	00000
55	.99	.90	.81	.72	.63	.55	.46	.39	.32	.26	.21	.17	0	0	0	0	00000
56	1.1	1.0	.93	.82	.72	.62	.53	.44	.37	.30	.24	.19	0	0	0	0	00000
57	1.2	1.1	1.0	.92	.81	.70	.59	.50	.41	.34	.27	.21	0	0	0	0	00000
58	1.4	1.2	1.1	1.0	.90	.77	.66	.55	.46	.37	.30	.24	0	0	0	0	00000
59	1.5	1.4	1.2	1.1	.98	.84	.72	.60	.50	.41	.33	.26	0	0	0	0	00000
60	1.6	1.5	1.3	1.2	1.0	.91	.77	.65	.54	.44	.35	.28	0	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.35	.32	.29	.25	.22	.19	.16	.14	.11	.09	.07	.06	0	0	0	0	00000
45	.47	.43	.38	.34	.30	.26	.22	.18	.15	.12	.10	.08	0	0	0	0	00000
46	.61	.56	.50	.45	.39	.34	.29	.24	.20	.16	.13	.10	0	0	0	0	00000
47	.79	.72	.65	.58	.50	.43	.37	.31	.26	.21	.17	.13	0	0	0	0	00000
48	1.0	.92	.83	.73	.64	.55	.47	.40	.33	.27	.21	.17	0	0	0	0	00000
49	1.2	1.1	1.0	.92	.81	.70	.59	.50	.41	.33	.27	.21	0	0	0	0	00000
50	1.5	1.4	1.2	1.1	1.0	.86	.73	.62	.51	.42	.33	.26	0	0	0	0	00000
51	1.9	1.7	1.5	1.3	1.2	1.0	.90	.75	.62	.51	.41	.32	0	0	0	0	00000
52	2.2	2.1	1.8	1.6	1.4	1.2	1.0	.91	.75	.61	.49	.39	0	0	0	0	00000
53	2.7	2.4	2.2	1.9	1.7	1.5	1.2	1.0	.89	.73	.58	.46	0	0	0	0	00000
54	3.1	2.9	2.6	2.3	2.0	1.7	1.5	1.2	1.0	.85	.68	.54	0	0	0	0	00000
55	3.6	3.3	3.0	2.6	2.3	2.0	1.7	1.4	1.2	.98	.79	.63	0	0	0	0	00000
56	4.1	3.8	3.4	3.0	2.6	2.3	1.9	1.6	1.3	1.1	.90	.71	0	0	0	0	00000
57	4.6	4.2	3.8	3.4	3.0	2.5	2.2	1.8	1.5	1.2	1.0	.80	0	0	0	0	00000
58	5.1	4.7	4.2	3.7	3.3	2.8	2.4	2.0	1.7	1.3	1.1	.89	0	0	0	0	00000
59	5.6	5.1	4.6	4.1	3.6	3.1	2.6	2.2	1.8	1.5	1.2	.97	0	0	0	0	00000
60	6.0	5.5	5.0	4.4	3.9	3.3	2.8	2.4	2.0	1.6	1.3	1.0	0	0	0	0	00000

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	.03	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
34	.04	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	00000
35	.05	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
36	.05	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
37	.05	.03	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	00000
38	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	00000
39	.07	.04	.03	.01	.01	+	+	+	0	0	0	0	0	0	0	0	00000
40	.07	.05	.03	.01	.01	+	+	+	0	0	0	0	0	0	0	0	00000
41	.07	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	00000
42	.07	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	00000
43	.07	.05	.04	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	00000
44	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	00000
45	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	00000
46	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	00000
47	.08	.06	.05	.03	.02	.02	.01	+	+	+	+	+	0	0	0	0	00000
48	.08	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0	00000
49	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0	00000
50	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0	00000
51	.09	.07	.05	.04	.03	.02	.02	.01	+	+	+	+	0	0	0	0	00000
52	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0	00000
53	.08	.07	.05	.04	.03	.03	.02	.01	.01	+	+	+	0	0	0	0	00000
54	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	0	0	0	0	00000
55	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	0	0	0	0	00000
56	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	+	+	0	0	0	0	00000
57	.08	.07	.06	.04	.04	.03	.02	.02	.01	.01	.01	+	0	0	0	0	00000
58	.08	.06	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	0	0	0	0	00000
59	.07	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	0	0	0	0	00000
60	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0	00000

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR copper

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4780.	1877.	0.4991E+07	0.4986E+07	2250.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.259E+00	2625.	1725.
3.00	0.0	0.718E-02	3675.	1800.
4.00	0.0	0.245E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.442E+02	2550.	1725.
3.00	0.0	0.106E+02	3600.	1800.
4.00	0.0	0.312E+01	4650.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR copper

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE		X-LOC (FT)	Z-LOC (FT)
		BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)		
0.33	0.0	0.122E-03	0.270E-02	825.	1575.
0.67	0.0	0.665E-04	0.265E-02	1200.	1650.
1.00	0.0	0.394E-04	0.262E-02	1575.	1650.
1.33	0.0	0.244E-04	0.260E-02	1950.	1650.
1.67	0.0	0.165E-04	0.260E-02	2250.	1725.
2.00	0.0	0.117E-04	0.259E-02	2625.	1725.
2.33	0.0	0.845E-05	0.259E-02	3000.	1725.
2.67	0.0	0.633E-05	0.259E-02	3375.	1800.
3.00	0.0	0.486E-05	0.258E-02	3675.	1800.
3.33	0.0	0.382E-05	0.258E-02	4050.	1800.
3.67	0.0	0.305E-05	0.258E-02	4425.	1875.
4.00	0.0	0.247E-05	0.258E-02	4800.	1875.
0.33	6.8	0.451E-03	0.303E-02	825.	1575.
0.67	6.8	0.246E-03	0.283E-02	1200.	1650.
1.00	6.8	0.146E-03	0.273E-02	1575.	1650.
1.33	6.8	0.902E-04	0.267E-02	1950.	1650.
1.67	6.8	0.609E-04	0.264E-02	2250.	1725.
2.00	6.8	0.431E-04	0.262E-02	2625.	1725.
2.33	6.8	0.312E-04	0.261E-02	3000.	1725.
2.67	6.8	0.234E-04	0.260E-02	3375.	1800.
3.00	6.8	0.180E-04	0.260E-02	3675.	1800.
3.33	6.8	0.141E-04	0.259E-02	4050.	1800.
3.67	6.8	0.113E-04	0.259E-02	4425.	1875.
4.00	6.8	0.914E-05	0.259E-02	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

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0AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3    TIME                SNAPSHOT                ACCUMULATED                3
3    ( SEC )            AREA(SQ FT)    L(FT)    W(FT)    AREA(SQ FT)    L(FT)    W(FT)    3
3
3    1200.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    2400.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    3600.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    4800.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    6000.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    7200.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    8400.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3    9600.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3   10800.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3   12000.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3   13200.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3   14400.0            0.000000E+00    0.        0.        0.000000E+00    0.        0.        3
3
3AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA

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*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.

THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS
DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS
LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT
WIDTH OF BARGE, BARGW = 50. FT
DRAFT OF LOADED BARGE, DREL1 = 12.0 FT
DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF mercury FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF mercury IS 0.214000E-04 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.1610000E-04 MG/L.

THE WATER QUALITY STANDARD FOR mercury IS 0.9400000E-03 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 1 30.31	500.3	1575.	143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 2 30.61	500.2	1575.	159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 3 30.92	500.2	1575.	171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 4 31.23	500.2	1575.	181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 5 31.54	500.2	1575.	189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 6 31.84	500.2	1575.	195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 7 32.15	500.2	1575.	201.6	11.25	0.9467E-01	2.327	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 8 32.46	500.2	1575.	206.7	11.34	0.7957E-01	2.003	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 9 32.77	500.2	1575.	211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 1) = 10 33.07	500.2	1575.	215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(CU FT)	(CU FT)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 1 30.31	500.3	1575.	143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 2 30.61	500.2	1575.	159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 3 30.92	500.2	1575.	171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 4 31.23	500.2	1575.	181.1	10.80	0.1911	7.461	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 5 31.54	500.2	1575.	189.1	10.99	0.1448	5.884	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 6 31.84	500.2	1575.	195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 7 32.15	500.2	1575.	201.6	11.25	0.9467E-01	4.083	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 8 32.46	500.2	1575.	206.7	11.34	0.7957E-01	3.512	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 9 32.77	500.2	1575.	211.1	11.42	0.6810E-01	3.066	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 2) = 10 33.07	500.2	1575.	215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(CU FT)	(CU FT)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 1 30.31	500.3	1575.	143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 2 30.61	500.2	1575.	159.3	10.08	0.4471	6.960	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 3 30.92	500.2	1575.	171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 4 31.23	500.2	1575.	181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 5 31.54	500.2	1575.	189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 6 31.84	500.2	1575.	195.8	11.13	0.1152	2.190	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 7 32.15	500.2	1575.	201.6	11.25	0.9467E-01	1.849	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 8 32.46	500.2	1575.	206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 9 32.77	500.2	1575.	211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 3) = 10 33.07	500.2	1575.	215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 1 30.31	500.3	1575.	143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 2 30.61	500.2	1575.	159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 3 30.92	500.2	1575.	171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 4 31.23	500.2	1575.	181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 5 31.54	500.2	1575.	189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 6 31.84	500.2	1575.	195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 7 32.15	500.2	1575.	201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 8 32.46	500.2	1575.	206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 9 32.77	500.2	1575.	211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 4) = 10 33.07	500.2	1575.	215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)		CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2	1575.	5) = 1 215.1	10.07	3.431	38.59	23.61	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 144.63

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7091.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.868

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7178.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.601

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7212.4

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564. 1650.	3.674	0.0000E+00	466.9	0.0000E+00	13.50	0.100000E-01
2	1564. 1650.	0.9189	0.0000E+00	491.6	0.0000E+00	13.50	0.100000E-01
3	1564. 1650.	0.6027	0.0000E+00	509.9	0.0000E+00	13.50	0.100000E-01
4	1564. 1650.	0.4163	0.0000E+00	524.4	0.0000E+00	13.50	0.100000E-01
5	1564. 1650.	0.3492	0.0000E+00	536.2	0.0000E+00	13.50	0.100000E-01
6	1563. 1650.	0.2863	0.0000E+00	546.1	0.0000E+00	13.50	0.100000E-01
7	1563. 1650.	0.2448	0.0000E+00	554.5	0.0000E+00	13.50	0.100000E-01
8	1563. 1650.	0.2099	0.0000E+00	561.8	0.0000E+00	13.50	0.100000E-01
9	1563. 1650.	0.1815	0.0000E+00	568.2	0.0000E+00	13.50	0.100000E-01
10	1563. 1650.	16.72	0.0000E+00	573.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.6253
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9256
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6010
 TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.4

MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.2492	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2637.	1726.	0.6233E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2637.	1726.	0.4089E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2636.	1726.	0.2824E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2636.	1726.	0.2369E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2636.	1726.	0.1942E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2636.	1726.	0.1660E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2636.	1726.	0.1424E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2636.	1726.	0.1231E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2636.	1726.	1.134	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65294
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26630
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10861
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE), 10800.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

Table with columns M N= 2 to 31 and rows 2 to 59. The table contains numerical data representing silt accumulation, with many values being 0 or small decimals, and some rows showing cumulative sums with '+' signs.

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	0	0	0	0	0	0	0	0	0	0	00000
24	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	0	0	0	0	0	0	0	0	0	00000
26	+	+	+	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	0	0	0	0	0	0	0	0	00000
28	+	+	+	+	0	0	0	0	0	0	0	00000
29	+	+	+	+	0	0	0	0	0	0	0	00000
30	+	+	+	+	+	0	0	0	0	0	0	00000
31	+	+	+	+	+	0	0	0	0	0	0	00000
32	+	+	+	+	+	0	0	0	0	0	00000
33	+	+	+	+	+	+	0	0	0	0	00000
34	+	+	+	+	+	+	0	0	0	00000
35	+	+	+	+	+	+	0	0	00000
36	+	+	+	+	+	+	+	0	00000
37	+	+	+	+	+	+	+	0	00000
38	+	+	+	+	+	+	+	0	00000
39	+	+	+	+	+	+	+	0	00000
40	+	+	+	+	+	+	+	0	00000
41	+	+	+	+	+	+	+	0	00000
42	+	+	+	+	+	+	+	+	00000
43	+	+	+	+	+	+	+	+	00000
44	+	+	+	+	+	+	+	+	00000
45	+	+	+	+	+	+	+	+	00000
46	+	+	+	+	+	+	+	+	00000
47	+	+	+	+	+	+	+	+	00000
48	+	+	+	+	+	+	+	+00000
49	+	+	+	+	+	+	+	+00000
50	+	+	+	+	+	+	+	+00000
51	+	+	+	+	+	+	+	+	00000
52	+	+	+	+	+	+	+	+	00000
53	+	+	+	+	+	+	+	+	00000
54	+	+	+	+	+	+	+	+	00000
55	+	+	+	+	+	00000
56	+	+	+	+	+	00000
57	+	+	+	+	0	00000
58	+	+	+	0	00000
59	+	+	0	00000
60	+	0	0	0	00000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3710. 1801.	0.1691E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	3710. 1801.	0.4229E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	3709. 1801.	0.2774E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	3709. 1801.	0.1916E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	3709. 1801.	0.1607E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	3709. 1801.	0.1317E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	3709. 1801.	0.1126E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	3709. 1801.	0.9658E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	3709. 1801.	0.8352E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	3709. 1801.	0.7693E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44293E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18065E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73674E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM		MASS FROM DISPOSAL	ENTRAINED MASS	CLOUD X-Z DIAMETER	DEPTH OF TOP OF CLOUD	CLOUD VERT. THICKNESS	SOLIDS FALL VELOCITY
	TOP OF GRID	LEFT OF GRID	(CU FT)	(CU FT)	(FT)	(FT)	(FT)	(FPS)
1	4782.	1877.	0.1147E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2869E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	4782.	1877.	0.1882E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	4782.	1877.	0.1300E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	4782.	1877.	0.1090E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	4782.	1877.	0.8937E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	4782.	1877.	0.7641E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	4782.	1877.	0.6552E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	4782.	1877.	0.5666E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	4782.	1877.	0.5219E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1419.2

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1858.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 611.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2665.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 484.33

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2793.5

