

[illegible]

[illegible]

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SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1548.	1649.	134.9	0.0000E+00	466.9	0.0000E+00	0.200000E-02
2	1564.	1650.	4.086	0.0000E+00	491.6	0.0000E+00	0.200000E-02
3	1564.	1650.	2.691	0.0000E+00	509.9	0.0000E+00	0.200000E-02
4	1564.	1650.	1.960	0.0000E+00	524.4	0.0000E+00	0.200000E-02
5	1564.	1650.	1.544	0.0000E+00	536.2	0.0000E+00	0.200000E-02
6	1563.	1650.	1.266	0.0000E+00	546.1	0.0000E+00	0.200000E-02
7	1563.	1650.	1.070	0.0000E+00	554.5	0.0000E+00	0.200000E-02
8	1563.	1650.	0.9198	0.0000E+00	561.8	0.0000E+00	0.200000E-02
9	1563.	1650.	0.8021	0.0000E+00	568.2	0.0000E+00	0.200000E-02
10	1433.	1641.	335.1	0.0000E+00	573.9	0.1115	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 405.31
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2872.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 339.19
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2938.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 283.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2993.9

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7200.00 SECONDS AFTER DUMP

0 = .LT. .0000001)

[illegible]

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2621.	1724.	79.04	0.0000E+00	915.3	0.0000E+00	0.200000E-02
2	2637.	1726.	2.395	0.0000E+00	946.7	0.0000E+00	0.200000E-02
3	2637.	1726.	1.577	0.0000E+00	969.8	0.0000E+00	0.200000E-02
4	2636.	1726.	1.149	0.0000E+00	987.9	0.0000E+00	0.200000E-02
5	2636.	1726.	0.9049	0.0000E+00	1003.	0.0000E+00	0.200000E-02
6	2636.	1726.	0.7418	0.0000E+00	1015.	0.0000E+00	0.200000E-02
7	2636.	1726.	0.6271	0.0000E+00	1026.	0.0000E+00	0.200000E-02
8	2636.	1726.	0.5391	0.0000E+00	1035.	0.0000E+00	0.200000E-02
9	2636.	1726.	0.4701	0.0000E+00	1043.	0.0000E+00	0.200000E-02
10	2505.	1716.	196.4	0.0000E+00	1050.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 237.55
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3040.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 198.79
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3079.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 166.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3111.4

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	.14	.12	.09	.07	.05	.03	.02	0	0	0	0	0	0	0	0	0	0	00000
34	.22	.18	.14															

[illegible]

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

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59 0000 . . + + + + + + + + .01 .01 .02 .02 .02 .03 .03 .04 .04 .04 .04 .03 .03 .03 .02 .02

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M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
32	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
35	.13	.08	.05	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
36	.15	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.17	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	0
39	.17	.12	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.18	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.17	.13	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	0
46	.17	.12	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	0
47	.16	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
49	.13	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
50	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
51	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
52	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	0
53	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
54	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
56	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
57	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	0
58	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	0
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	0
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3694.	1800.	46.32	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	3710.	1801.	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	3709.	1801.	0.9242	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	3709.	1801.	0.6733	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	3709.	1801.	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	3709.	1801.	0.4348	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	3709.	1801.	0.3675	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	3709.	1801.	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	3709.	1801.	0.2755	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	3578.	1792.	115.1	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 139.22
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3138.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 116.51
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3160.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 97.504
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3179.3

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M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.09	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0
43	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
44	.17	.15	.14	.12	.10	.09	.08	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.22	.20	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	.02	0	0	0	0
46	.29	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
47	.36	.33	.30	.26	.23	.20	.17	.14	.11	.09	.07	.06	.04	0	0	0	0
48	.46	.42	.37	.33	.29	.25	.21	.17	.14	.11	.09	.07	.05	0	0	0	0
49	.57	.51	.46	.41	.36	.31	.26	.22	.18	.14	.11	.09	.07	0	0	0	0
50	.69	.63	.56	.50	.43	.37	.32	.26	.22	.17	.14	.11	.08	0	0	0	0
51	.83	.76	.68	.60	.52	.45	.38	.32	.26	.21	.17	.13	.10	0	0	0	0
52	.99	.90	.81	.71	.62	.53	.45	.38	.31	.25	.20	.16	.12	0	0	0	0
53	1.1	1.0	.94	.83	.73	.62	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
54	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.21	.16	0	0	0	0
55	1.5	1.3	1.2	1.0	.95	.82	.69	.58	.48	.39	.31	.24	.19	0	0	0	0
56	1.7	1.5	1.3	1.2	1.0	.92	.78	.65	.53	.43	.34	.27	.21	0	0	0	0
57	1.8	1.7	1.5	1.3	1.1	1.0	.86	.72	.59	.48	.38	.30	.23	0	0	0	0
58	2.0	1.8	1.6	1.4	1.2	1.1	.94	.78	.64	.52	.42	.33	.25	0	0	0	0
59	2.2	2.0	1.8	1.5	1.3	1.1	1.0	.84	.69	.56	.45	.35	.27	0	0	0	0
60	2.3	2.1	1.9	1.6	1.4	1.2	1.0	.89	.73	.59	.47	.37	.29	0	0	0	0

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4767.	1876.	27.15	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.8226	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	4782.	1877.	0.5417	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	4782.	1877.	0.3946	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	4782.	1877.	0.3108	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	4782.	1877.	0.2548	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	4782.	1877.	0.2154	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	4782.	1877.	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	4782.	1877.	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	4651.	1868.	67.47	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF mercury

SUMMARY OF mercury DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	847.9	1600.	639.6	624.6	318.3	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1206.	1625.	1154.	1139.	439.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

M	N=	0.00 FT BELOW THE WATER SURFACE ...MULTIPLY DISPLAYED VALUES BY 0.1000E-06 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)																													
2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000		
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	0		
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	0		
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	+	+	.01	.01	.02	.02	.02	.01	.01	+	+	0		
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	+	.01	.03	.05	.07	.08	.07	.05	.03	.01	+	0		
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	+	+	+	.01	.03	.08	.13	.18	.21	.18	.13	.08	.03	.01	0		
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	+	+	+	.02	.07	.16	.28	.38	.43	.38	.28	.16	.07	.02	0		
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	+	+	.01	.04	.12	.27	.46	.64	.71	.64	.46	.27	.12	.04	0		
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	+	+	.02	.06	.17	.36	.62	.85	.95								

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	1563.	1650.	1993.	1978.	573.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1921.	1675.	3167.	3152.	721.1	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2278.	1700.	4732.	4717.	880.0	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.980

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2636.	1726.	6748.	6733.	1050.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2994.	1751.	9273.	9258.	1230.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3351.	1776.	0.1237E+05	0.1235E+05	1420.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000005 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	3709.	1801.	0.1609E+05	0.1608E+05	1619.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4066.	1826.	0.2050E+05	0.2049E+05	1827.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4424.	1852.	0.2566E+05	0.2564E+05	2043.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 14.979

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.09	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0
45	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
46	.16	.15	.14	.12	.10	.09	.08	.06	.05	.04	.03	.02	.02	0	0	0	0
47	.21	.19	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	.03	0	0	0	0
48	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
49	.34	.31	.28	.25	.22	.19	.16	.13	.11	.09	.07	.06	.04	0	0	0	0
50	.42	.39	.35	.31	.27	.23	.20	.17	.14	.11	.09	.07	.05	0	0	0	0
51	.51	.47	.42	.38	.33	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
52	.62	.56	.51	.45	.40	.34	.29	.25	.20	.17	.13	.10	.08	0	0	0	0
53	.73	.67	.60	.54	.47	.41	.35	.29	.24	.20	.16	.12	.10	0	0	0	0
54	.85	.78	.70	.63	.55	.48	.41	.34	.28	.23	.19	.15	.11	0	0	0	0
55	.98	.90	.81	.72	.63	.55	.47	.39	.33	.27	.21	.17	.13	0	0	0	0
56	1.1	1.0	.92	.82	.72	.62	.53	.45	.37	.30	.24	.19	.15	0	0	0	0
57	1.2	1.1	1.0	.92	.81	.70	.60	.50	.42	.34	.27	.22	.17	0	0	0	0
58	1.3	1.2	1.1	1.0	.89	.77	.66	.55	.46	.38	.30	.24	.19	0	0	0	0
59	1.5	1.3	1.2	1.1	.97	.84	.72	.60	.50	.41	.33	.26	.21	0	0	0	0
60	1.6	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.36	.28	.22	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
39	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
40	.02	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
41	.02	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0
42	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
43	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
44	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
45	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0	0
46	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	0	0	0
47	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
48	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
49	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
50	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
51	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
52	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
53	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
54	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
55	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
56	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
57	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
58	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
59	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0
60	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4782.	1877.	0.3162E+05	0.3161E+05	2268.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
25	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
27	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
28	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
29	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
30	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
31	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0
32	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
33	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
34	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
35	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
36	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
37	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
38	.01	.01	+	+	+	+												

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.263E+00	2625.	1725.
3.00	0.0	0.735E-02	3675.	1800.
4.00	0.0	0.252E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.255E+03	1500.	1650.
2.00	0.0	0.467E+02	2550.	1725.
3.00	0.0	0.114E+02	3600.	1800.
4.00	0.0	0.336E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR mercury

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.312E-06	0.164E-04	825.	1575.
0.67	0.0	0.172E-06	0.163E-04	1200.	1650.
1.00	0.0	0.103E-06	0.162E-04	1575.	1650.
1.33	0.0	0.639E-07	0.162E-04	1950.	1650.
1.67	0.0	0.432E-07	0.161E-04	2250.	1725.
2.00	0.0	0.307E-07	0.161E-04	2625.	1725.
2.33	0.0	0.223E-07	0.161E-04	3000.	1725.
2.67	0.0	0.167E-07	0.161E-04	3375.	1800.
3.00	0.0	0.129E-07	0.161E-04	3675.	1800.
3.33	0.0	0.101E-07	0.161E-04	4050.	1800.
3.67	0.0	0.810E-08	0.161E-04	4425.	1875.
4.00	0.0	0.658E-08	0.161E-04	4800.	1875.
0.33	6.8	0.115E-05	0.173E-04	825.	1575.
0.67	6.8	0.634E-06	0.167E-04	1200.	1650.
1.00	6.8	0.379E-06	0.165E-04	1575.	1650.
1.33	6.8	0.236E-06	0.163E-04	1950.	1650.
1.67	6.8	0.160E-06	0.163E-04	2250.	1725.
2.00	6.8	0.113E-06	0.162E-04	2625.	1725.
2.33	6.8	0.825E-07	0.162E-04	3000.	1725.
2.67	6.8	0.619E-07	0.162E-04	3375.	1800.
3.00	6.8	0.476E-07	0.161E-04	3675.	1800.
3.33	6.8	0.374E-07	0.161E-04	4050.	1800.
3.67	6.8	0.299E-07	0.161E-04	4425.	1875.
4.00	6.8	0.243E-07	0.161E-04	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME		SNAPSHOT		ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF mercury FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF mercury IS 0.210000E-05 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.1610000E-04 MG/L.

THE WATER QUALITY STANDARD FOR mercury IS 0.9400000E-03 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	1) = 197.4	10.91	0.2177	34.30	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	1) = 224.8	11.43	0.1157	20.28	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	1) = 232.3	11.55	0.9997E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	2) = 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	2) = 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	2) = 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	2) = 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	2) = 185.6	10.61	0.2974	8.984	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	2) = 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	2) = 207.6	11.12	0.1689	5.614	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	2) = 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	2) = 224.8	11.43	0.1157	4.102	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	2) = 232.3	11.55	0.9997E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	2) = 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	3) = 113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	3) = 134.8	8.477	1.036	9.913	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	3) = 154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	3) = 171.6	10.18	0.4327	5.259	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	3) = 185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	3) = 197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	3) = 207.6	11.12	0.1689	2.428	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	3) = 216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	3) = 224.8	11.43	0.1157	1.773	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	3) = 232.3	11.55	0.9997E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	3) = 233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	4) = 1 233.4	9.779	3.721	37.91	37.00	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 167.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5902.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.559
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6002.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.553
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6042.0

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	2.333	0.0000E+00	419.0	0.0000E+00	0.100000E-01
2	1563.	1650.	1.539	0.0000E+00	453.4	0.0000E+00	0.100000E-01
3	1563.	1650.	1.101	0.0000E+00	484.4	0.0000E+00	0.100000E-01
4	1563.	1650.	0.7476	0.0000E+00	510.1	0.0000E+00	0.100000E-01
5	1563.	1650.	0.5443	0.0000E+00	531.0	0.0000E+00	0.100000E-01
6	1562.	1650.	0.4158	0.0000E+00	548.3	0.0000E+00	0.100000E-01
7	1562.	1650.	0.3351	0.0000E+00	563.0	0.0000E+00	0.100000E-01
8	1562.	1650.	0.2858	0.0000E+00	576.0	0.0000E+00	0.100000E-01
9	1562.	1650.	0.2452	0.0000E+00	587.6	0.0000E+00	0.100000E-01
10	1562.	1650.	0.2115	0.0000E+00	598.2	0.0000E+00	0.100000E-01
11	1562.	1650.	19.79	0.0000E+00	599.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.237
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6058.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.5829
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6065.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.8691
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.7

[illegible]

[illegible]

[illegible]

15 24 15

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
25	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
28	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0		

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1583	0.0000E+00	853.9	0.0000E+00	0.100000E-01
2	2636.	1726.	0.1044	0.0000E+00	898.1	0.0000E+00	0.100000E-01
3	2636.	1726.	0.7469E-01	0.0000E+00	937.5	0.0000E+00	0.100000E-01
4	2636.	1726.	0.5071E-01	0.0000E+00	970.0	0.0000E+00	0.100000E-01
5	2635.	1726.	0.3693E-01	0.0000E+00	996.2	0.0000E+00	0.100000E-01
6	2635.	1726.	0.2821E-01	0.0000E+00	1018.	0.0000E+00	0.100000E-01
7	2635.	1725.	0.2273E-01	0.0000E+00	1036.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.1939E-01	0.0000E+00	1052.	0.0000E+00	0.100000E-01
9	2635.	1725.	0.1663E-01	0.0000E+00	1067.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1435E-01	0.0000E+00	1080.	0.0000E+00	0.100000E-01
11	2634.	1725.	1.343	0.0000E+00	1082.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76229
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31089
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12679
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
28	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
31	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
32	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
34	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
35	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
36	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	00000
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
55	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
56	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
57	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	00000
58	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	00000
59	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	00000
60	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	00000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.1074E-01	0.0000E+00	1389.	0.0000E+00	0.100000E-01
2	3709.	1801.	0.7081E-02	0.0000E+00	1441.	0.0000E+00	0.100000E-01
3	3709.	1801.	0.5067E-02	0.0000E+00	1487.	0.0000E+00	0.100000E-01
4	3708.	1801.	0.3440E-02	0.0000E+00	1526.	0.0000E+00	0.100000E-01
5	3708.	1801.	0.2505E-02	0.0000E+00	1556.	0.0000E+00	0.100000E-01
6	3708.	1801.	0.1913E-02	0.0000E+00	1582.	0.0000E+00	0.100000E-01
7	3708.	1801.	0.1542E-02	0.0000E+00	1603.	0.0000E+00	0.100000E-01
8	3708.	1801.	0.1315E-02	0.0000E+00	1622.	0.0000E+00	0.100000E-01
9	3707.	1801.	0.1128E-02	0.0000E+00	1638.	0.0000E+00	0.100000E-01
10	3707.	1801.	0.9735E-03	0.0000E+00	1654.	0.0000E+00	0.100000E-01
11	3707.	1801.	0.9109E-01	0.0000E+00	1656.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.51711E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21090E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.86012E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.7283E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.4803E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3437E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2334E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1699E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1298E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1046E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.8922E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7655E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6604E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.6179E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.														

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1232.1

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1392.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 435.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2189.1

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	112.6	0.0000E+00	419.0	0.0000E+00	0.200000E-02
2	1563.	1650.	5.895	0.0000E+00	453.4	0.0000E+00	0.200000E-02
3	1563.	1650.	4.298	0.0000E+00	484.4	0.0000E+00	0.200000E-02
4	1563.	1650.	3.093	0.0000E+00	510.1	0.0000E+00	0.200000E-02
5	1563.	1650.	2.260	0.0000E+00	531.0	0.0000E+00	0.200000E-02
6	1562.	1650.	1.742	0.0000E+00	548.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.388	0.0000E+00	563.0	0.0000E+00	0.200000E-02
8	1562.	1650.	1.183	0.0000E+00	576.0	0.0000E+00	0.200000E-02
9	1562.	1650.	1.025	0.0000E+00	587.6	0.0000E+00	0.200000E-02
10	1562.	1650.	0.9074	0.0000E+00	598.2	0.0000E+00	0.200000E-02
11	1438.	1641.	300.8	0.0000E+00	599.8	0.3251E-01	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 364.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2260.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2319.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 255.11
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2369.3

[illegible]

[illegible]

7200.00 SECONDS AFTER DUMP

0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	66.02	0.0000E+00	853.9	0.0000E+00	0.200000E-02
2	2636.	1726.	3.455	0.0000E+00	898.1	0.0000E+00	0.200000E-02
3	2636.	1726.	2.519	0.0000E+00	937.5	0.0000E+00	0.200000E-02
4	2636.	1726.	1.813	0.0000E+00	970.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.324	0.0000E+00	996.2	0.0000E+00	0.200000E-02
6	2635.	1726.	1.021	0.0000E+00	1018.	0.0000E+00	0.200000E-02
7	2635.	1725.	0.8135	0.0000E+00	1036.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.6936	0.0000E+00	1052.	0.0000E+00	0.200000E-02
9	2635.	1725.	0.6010	0.0000E+00	1067.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5318	0.0000E+00	1080.	0.0000E+00	0.200000E-02
11	2511.	1717.	176.3	0.0000E+00	1082.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2410.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.67
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2445.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2474.9

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.14	.11	.09	.07	.05	.04	.02	0	0	0	0	0	0	0	0	0	0
34		.21	.17	.13	.10	.08	.06	.04	0	0	0	0	0	0	0	0	0	0
35		.31	.25	.20	.15	.12	.08	.06	0	0	0	0	0					

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
40	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.16	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.16	.12	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
54	.06	.04	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
56	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.0000
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	38.69	0.0000E+00	1389.	0.0000E+00	0.200000E-02
2	3709.	1801.	2.025	0.0000E+00	1441.	0.0000E+00	0.200000E-02
3	3709.	1801.	1.476	0.0000E+00	1487.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.062	0.0000E+00	1526.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.7763	0.0000E+00	1556.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.5983	0.0000E+00	1582.	0.0000E+00	0.200000E-02
7	3708.	1801.	0.4768	0.0000E+00	1603.	0.0000E+00	0.200000E-02
8	3708.	1801.	0.4065	0.0000E+00	1622.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3522	0.0000E+00	1638.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3117	0.0000E+00	1654.	0.0000E+00	0.200000E-02
11	3583.	1792.	103.3	0.0000E+00	1656.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 125.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2499.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.71
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2519.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.632
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2535.8

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
43	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.20	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	0
46	.25	.23	.21	.18	.16	.14	.12	.10	.08	.06	.05	.04	.03	0	0	0	0
47	.32	.29	.26	.23	.20	.18	.15	.12	.10	.08	.07	.05	.04	0	0	0	0
48	.40	.37	.33	.29	.26	.22	.19	.16	.13	.10	.08	.07	.05	0	0	0	0
49	.50	.45	.41	.36	.32	.27	.23	.19	.16	.13	.10	.08	.06	0	0	0	0
50	.61	.55	.50	.44	.38	.33	.28	.23	.19	.16	.13	.10	.08	0	0	0	0
51	.73	.66	.60	.53	.46	.40	.34	.28	.23	.19	.15	.12	.09	0	0	0	0
52	.86	.79	.71	.63	.55	.47	.40	.33	.28	.22	.18	.14	.11	0	0	0	0
53	1.0	.92	.83	.73	.64	.55	.47	.39	.32	.26	.21	.17	.13	0	0	0	0
54	1.1	1.0	.96	.85	.74	.63	.54	.45	.37	.30	.24	.19	.15	0	0	0	0
55	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.22	.17	0	0	0	0
56	1.5	1.3	1.2	1.0	.94	.81	.69	.57	.47	.38	.31	.24	.19	0	0	0	0
57	1.6	1.5	1.3	1.2	1.0	.90	.76	.64	.52	.43	.34	.27	.21	0	0	0	0
58	1.8	1.6	1.4	1.3	1.1	.98	.83	.69	.57	.46	.37	.29	.23	0	0	0	0
59	1.9	1.7	1.6	1.4	1.2	1.0	.89	.75	.61	.50	.40	.31	.24	0	0	0	0
60	2.0	1.8	1.7	1.5	1.3	1.1	.95	.79	.65	.53	.42	.33	.26	0	0	0	0

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M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	22.68	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8653	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6227	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2795	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2382	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2064	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	4656.	1868.	60.57	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

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M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF mercury

SUMMARY OF mercury DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90979

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.4	1599.	710.3	709.4	339.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90967

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	1264.	1263.	462.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90967

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1562.	1650.	2160.	2159.	599.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90967

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	3400.	3399.	749.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90967

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2277.	1700.	5043.	5042.	910.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.90967

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	7147.	7146.	1082.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91016

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	9772.	9771.	1264.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91016

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3350.	1776.	0.1298E+05	0.1298E+05	1455.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91016

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF mercury (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-08 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)																																			
M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31					
2	000																																		

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1682E+05	0.1682E+05	1656.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91016

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.2136E+05	0.2136E+05	1865.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91211

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.2666E+05	0.2666E+05	2083.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.91406

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
44	.06	.06	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	00000
45	.08	.07	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	00000
46	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	00000
47	.14	.12	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0	0	0	00000
48	.17	.16	.14	.13	.11	.10	.08	.07	.06	.05	.04	.03	.02	0	0	0	00000
49	.21	.20	.18	.16	.14	.12	.10	.09	.07	.06	.05	.04	.03	0	0	0	00000
50	.26	.24	.22	.19	.17	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	00000
51	.32	.29	.26	.24	.21	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	00000
52	.38	.35	.32	.28	.25	.21	.18	.16	.13	.11	.09	.07	.05	0	0	0	00000
53	.45	.41	.37	.33	.29	.25	.22	.18	.15	.13	.10	.08	.06	0	0	0	00000
54	.52	.48	.43	.39	.34	.30	.25	.21	.18	.15	.12	.09	.07	0	0	0	00000
55	.60	.55	.50	.44	.39	.34	.29	.25	.20	.17	.14	.11	.08	0	0	0	00000
56	.68	.62	.56	.50	.44	.38	.33	.28	.23	.19	.15	.12	.10	0	0	0	00000
57	.75	.69	.63	.56	.49	.43	.37	.31	.26	.21	.17	.14	.11	0	0	0	00000
58	.83	.76	.69	.62	.54	.47	.40	.34	.29	.23	.19	.15	.12	0	0	0	00000
59	.90	.83	.75	.67	.59	.51	.44	.37	.31	.26	.21	.17	.13	0	0	0	00000
60	.97	.89	.80	.72	.63	.55	.47	.40	.33	.27	.22	.18	.14	0	0	0	00000

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.02	.01	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.03	.01	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.04	.02	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.05	.03	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.07	.04	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.08	.04	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
35	.09	.05	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.09	.05	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.09	.06	.04	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0
38	.10	.07	.05	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
39	.12	.08	.05	.02	.02	+	+	+	+	0	0	0	0	0	0	0	0
40	.12	.08	.05	.03	.02	.01	+	+	+	0	0	0	0	0	0	0	0
41	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	0	0	0	0	0	0
42	.12	.09	.06	.04	.03	.01	.01	+	+	+	+	0	0	0	0	0	0
43	.13	.10	.07	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0
44	.14	.10	.08	.05	.04	.02	.01	+	+	+	+	+	+	0	0	0	0
45	.14	.11	.08	.06	.04	.02	.02	.01	+	+	+	+	+	0	0	0	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0
47	.14	.10	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0
48	.13	.11	.09	.07	.05	.04	.02	.01	.01	+	+	+	+	0	0	0	0
49	.14	.11	.09	.07	.05	.04	.03	.02	.01	+	+	+	+	0	0	0	0
50	.14	.12	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	0	0	0	0
51	.14	.12	.09	.07	.05	.04	.03	.02	.02	.01	.01	+	+	0	0	0	0
52	.14	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	0	0	0	0
53	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
54	.13	.11	.10	.08	.06	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
55	.13	.12	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	0	0	0	0
56	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
57	.13	.11	.09	.08	.06	.05	.04	.03	.03	.02	.01	.01	.01	0	0	0	0
58	.12	.11	.09	.08	.07	.05	.04	.04	.03	.02	.01	.01	.01	0	0	0	0
59	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
60	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.3278E+05	0.3278E+05	2310.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21		+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
23		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
25		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
26		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
27		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
28		+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
29		+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
30		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
31		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
32		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
33	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
34	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
35	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
36	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
37	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
38	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.152E+02	1575.	1650.
2.00	0.0	0.299E+00	2625.	1725.
3.00	0.0	0.840E-02	3675.	1800.
4.00	0.0	0.289E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.419E+02	2550.	1725.
3.00	0.0	0.102E+02	3675.	1800.
4.00	0.0	0.302E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR mercury

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.169E-07	0.161E-04	825.	1575.
0.67	0.0	0.942E-08	0.161E-04	1200.	1650.
1.00	0.0	0.570E-08	0.161E-04	1575.	1650.
1.33	0.0	0.360E-08	0.161E-04	1950.	1650.
1.67	0.0	0.246E-08	0.161E-04	2250.	1725.
2.00	0.0	0.176E-08	0.161E-04	2625.	1725.
2.33	0.0	0.128E-08	0.161E-04	3000.	1725.
2.67	0.0	0.968E-09	0.161E-04	3375.	1800.
3.00	0.0	0.748E-09	0.161E-04	3675.	1800.
3.33	0.0	0.590E-09	0.161E-04	4050.	1800.
3.67	0.0	0.474E-09	0.161E-04	4425.	1875.
4.00	0.0	0.387E-09	0.161E-04	4800.	1875.
0.33	6.8	0.623E-07	0.162E-04	825.	1575.
0.67	6.8	0.348E-07	0.161E-04	1200.	1650.
1.00	6.8	0.211E-07	0.161E-04	1575.	1650.
1.33	6.8	0.133E-07	0.161E-04	1950.	1650.
1.67	6.8	0.908E-08	0.161E-04	2250.	1725.
2.00	6.8	0.649E-08	0.161E-04	2625.	1725.
2.33	6.8	0.475E-08	0.161E-04	3000.	1725.
2.67	6.8	0.358E-08	0.161E-04	3375.	1800.
3.00	6.8	0.277E-08	0.161E-04	3675.	1800.
3.33	6.8	0.218E-08	0.161E-04	4050.	1800.
3.67	6.8	0.175E-08	0.161E-04	4425.	1875.
4.00	6.8	0.143E-08	0.161E-04	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME SNAPSHOT ACCUMULATED							
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF mercury FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF mercury IS 0.261000E-03 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.1610000E-04 MG/L.

THE WATER QUALITY STANDARD FOR mercury IS 0.9400000E-03 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	1) = 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	1) = 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	1) = 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	1) = 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	1) = 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	1) = 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	1) = 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	1) = 201.4	11.31	0.1341	8.588	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	1) = 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	1) = 214.3	11.55	0.9280E-01	6.297	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	1) = 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	2) = 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	2) = 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	2) = 144.6	9.538	0.6070	13.14	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	2) = 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	2) = 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	2) = 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	2) = 193.7	11.14	0.1709	4.997	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	2) = 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	2) = 208.2	11.44	0.1096	3.434	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	2) = 214.3	11.55	0.9280E-01	2.986	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	2) = 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0 1575.	3) = 114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7 1575.	3) = 128.4	8.827	0.7117	5.741	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5 1575.	3) = 144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4 1575.	3) = 160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3 1575.	3) = 173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3 1575.	3) = 184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3 1575.	3) = 193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3 1575.	3) = 201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3 1575.	3) = 208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3 1575.	3) = 214.3	11.55	0.9280E-01	1.260	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3 1575.	3) = 214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0 1575.	4) = 1 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7 1575.	4) = 2 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5 1575.	4) = 3 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4 1575.	4) = 4 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3 1575.	4) = 5 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3 1575.	4) = 6 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3 1575.	4) = 7 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3 1575.	4) = 8 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3 1575.	4) = 9 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3 1575.	4) = 10 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3 1575.	4) = 11 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	5) = 1 214.5	10.08	3.420	159.7	23.22	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 128.12

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4904.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 51.587

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4981.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 21.039

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5011.7

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.250	0.0000E+00	420.7	0.0000E+00	13.50
2	1563.	1650.	0.9148	0.0000E+00	443.1	0.0000E+00	13.50
3	1563.	1650.	0.8659	0.0000E+00	468.8	0.0000E+00	13.50
4	1563.	1650.	0.6671	0.0000E+00	492.8	0.0000E+00	13.50
5	1562.	1650.	0.5040	0.0000E+00	512.9	0.0000E+00	13.50
6	1562.	1650.	0.3810	0.0000E+00	529.3	0.0000E+00	13.50
7	1562.	1650.	0.2980	0.0000E+00	542.7	0.0000E+00	13.50
8	1562.	1650.	0.2459	0.0000E+00	554.0	0.0000E+00	13.50
9	1562.	1650.	0.2051	0.0000E+00	563.8	0.0000E+00	13.50
10	1561.	1650.	0.1706	0.0000E+00	572.5	0.0000E+00	13.50
11	1561.	1650.	15.54	0.0000E+00	572.8	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 8.5805
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5024.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.4994
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.4272
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.8483E-01	0.0000E+00	856.1	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.6206E-01	0.0000E+00	884.9	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.5874E-01	0.0000E+00	917.7	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.4525E-01	0.0000E+00	948.2	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.3419E-01	0.0000E+00	973.5	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.2584E-01	0.0000E+00	994.1	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2022E-01	0.0000E+00	1011.	0.0000E+00	13.50	0.100000E-01
8	2635.	1725.	0.1668E-01	0.0000E+00	1025.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1391E-01	0.0000E+00	1037.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1157E-01	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.054	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.58207
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.23739
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.96817E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.5754E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.4210E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.3985E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3070E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2319E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1753E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1371E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1132E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.9436E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.7852E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7149E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.39486E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.16104E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65677E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.3904E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2856E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.2703E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2082E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1573E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1189E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.9304E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.7677E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.6401E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.5326E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4850E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

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[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 938.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1183.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.09

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1694.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 343.50

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1778.7

[illegible]

[illegible]

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[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	96.43	0.0000E+00	420.7	0.0000E+00	0.200000E-02
2	1563.	1650.	3.412	0.0000E+00	443.1	0.0000E+00	0.200000E-02
3	1563.	1650.	3.268	0.0000E+00	468.8	0.0000E+00	0.200000E-02
4	1563.	1650.	2.684	0.0000E+00	492.8	0.0000E+00	0.200000E-02
5	1562.	1650.	2.040	0.0000E+00	512.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.556	0.0000E+00	529.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.188	0.0000E+00	542.7	0.0000E+00	0.200000E-02
8	1562.	1650.	0.9942	0.0000E+00	554.0	0.0000E+00	0.200000E-02
9	1562.	1650.	0.8375	0.0000E+00	563.8	0.0000E+00	0.200000E-02
10	1561.	1650.	0.7256	0.0000E+00	572.5	0.0000E+00	0.200000E-02
11	1435.	1641.	230.4	0.0000E+00	572.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 287.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 240.57
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1881.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 201.32
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1920.9

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
19		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
20		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
21		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
24		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
26	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
27	.02	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
28	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
29	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
30	.03	.01	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
31	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
32	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
33	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
34	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
35	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
36	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
37	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	56.52	0.0000E+00	856.1	0.0000E+00	0.200000E-02
2	2636.	1726.	2.000	0.0000E+00	884.9	0.0000E+00	0.200000E-02
3	2636.	1726.	1.915	0.0000E+00	917.7	0.0000E+00	0.200000E-02
4	2635.	1726.	1.573	0.0000E+00	948.2	0.0000E+00	0.200000E-02
5	2635.	1726.	1.195	0.0000E+00	973.5	0.0000E+00	0.200000E-02
6	2635.	1726.	0.9122	0.0000E+00	994.1	0.0000E+00	0.200000E-02
7	2635.	1726.	0.6960	0.0000E+00	1011.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.5827	0.0000E+00	1025.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.4908	0.0000E+00	1037.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.4253	0.0000E+00	1048.	0.0000E+00	0.200000E-02
11	2508.	1717.	135.0	0.0000E+00	1048.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 168.48
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1953.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1981.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 117.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2004.2

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
28	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
34	.08	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.09	.05	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
37	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
38	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
40	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
41	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
42	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.0000
43	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
44	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
45	.12	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
46	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
47	.11	.08	.06	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
48	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
50	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
51	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
52	.06	.05	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
53	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
54	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
55	.03	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
56	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.0000
57	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.0000
58	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.0000
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	33.12	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.9218	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7006	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5347	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4079	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	3707. 1801.	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.2877	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	3581. 1792.	79.13	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 98.744
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2023.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 82.635
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2039.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 69.155
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2052.3

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0
44	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
45	.15	.13	.12	.10	.09	.08	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
46	.19	.17	.15	.14	.12	.10	.08	.07	.06	.04	.04	.03	.02	0	0	0	0
47	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
48	.31	.28	.25	.22	.19	.16	.14	.11	.09	.07	.06	.05	.03	0	0	0	0
49	.38	.35	.31	.27	.24	.20	.17	.14	.12	.09	.07	.06	.04	0	0	0	0
50	.47	.43	.38	.34	.29	.25	.21	.17	.14	.12	.09	.07	.05	0	0	0	0
51	.57	.52	.46	.41	.35	.30	.25	.21	.17	.14	.11	.09	.07	0	0	0	0
52	.68	.61	.55	.49	.42	.36	.30	.25	.21	.17	.13	.10	.08	0	0	0	0
53	.80	.72	.65	.57	.50	.42	.36	.30	.24	.20	.16	.12	.09	0	0	0	0
54	.93	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	.11	0	0	0	0
55	1.0	.96	.86	.76	.66	.56	.47	.39	.32	.26	.21	.16	.12	0	0	0	0
56	1.1	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
57	1.3	1.2	1.0	.95	.82	.70	.59	.49	.40	.32	.26	.20	.16	0	0	0	0
58	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.36	.28	.22	.17	0	0	0	0
59	1.5	1.4	1.2	1.1	.97	.83	.70	.58	.48	.38	.30	.24	.18	0	0	0	0
60	1.6	1.5	1.3	1.1	1.0	.88	.74	.62	.51	.41	.32	.25	.19	0	0	0	0

[illegible]

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. .0001    0 = .LT. .000001)

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[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	19.41	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.6580	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4106	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.2391	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2002	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1686	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	4654.	1868.	46.38	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.06	.03	.01	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

THICKNESS (FT) OF Clumps ACCUMULATED ON BOTTOM, 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF mercury

SUMMARY OF mercury DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.3	1599.	757.6	621.1	317.4	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	1270.	1134.	438.3	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1561.	1650.	2107.	1971.	572.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	3278.	3141.	719.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	2277.	1700.	4840.	4703.	878.7	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	6852.	6716.	1048.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2992.	1751.	9374.	9237.	1228.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3349.	1776.	0.1246E+05	0.1233E+05	1418.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1618E+05	0.1604E+05	1617.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.2059E+05	0.2045E+05	1825.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.49

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.2574E+05	0.2560E+05	2041.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 136.59

MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.09	.08	.07	.06	.05	.05	.04	.03	.03	.02	.01	.01	.01	0	0	0	0
45	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
46	.15	.14	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
47	.19	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	0
48	.25	.23	.20	.18	.16	.14	.12	.10	.08	.06	.05	.04	.03	0	0	0	0
49	.31	.28	.26	.23	.20	.17	.15	.12	.10	.08	.06	.05	.04	0	0	0	0
50	.39	.35	.32	.28	.25	.21	.18	.15	.13	.10	.08	.06	.05	0	0	0	0
51	.47	.43	.39	.34	.30	.26	.22	.19	.15	.12	.10	.08	.06	0	0	0	0
52	.56	.52	.46	.41	.36	.31	.27	.22	.18	.15	.12	.10	.07	0	0	0	0
53	.67	.61	.55	.49	.43	.37	.32	.27	.22	.18	.14	.11	.09	0	0	0	0
54	.78	.71	.64	.57	.50	.43	.37	.31	.26	.21	.17	.13	.10	0	0	0	0
55	.90	.82	.74	.66	.58	.50	.43	.36	.30	.24	.19	.15	.12	0	0	0	0
56	1.0	.94	.84	.75	.66	.57	.48	.41	.34	.28	.22	.18	.14	0	0	0	0
57	1.1	1.0	.94	.84	.74	.64	.54	.46	.38	.31	.25	.20	.15	0	0	0	0
58	1.2	1.1	1.0	.93	.81	.70	.60	.51	.42	.34	.28	.22	.17	0	0	0	0
59	1.3	1.2	1.1	1.0	.89	.77	.66	.55	.46	.37	.30	.24	.19	0	0	0	0
60	1.4	1.3	1.2	1.0	.95	.83	.70	.59	.49	.40	.32	.26	.20	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
40	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
41	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
42	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0
43	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
44	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
45	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
46	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
47	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
48	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
49	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
50	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
51	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
52	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
53	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
54	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
55	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
56	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
57	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
58	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
59	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
60	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.3170E+05	0.3156E+05	2266.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.122E+02	1575.	1650.
2.00	0.0	0.236E+00	2625.	1725.
3.00	0.0	0.659E-02	3675.	1800.
4.00	0.0	0.226E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.200E+03	1500.	1650.
2.00	0.0	0.346E+02	2550.	1725.
3.00	0.0	0.834E+01	3675.	1800.
4.00	0.0	0.246E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR mercury

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.287E-05	0.190E-04	825.	1575.
0.67	0.0	0.157E-05	0.177E-04	1200.	1650.
1.00	0.0	0.937E-06	0.170E-04	1575.	1650.
1.33	0.0	0.584E-06	0.167E-04	1950.	1650.
1.67	0.0	0.395E-06	0.165E-04	2250.	1725.
2.00	0.0	0.280E-06	0.164E-04	2625.	1725.
2.33	0.0	0.204E-06	0.163E-04	3000.	1725.
2.67	0.0	0.153E-06	0.163E-04	3375.	1800.
3.00	0.0	0.118E-06	0.162E-04	3675.	1800.
3.33	0.0	0.925E-07	0.162E-04	4050.	1800.
3.67	0.0	0.739E-07	0.162E-04	4425.	1875.
4.00	0.0	0.601E-07	0.162E-04	4800.	1875.
0.33	6.8	0.106E-04	0.267E-04	825.	1575.
0.67	6.8	0.581E-05	0.219E-04	1200.	1650.
1.00	6.8	0.346E-05	0.196E-04	1575.	1650.
1.33	6.8	0.216E-05	0.183E-04	1950.	1650.
1.67	6.8	0.146E-05	0.176E-04	2250.	1725.
2.00	6.8	0.104E-05	0.171E-04	2625.	1725.
2.33	6.8	0.753E-06	0.169E-04	3000.	1725.
2.67	6.8	0.565E-06	0.167E-04	3375.	1800.
3.00	6.8	0.435E-06	0.165E-04	3675.	1800.
3.33	6.8	0.342E-06	0.164E-04	4050.	1800.
3.67	6.8	0.273E-06	0.164E-04	4425.	1875.
4.00	6.8	0.222E-06	0.163E-04	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF mercury FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF mercury IS 0.149000E-04 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.1610000E-04 MG/L.

THE WATER QUALITY STANDARD FOR mercury IS 0.9400000E-03 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED	
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	1) = 109.2	1	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	1) = 130.9	2	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	1) = 152.5	3	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	1) = 171.5	4	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	1) = 187.3	5	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	1) = 200.5	6	10.89	0.2393	53.70	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	1) = 211.8	7	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	1) = 221.7	8	11.31	0.1469	35.76	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	1) = 230.7	9	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	1) = 238.9	10	11.58	0.1054	27.19	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	1) = 239.2	11	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	2) = 1 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	2) = 2 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	2) = 3 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	2) = 4 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	2) = 5 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	2) = 6 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	2) = 7 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	2) = 8 221.7	11.31	0.1469	0.4822	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	2) = 9 230.7	11.46	0.1227	0.4153	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	2) = 10 238.9	11.58	0.1054	0.3668	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	2) = 11 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED	
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	3) = 109.2	1	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	3) = 130.9	2	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	3) = 152.5	3	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	3) = 171.5	4	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	3) = 187.3	5	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	3) = 200.5	6	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	3) = 211.8	7	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	3) = 221.7	8	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	3) = 230.7	9	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	3) = 238.9	10	11.58	0.1054	0.1514	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	3) = 239.2	11	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	4) = 1 239.2	9.685	3.815	45.72	41.71	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.411

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 493.19

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 38.912

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 549.69

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 15.870

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 572.73

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.488	0.0000E+00	411.8	0.0000E+00	0.100000E-01
2	1563.	1650.	0.1670	0.0000E+00	447.2	0.0000E+00	0.100000E-01
3	1563.	1650.	0.1244	0.0000E+00	481.0	0.0000E+00	0.100000E-01
4	1563.	1650.	0.8470E-01	0.0000E+00	509.8	0.0000E+00	0.100000E-01
5	1562.	1650.	0.6077E-01	0.0000E+00	533.4	0.0000E+00	0.100000E-01
6	1562.	1650.	0.4553E-01	0.0000E+00	552.7	0.0000E+00	0.100000E-01
7	1562.	1650.	0.3587E-01	0.0000E+00	569.0	0.0000E+00	0.100000E-01
8	1562.	1650.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	0.100000E-01
9	1562.	1650.	0.2516E-01	0.0000E+00	596.0	0.0000E+00	0.100000E-01
10	1562.	1650.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	0.100000E-01
11	1562.	1650.	13.79	0.0000E+00	607.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.4723
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 582.12

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.6397
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.96

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.0766
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.52
MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1009	0.0000E+00	844.6	0.0000E+00	13.50
2	2636.	1726.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	13.50
3	2636.	1726.	0.8436E-02	0.0000E+00	933.3	0.0000E+00	13.50
4	2635.	1726.	0.5746E-02	0.0000E+00	969.7	0.0000E+00	13.50
5	2635.	1726.	0.4122E-02	0.0000E+00	999.2	0.0000E+00	13.50
6	2635.	1726.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	13.50
7	2635.	1725.	0.2433E-02	0.0000E+00	1044.	0.0000E+00	13.50
8	2635.	1725.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	13.50
9	2635.	1725.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	13.50
10	2634.	1725.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	13.50
11	2634.	1725.	0.9353	0.0000E+00	1092.	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.43906
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.16

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17907
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.42

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73030E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.52
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
51	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
52	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
53	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
54	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
56	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
57	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	0
58	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
59	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
60	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.6846E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.7684E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3898E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2796E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2095E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	3708.	1801.	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1004E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.6345E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.29784E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.57

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12147E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.49541E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.59
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4644E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3882E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2644E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1421E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7853E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6808E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4304E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31			
2 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
3 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
4 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
5 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	0	0	0	0	0	0	0			
6 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	.	.	0	0	0	0	0	0			
7 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	+	+	+	+	0	0	0	0	0			
8 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+.03	.10	.17	.16	.08	.02	+	+	.	0	0	0		
9 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.06	.34	1.0	1.6	1.5	.75	.20	.03	+	+	.	0	0		
10 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.03	.33	1.8	5.3	8.7	7.8	3.9	1.0	.16	.01	+	.	0	0		
11 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.10	.97	5.2	16	27	24	11	3.1	.47	.04	+	.	0	0		
12 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.16	1.5	8.3	27	52	44	19	4.9	.76	.06	+	+	.	0	0	
13 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.14	1.3	7.3	23	43	38	17	4.4	.69	.06	+	+	.	0	0		
14 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+.08	.73	3.7	11	18	17	8.1	2.3	.42	.05	+	+	+	0	0		
15 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+.05	.33	1.3	3.7	5.9	5.5	3.1	1.1	.31	.07	.01	+	+	.	0	0	
16 0000	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+.01	.07	.28	.87	1.9	3.1	3.2	2.1	1.0	.38	.11	.02	+	+	.	0	0	
17 0000	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+.01	.08	.31	.91	1.9	3.1	3.3	2.4	1.2	.46	.14	.03	+	+	.	0	0	
18 0000	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+.01	.08	.29	.81	1.7	2.6	2.8	2.0	1.0	.44	.14	.03	+	+	.	0	0	
19 0000	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+.01	.07	.22	.58	1.1	1.7	1.8	1.4	.81	.36	.13	.04	.01	+	+	.	0	0
20 0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+.01	.06																

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.871

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.29

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.710

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 136.65

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 106.35

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	13.35	0.0000E+00	411.8	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	0.5799	0.0000E+00	447.2	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	0.4376	0.0000E+00	481.0	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	0.3164	0.0000E+00	509.8	0.0000E+00	13.50	0.200000E-02
5	1562.	1650.	0.2289	0.0000E+00	533.4	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	0.1739	0.0000E+00	552.7	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	0.1387	0.0000E+00	569.0	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	0.1153	0.0000E+00	583.3	0.0000E+00	13.50	0.200000E-02
9	1562.	1650.	0.9923E-01	0.0000E+00	596.0	0.0000E+00	13.50	0.200000E-02
10	1562.	1650.	0.8740E-01	0.0000E+00	607.5	0.0000E+00	13.50	0.200000E-02
11	1562.	1650.	121.1	0.0000E+00	607.9	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.64

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.702
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 147.30

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.91

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
22	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
25	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
26	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
27	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
28	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
29	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0
30	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
31	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
32	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
33	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
34	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
35	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
36	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
37	.02	.01	+	+	+	+	+	+	.	.	.	.						

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	7.825	0.0000E+00	844.6	0.0000E+00	0.200000E-02
2	2636.	1726.	0.3399	0.0000E+00	890.2	0.0000E+00	0.200000E-02
3	2636.	1726.	0.2564	0.0000E+00	933.3	0.0000E+00	0.200000E-02
4	2635.	1726.	0.1854	0.0000E+00	969.7	0.0000E+00	0.200000E-02
5	2635.	1726.	0.1342	0.0000E+00	999.2	0.0000E+00	0.200000E-02
6	2635.	1726.	0.1019	0.0000E+00	1023.	0.0000E+00	0.200000E-02
7	2635.	1725.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	0.200000E-02
9	2635.	1725.	0.5816E-01	0.0000E+00	1077.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5122E-01	0.0000E+00	1091.	0.0000E+00	0.200000E-02
11	2634.	1725.	70.99	0.0000E+00	1092.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.024
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.91

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 46.940
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 196.06

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]


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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21		+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
25		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
26		+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
28	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
29	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
30	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
31	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
32	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
33	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
34	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
35	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
36	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0
37	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0
38	.05	.03	.02	.01	+	+	+	+										

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	3709.	1801.	4.586	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	3709.	1801.	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	3709.	1801.	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	3708.	1801.	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	3708.	1801.	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	3708.	1801.	0.5973E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	3708.	1801.	0.4763E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	3708.	1801.	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	3707.	1801.	0.3409E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	3707.	1801.	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	3707.	1801.	41.61	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.282
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.69

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.874
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.511
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 215.12

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.03	.03	.03	.02	.02	.02	.01	.01	.01	.01	+	+	+	0	0	0	0
45	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	0	0	0	0
46	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0
47	.08	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
48	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
49	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
50	.16	.14	.13	.11	.10	.09	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
51	.19	.17	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
52	.23	.21	.19	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
53	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	0
54	.32	.29	.26	.23	.20	.18	.15	.13	.10	.08	.07	.05	.04	0	0	0	0
55	.36	.33	.30	.27	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
56	.41	.38	.34	.30	.27	.23	.20	.16	.14	.11	.09	.07	.06	0	0	0	0
57	.46	.42	.38	.34	.30	.26	.22	.18	.15	.13	.10	.08	.06	0	0	0	0
58	.51	.47	.42	.37	.33	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
59	.56	.51	.46	.41	.36	.31	.26	.22	.18	.15	.12	.10	.08	0	0	0	0
60	.60	.55	.49	.44	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0

[illegible]

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	2.688	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1998E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1759E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	4780.	1877.	24.38	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	00000
23	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	00000
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
25	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
26	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	00000
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
28	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	00000
29	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
30	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
31	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
32	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
33	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
34	.05	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
35	.06	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
36	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
37	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
38	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
39	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
40	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
41	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
42	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
43	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
44	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
45	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
46	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+0000
50	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
51	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
52	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
53	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
54	.08	.07	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
55	.08	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
56	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
58	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
59	.06	.05	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
60	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF mercury

SUMMARY OF mercury DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0120

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.4	1599.	741.1	737.1	345.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0121

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	1307.	1303.	470.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0120

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	1562.	1650.	2221.	2217.	607.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0120

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	3482.	3478.	758.0	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2277.	1700.	5150.	5146.	919.5	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2634.	1725.	7282.	7278.	1092.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0107

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	9938.	9934.	1274.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0107

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3350.	1776.	0.1318E+05	0.1317E+05	1466.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1706E+05	0.1705E+05	1667.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.2164E+05	0.2164E+05	1878.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.2699E+05	0.2698E+05	2096.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 4.0117

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.29	.27	.24	.21	.19	.16	.14	.12	.10	.08	.06	.05	.04	0	0	0	0
45	.38	.35	.31	.28	.25	.22	.18	.16	.13	.11	.09	.07	.05	0	0	0	0
46	.49	.45	.41	.36	.32	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
47	.62	.57	.52	.46	.41	.35	.30	.26	.22	.18	.14	.11	.09	0	0	0	0
48	.78	.72	.65	.58	.51	.45	.38	.32	.27	.22	.18	.15	.11	0	0	0	0
49	.97	.89	.80	.72	.63	.55	.47	.40	.34	.28	.23	.18	.14	0	0	0	0
50	1.1	1.0	.98	.88	.78	.68	.58	.49	.41	.34	.28	.22	.18	0	0	0	0
51	1.4	1.3	1.1	1.0	.94	.81	.70	.59	.50	.41	.33	.27	.21	0	0	0	0
52	1.6	1.5	1.4	1.2	1.1	.97	.83	.71	.59	.49	.40	.32	.25	0	0	0	0
53	1.9	1.8	1.6	1.4	1.3	1.1	.98	.83	.70	.57	.47	.38	.30	0	0	0	0
54	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.96	.81	.67	.54	.44	.35	0	0	0	0
55	2.6	2.4	2.2	1.9	1.7	1.5	1.3	1.1	.92	.76	.62	.50	.40	0	0	0	0
56	2.9	2.7	2.4	2.2	1.9	1.7	1.4	1.2	1.0	.86	.70	.57	.45	0	0	0	0
57	3.3	3.0	2.7	2.4	2.1	1.9	1.6	1.3	1.1	.96	.78	.63	.50	0	0	0	0
58	3.6	3.3	3.0	2.7	2.4	2.0	1.8	1.5	1.2	1.0	.86	.69	.55	0	0	0	0
59	3.9	3.6	3.3	2.9	2.6	2.2	1.9	1.6	1.3	1.1	.94	.75	.60	0	0	0	0
60	4.2	3.8	3.5	3.1	2.7	2.4	2.0	1.7	1.4	1.2	1.0	.81	.64	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.01	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.02	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.03	.02	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
35	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.04	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0
40	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0
41	.05	.04	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0
42	.05	.04	.02	.02	.01	+	+	+	+	+	0	0	0	0	0	0	0
43	.05	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0	0	0
44	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0
45	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0
46	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	0	0	0	0
47	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	0	0	0	0
48	.06	.04	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	0
49	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0	0	0	0
50	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0	0	0	0
51	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0	0	0	0
52	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0	0	0	0
53	.05	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	0	0	0	0
54	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	0	0	0	0
55	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	0	0	0	0
56	.06	.05	.04	.03	.03	.02	.01	.01	.01	.01	+	+	+	0	0	0	0
57	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	0
58	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	0
59	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	+	+	0	0	0	0
60	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	.01	+	+	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.3315E+05	0.3315E+05	2323.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....


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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
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[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	.	.	.	.</														

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.819E+01	1575.	1650.
2.00	0.0	0.164E+00	2625.	1725.
3.00	0.0	0.467E-02	3675.	1800.
4.00	0.0	0.162E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.702E+02	1575.	1650.
2.00	0.0	0.122E+02	2625.	1725.
3.00	0.0	0.299E+01	3675.	1800.
4.00	0.0	0.896E+00	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR mercury

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.717E-07	0.162E-04	825.	1575.
0.67	0.0	0.403E-07	0.161E-04	1200.	1650.
1.00	0.0	0.245E-07	0.161E-04	1575.	1650.
1.33	0.0	0.155E-07	0.161E-04	1950.	1650.
1.67	0.0	0.106E-07	0.161E-04	2250.	1725.
2.00	0.0	0.760E-08	0.161E-04	2625.	1725.
2.33	0.0	0.557E-08	0.161E-04	3000.	1725.
2.67	0.0	0.420E-08	0.161E-04	3375.	1800.
3.00	0.0	0.325E-08	0.161E-04	3675.	1800.
3.33	0.0	0.257E-08	0.161E-04	4050.	1800.
3.67	0.0	0.206E-08	0.161E-04	4425.	1875.
4.00	0.0	0.168E-08	0.161E-04	4800.	1875.
0.33	6.8	0.265E-06	0.164E-04	825.	1575.
0.67	6.8	0.149E-06	0.162E-04	1200.	1650.
1.00	6.8	0.904E-07	0.162E-04	1575.	1650.
1.33	6.8	0.573E-07	0.162E-04	1950.	1650.
1.67	6.8	0.392E-07	0.161E-04	2250.	1725.
2.00	6.8	0.281E-07	0.161E-04	2625.	1725.
2.33	6.8	0.206E-07	0.161E-04	3000.	1725.
2.67	6.8	0.155E-07	0.161E-04	3375.	1800.
3.00	6.8	0.120E-07	0.161E-04	3675.	1800.
3.33	6.8	0.949E-08	0.161E-04	4050.	1800.
3.67	6.8	0.762E-08	0.161E-04	4425.	1875.
4.00	6.8	0.621E-08	0.161E-04	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME		SNAPSHOT		ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF mercury FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF mercury IS 0.149000E-04 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.1610000E-04 MG/L.

THE WATER QUALITY STANDARD FOR mercury IS 0.9400000E-03 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.000	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 72.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 235.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	1) = 123.6	9.291	0.6767E-01	140.1	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	1) = 137.3	9.359	0.5698	2.383	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	1) = 151.3	9.929	0.4586	2.134	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	1) = 163.7	10.39	0.3367	1.710	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	1) = 174.2	10.72	0.2440	1.325	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	1) = 182.8	10.97	0.1815	1.038	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	1) = 190.1	11.15	0.1404	0.8352	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	1) = 196.3	11.29	0.1129	0.6941	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	1) = 201.8	11.40	0.9417E-01	0.5948	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	1) = 206.8	11.50	0.8092E-01	0.5234	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	1) = 207.7	10.19	3.312	847.7	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	2) = 1 123.6	9.291	0.6767E-01	1135.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	2) = 2 137.3	9.359	0.5698	19.31	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	2) = 3 151.3	9.929	0.4586	17.29	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	2) = 4 163.7	10.39	0.3367	13.86	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	2) = 5 174.2	10.72	0.2440	10.74	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	2) = 6 182.8	10.97	0.1815	8.406	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	2) = 7 190.1	11.15	0.1404	6.765	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	2) = 8 196.3	11.29	0.1129	5.626	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	2) = 9 201.8	11.40	0.9417E-01	4.820	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	2) = 10 206.8	11.50	0.8092E-01	4.242	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	2) = 11 207.7	10.19	3.312	6869.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0 1575.	3) = 123.6	9.291	0.6767E-01	446.7	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7 1575.	3) = 137.3	9.359	0.5698	7.601	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5 1575.	3) = 151.3	9.929	0.4586	6.806	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4 1575.	3) = 163.7	10.39	0.3367	5.455	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2 1575.	3) = 174.2	10.72	0.2440	4.227	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1 1575.	3) = 182.8	10.97	0.1815	3.309	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1 1575.	3) = 190.1	11.15	0.1404	2.663	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0 1575.	3) = 196.3	11.29	0.1129	2.214	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0 1575.	3) = 201.8	11.40	0.9417E-01	1.897	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0 1575.	3) = 206.8	11.50	0.8092E-01	1.670	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0 1575.	3) = 207.7	10.19	3.312	2703.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	4) = 123.6	13.50	0.1000E-02	3949.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	4) = 137.3	13.50	0.1000E-02	3128.	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	4) = 151.3	13.50	0.1000E-02	2120.	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	4) = 163.7	13.50	0.1000E-02	1343.	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	4) = 174.2	13.50	0.1000E-02	798.7	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	4) = 182.8	13.50	0.1000E-02	450.2	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	4) = 190.1	13.50	0.1000E-02	243.2	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	4) = 196.3	13.50	0.1000E-02	126.9	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	4) = 201.8	13.50	0.1000E-02	64.40	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	4) = 206.8	13.50	0.1000E-02	31.89	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	4) = 207.7	10.19	3.312	29.13	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	5) = 1 207.7	10.19	3.312	31.21	18.79	235	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.31

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7954.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 55.287

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8039.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.548

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8072.0

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36		0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.588	0.0000E+00	435.4	0.0000E+00	0.100000E-01
2	1563.	1650.	1.229	0.0000E+00	457.2	0.0000E+00	0.100000E-01
3	1563.	1650.	1.037	0.0000E+00	479.1	0.0000E+00	0.100000E-01
4	1563.	1650.	0.8205	0.0000E+00	498.2	0.0000E+00	0.100000E-01
5	1562.	1650.	0.6312	0.0000E+00	513.9	0.0000E+00	0.100000E-01
6	1562.	1650.	0.4945	0.0000E+00	526.7	0.0000E+00	0.100000E-01
7	1562.	1650.	0.3970	0.0000E+00	537.4	0.0000E+00	0.100000E-01
8	1562.	1650.	0.3360	0.0000E+00	546.5	0.0000E+00	0.100000E-01
9	1561.	1650.	0.2856	0.0000E+00	554.5	0.0000E+00	0.100000E-01
10	1561.	1650.	0.2423	0.0000E+00	561.7	0.0000E+00	0.100000E-01
11	1561.	1650.	15.49	0.0000E+00	562.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.1960
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.7505
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5296
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.1
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1077	0.0000E+00	875.0	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.8339E-01	0.0000E+00	903.0	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.7035E-01	0.0000E+00	930.9	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.5566E-01	0.0000E+00	955.0	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.4282E-01	0.0000E+00	974.8	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.3355E-01	0.0000E+00	990.9	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2693E-01	0.0000E+00	1004.	0.0000E+00	13.50	0.100000E-01
8	2634.	1725.	0.2279E-01	0.0000E+00	1016.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1937E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1644E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.051	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.62383
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25442
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10376
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
29	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
32	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
56	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
57	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
58	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
60	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.7308E-02	0.0000E+00	1414.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.5657E-02	0.0000E+00	1447.	0.0000E+00	13.50	0.100000E-01
3	3708.	1801.	0.4772E-02	0.0000E+00	1480.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3776E-02	0.0000E+00	1508.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2905E-02	0.0000E+00	1531.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2276E-02	0.0000E+00	1550.	0.0000E+00	13.50	0.100000E-01
7	3707.	1801.	0.1827E-02	0.0000E+00	1566.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1546E-02	0.0000E+00	1579.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1314E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1115E-02	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7127E-01	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.42318E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17259E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.70389E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4957E-03	0.0000E+00	2037.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.3838E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3237E-03	0.0000E+00	2111.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2561E-03	0.0000E+00	2143.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1970E-03	0.0000E+00	2169.	0.0000E+00	13.50	0.100000E-01
6	4780.	1877.	0.1544E-03	0.0000E+00	2191.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.1239E-03	0.0000E+00	2208.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.1049E-03	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.8914E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.7563E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4835E-02	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1351.5

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 562.96

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2623.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 439.38

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2746.6

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1521.	1647.	109.6	0.0000E+00	435.4	0.0000E+00	0.200000E-02
2	1563.	1650.	4.474	0.0000E+00	457.2	0.0000E+00	0.200000E-02
3	1563.	1650.	3.999	0.0000E+00	479.1	0.0000E+00	0.200000E-02
4	1563.	1650.	3.201	0.0000E+00	498.2	0.0000E+00	0.200000E-02
5	1562.	1650.	2.453	0.0000E+00	513.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.918	0.0000E+00	526.7	0.0000E+00	0.200000E-02
7	1562.	1650.	1.539	0.0000E+00	537.4	0.0000E+00	0.200000E-02
8	1562.	1650.	1.281	0.0000E+00	546.5	0.0000E+00	0.200000E-02
9	1561.	1650.	1.097	0.0000E+00	554.5	0.0000E+00	0.200000E-02
10	1561.	1650.	0.9626	0.0000E+00	561.7	0.0000E+00	0.200000E-02
11	1420.	1640.	308.8	0.0000E+00	562.9	0.2463	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 367.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2818.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 307.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2878.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 257.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2928.5

[illegible]

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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$$0 = .LT. .000001)$$
[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
24	.01	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
25	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0000
26	.02	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0000
27	.02	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0000
28	.03	.01	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0000
29	.04	.02	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0000
30	.05	.02	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
31	.05	.02	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
32	.06	.03	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
33	.06	.03	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
34	.06	.03	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
35	.05	.03	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
36	.05	.02	.01	+	+													

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2594.	1723.	64.26	0.0000E+00	875.0	0.0000E+00	0.200000E-02
2	2636.	1726.	2.622	0.0000E+00	903.0	0.0000E+00	0.200000E-02
3	2636.	1726.	2.344	0.0000E+00	930.9	0.0000E+00	0.200000E-02
4	2635.	1726.	1.876	0.0000E+00	955.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.438	0.0000E+00	974.8	0.0000E+00	0.200000E-02
6	2635.	1726.	1.124	0.0000E+00	990.9	0.0000E+00	0.200000E-02
7	2635.	1726.	0.9021	0.0000E+00	1004.	0.0000E+00	0.200000E-02
8	2634.	1725.	0.7508	0.0000E+00	1016.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.6427	0.0000E+00	1026.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5642	0.0000E+00	1035.	0.0000E+00	0.200000E-02
11	2493.	1716.	181.0	0.0000E+00	1036.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 215.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2970.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.34
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3005.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 150.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.1

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.13	.11	.08	.06	.04	.03	.02	0	0	0	0	0	0	0	0	0	0
34		.20	.16	.13	.10	.07	.05	.03	0	0	0	0	0	0	0	0	0	0
35		.31	.25	.19	.15	.11	.08	.05	0	0	0	0	0					

[illegible]

0 = .LT. .0000001)

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.
30	.06	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.
38	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.
39	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.
40	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+
41	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+
42	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+
43	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+
44	.16	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
45	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
46	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
47	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
48	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
49	.11	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+
50	.10	.08	.06	.04	.03	.02	.01	.	+	+	+	+	+	+	+	+	+
51	.09	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+
52	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+
53	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+
54	.05	.04	.03	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	+
55	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+
56	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+
57	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	+	+	+
58	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3666.	1798.	37.66	0.0000E+00	1414.	0.0000E+00	0.200000E-02
2	3709.	1801.	1.537	0.0000E+00	1447.	0.0000E+00	0.200000E-02
3	3708.	1801.	1.374	0.0000E+00	1480.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.099	0.0000E+00	1508.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.8428	0.0000E+00	1531.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.6587	0.0000E+00	1550.	0.0000E+00	0.200000E-02
7	3707.	1801.	0.5287	0.0000E+00	1566.	0.0000E+00	0.200000E-02
8	3707.	1801.	0.4401	0.0000E+00	1579.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3767	0.0000E+00	1591.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3307	0.0000E+00	1601.	0.0000E+00	0.200000E-02
11	3566.	1791.	106.1	0.0000E+00	1603.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.30
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3059.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3080.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.453
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3096.7

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0	0
43	.12	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0	0
45	.20	.18	.16	.14	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0	0
46	.26	.24	.21	.19	.16	.14	.12	.10	.08	.06	.05	.04	0	0	0	0	0
47	.34	.31	.27	.24	.21	.18	.15	.12	.10	.08	.06	.05	0	0	0	0	0
48	.42	.38	.34	.30	.26	.23	.19	.16	.13	.10	.08	.06	0	0	0	0	0
49	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0	0
50	.64	.58	.52	.46	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	0	0
51	.78	.70	.63	.55	.48	.41	.35	.29	.24	.19	.15	.12	0	0	0	0	0
52	.92	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	0	0	0	0	0
53	1.0	.98	.88	.77	.67	.57	.48	.40	.33	.26	.21	.16	0	0	0	0	0
54	1.2	1.1	1.0	.89	.77	.66	.56	.46	.38	.31	.24	.19	0	0	0	0	0
55	1.4	1.2	1.1	1.0	.88	.75	.63	.53	.43	.35	.28	.22	0	0	0	0	0
56	1.5	1.4	1.2	1.1	.99	.84	.71	.59	.48	.39	.31	.24	0	0	0	0	0
57	1.7	1.6	1.4	1.2	1.0	.93	.79	.65	.53	.43	.34	.27	0	0	0	0	0
58	1.9	1.7	1.5	1.3	1.1	1.0	.86	.71	.58	.47	.37	.29	0	0	0	0	0
59	2.0	1.8	1.6	1.4	1.2	1.0	.92	.76	.62	.50	.40	.31	0	0	0	0	0
60	2.1	1.9	1.7	1.5	1.3	1.1	.97	.81	.66	.53	.42	.33	0	0	0	0	0

[illegible]

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[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4739.	1874.	22.07	0.0000E+00	2037.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.9008	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8050	0.0000E+00	2111.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6444	0.0000E+00	2143.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4939	0.0000E+00	2169.	0.0000E+00	13.50	0.200000E-02
6	4780.	1877.	0.3861	0.0000E+00	2191.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.3099	0.0000E+00	2208.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2579	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2208	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1938	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
11	4639.	1867.	62.17	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF mercury

SUMMARY OF mercury DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.419

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.0	1599.	602.6	590.2	309.5	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.419

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	1100.	1088.	429.3	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1561.	1650.	1916.	1904.	562.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	3061.	3049.	709.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2276.	1700.	4594.	4582.	867.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	6573.	6560.	1036.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2992.	1751.	9057.	9044.	1215.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.425

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3349.	1776.	0.1210E+05	0.1209E+05	1404.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.424

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000004 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1578E+05	0.1576E+05	1603.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.424

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	DISTANCE FROM TOP OF GRID	LEFT OF GRID						
1	4064.	1826.	0.2013E+05	0.2012E+05	1810.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.424

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.2523E+05	0.2521E+05	2026.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF mercury DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 12.424

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.07	.07	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0	0
45	.10	.09	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	0	0	0	0	0
46	.13	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0	0
47	.17	.16	.14	.13	.11	.09	.08	.07	.05	.04	.03	.03	0	0	0	0	0
48	.22	.20	.18	.16	.14	.12	.10	.08	.07	.06	.04	.03	0	0	0	0	0
49	.28	.25	.23	.20	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	0	0
50	.35	.32	.28	.25	.22	.19	.16	.13	.11	.09	.07	.06	0	0	0	0	0
51	.42	.39	.35	.31	.27	.23	.20	.16	.14	.11	.09	.07	0	0	0	0	0
52	.51	.47	.42	.37	.33	.28	.24	.20	.16	.13	.11	.08	0	0	0	0	0
53	.61	.55	.50	.44	.39	.33	.28	.24	.20	.16	.13	.10	0	0	0	0	0
54	.71	.65	.58	.52	.45	.39	.33	.28	.23	.19	.15	.12	0	0	0	0	0
55	.82	.75	.67	.60	.52	.45	.38	.32	.27	.22	.17	.14	0	0	0	0	0
56	.93	.85	.77	.68	.60	.51	.44	.37	.30	.25	.20	.16	0	0	0	0	0
57	1.0	.96	.86	.76	.67	.58	.49	.41	.34	.28	.22	.18	0	0	0	0	0
58	1.1	1.0	.95	.85	.74	.64	.54	.46	.38	.31	.25	.19	0	0	0	0	0
59	1.2	1.1	1.0	.92	.81	.70	.59	.50	.41	.34	.27	.21	0	0	0	0	0
60	1.3	1.2	1.1	.99	.87	.75	.64	.54	.44	.36	.29	.23	0	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
39	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
40	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
41	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
42	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
43	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
44	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0
45	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
46	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
47	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
48	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
49	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
50	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
51	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
52	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
53	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
54	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
55	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
56	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
57	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
58	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
59	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
60	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR mercury

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.3113E+05	0.3111E+05	2250.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.259E+00	2625.	1725.
3.00	0.0	0.718E-02	3675.	1800.
4.00	0.0	0.245E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.442E+02	2550.	1725.
3.00	0.0	0.106E+02	3600.	1800.
4.00	0.0	0.312E+01	4650.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR mercury

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.274E-06	0.164E-04	825.	1575.
0.67	0.0	0.149E-06	0.162E-04	1200.	1650.
1.00	0.0	0.883E-07	0.162E-04	1575.	1650.
1.33	0.0	0.547E-07	0.162E-04	1950.	1650.
1.67	0.0	0.369E-07	0.161E-04	2250.	1725.
2.00	0.0	0.261E-07	0.161E-04	2625.	1725.
2.33	0.0	0.190E-07	0.161E-04	3000.	1725.
2.67	0.0	0.142E-07	0.161E-04	3375.	1800.
3.00	0.0	0.109E-07	0.161E-04	3675.	1800.
3.33	0.0	0.855E-08	0.161E-04	4050.	1800.
3.67	0.0	0.683E-08	0.161E-04	4425.	1875.
4.00	0.0	0.554E-08	0.161E-04	4800.	1875.
0.33	6.8	0.101E-05	0.171E-04	825.	1575.
0.67	6.8	0.550E-06	0.167E-04	1200.	1650.
1.00	6.8	0.326E-06	0.164E-04	1575.	1650.
1.33	6.8	0.202E-06	0.163E-04	1950.	1650.
1.67	6.8	0.136E-06	0.162E-04	2250.	1725.
2.00	6.8	0.966E-07	0.162E-04	2625.	1725.
2.33	6.8	0.700E-07	0.162E-04	3000.	1725.
2.67	6.8	0.524E-07	0.162E-04	3375.	1800.
3.00	6.8	0.403E-07	0.161E-04	3675.	1800.
3.33	6.8	0.316E-07	0.161E-04	4050.	1800.
3.67	6.8	0.253E-07	0.161E-04	4425.	1875.
4.00	6.8	0.205E-07	0.161E-04	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF PCBs FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF PCBs IS 0.218000E-05 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.6500000E-05 MG/L.

THE WATER QUALITY STANDARD FOR PCBs IS 0.3000000E-04 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	1) = 1 143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	1) = 2 159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	1) = 3 171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	1) = 4 181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	1) = 5 189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	1) = 6 195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	1) = 7 201.6	11.25	0.9467E-01	2.327	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	1) = 8 206.7	11.34	0.7957E-01	2.003	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	1) = 9 211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	1) = 10 215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	2) = 1 143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	2) = 2 159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	2) = 3 171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	2) = 4 181.1	10.80	0.1911	7.461	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	2) = 5 189.1	10.99	0.1448	5.884	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	2) = 6 195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	2) = 7 201.6	11.25	0.9467E-01	4.083	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	2) = 8 206.7	11.34	0.7957E-01	3.512	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	2) = 9 211.1	11.42	0.6810E-01	3.066	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	2) = 10 215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	3) = 143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	3) = 159.3	10.08	0.4471	6.960	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	3) = 171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	3) = 181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	3) = 189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	3) = 195.8	11.13	0.1152	2.190	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	3) = 201.6	11.25	0.9467E-01	1.849	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	3) = 206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	3) = 211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	3) = 215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	4) = 1 143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	4) = 2 159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	4) = 3 171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	4) = 4 181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	4) = 5 189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	4) = 6 195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	4) = 7 201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	4) = 8 206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	4) = 9 211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	4) = 10 215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2	1575.	5) = 1 215.1	10.07	3.431	11.06	9.532	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 144.63

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7091.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.868

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7178.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.601

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7212.4

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	3.674	0.0000E+00	466.9	0.0000E+00	13.50
2	1564.	1650.	0.9189	0.0000E+00	491.6	0.0000E+00	13.50
3	1564.	1650.	0.6027	0.0000E+00	509.9	0.0000E+00	13.50
4	1564.	1650.	0.4163	0.0000E+00	524.4	0.0000E+00	13.50
5	1564.	1650.	0.3492	0.0000E+00	536.2	0.0000E+00	13.50
6	1563.	1650.	0.2863	0.0000E+00	546.1	0.0000E+00	13.50
7	1563.	1650.	0.2448	0.0000E+00	554.5	0.0000E+00	13.50
8	1563.	1650.	0.2099	0.0000E+00	561.8	0.0000E+00	13.50
9	1563.	1650.	0.1815	0.0000E+00	568.2	0.0000E+00	13.50
10	1563.	1650.	16.72	0.0000E+00	573.9	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.6253
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9256
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6010
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.4
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 7200.00 SECONDS AFTER DUMP

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...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
26	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
28	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
29	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
30	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
31	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
32	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
33	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
34	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
35	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
36	+	+	+	+	+	.	.	.	.	.								

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637. 1726.	0.2492	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2637. 1726.	0.6233E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2637. 1726.	0.4089E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2636. 1726.	0.2824E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2636. 1726.	0.2369E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2636. 1726.	0.1942E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2636. 1726.	0.1660E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2636. 1726.	0.1424E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2636. 1726.	0.1231E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2636. 1726.	1.134	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65294
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26630
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10861
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
32	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
56	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
57	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
58	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	0
59	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
60	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3710.	1801.	0.1691E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	3710.	1801.	0.4229E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.2774E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	3709.	1801.	0.1916E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	3709.	1801.	0.1607E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	3709.	1801.	0.1317E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	3709.	1801.	0.1126E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	3709.	1801.	0.9658E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	3709.	1801.	0.8352E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	3709.	1801.	0.7693E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44293E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18065E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73674E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.1147E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2869E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	4782.	1877.	0.1882E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	4782.	1877.	0.1300E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	4782.	1877.	0.1090E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	4782.	1877.	0.8937E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	4782.	1877.	0.7641E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	4782.	1877.	0.6552E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	4782.	1877.	0.5666E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	4782.	1877.	0.5219E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1419.2

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1858.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 611.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2665.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 484.33

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2793.5

[illegible]

[illegible]

[illegible]

BOTTOM ACCUMULATION OF Clay (CU FT/GRID SQUARE) , 3600.00 SECONDS AFTER DUMP

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...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1548.	1649.	134.9	0.0000E+00	466.9	0.0000E+00	0.200000E-02
2	1564.	1650.	4.086	0.0000E+00	491.6	0.0000E+00	0.200000E-02
3	1564.	1650.	2.691	0.0000E+00	509.9	0.0000E+00	0.200000E-02
4	1564.	1650.	1.960	0.0000E+00	524.4	0.0000E+00	0.200000E-02
5	1564.	1650.	1.544	0.0000E+00	536.2	0.0000E+00	0.200000E-02
6	1563.	1650.	1.266	0.0000E+00	546.1	0.0000E+00	0.200000E-02
7	1563.	1650.	1.070	0.0000E+00	554.5	0.0000E+00	0.200000E-02
8	1563.	1650.	0.9198	0.0000E+00	561.8	0.0000E+00	0.200000E-02
9	1563.	1650.	0.8021	0.0000E+00	568.2	0.0000E+00	0.200000E-02
10	1433.	1641.	335.1	0.0000E+00	573.9	0.1115	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 405.31
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2872.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 339.19
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2938.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 283.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2993.9

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2621.	1724.	79.04	0.0000E+00	915.3	0.0000E+00	0.200000E-02
2	2637.	1726.	2.395	0.0000E+00	946.7	0.0000E+00	0.200000E-02
3	2637.	1726.	1.577	0.0000E+00	969.8	0.0000E+00	0.200000E-02
4	2636.	1726.	1.149	0.0000E+00	987.9	0.0000E+00	0.200000E-02
5	2636.	1726.	0.9049	0.0000E+00	1003.	0.0000E+00	0.200000E-02
6	2636.	1726.	0.7418	0.0000E+00	1015.	0.0000E+00	0.200000E-02
7	2636.	1726.	0.6271	0.0000E+00	1026.	0.0000E+00	0.200000E-02
8	2636.	1726.	0.5391	0.0000E+00	1035.	0.0000E+00	0.200000E-02
9	2636.	1726.	0.4701	0.0000E+00	1043.	0.0000E+00	0.200000E-02
10	2505.	1716.	196.4	0.0000E+00	1050.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 237.55
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3040.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 198.79
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3079.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 166.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3111.4

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.14	.12	.09	.07	.05	.03	.02	0	0	0	0	0	0	0	0	0	0
34		.22	.18	.14	.11	.08	.06	.04	0	0	0	0	0	0	0	0	0	0
35		.33	.27	.21	.16	.12	.09	.06	0	0	0	0	0					

[illegible]

(CU FT/GRID SQUARE) , 10800.00 SECONDS AFTER DUMP

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.07	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.09	.05	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	0
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.13	.08	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.15	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	0
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.17	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	0
39	.17	.12	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.18	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.17	.13	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	0
46	.17	.12	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	0
47	.16	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
49	.13	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
50	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
51	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
52	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	0
53	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
54	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
56	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
57	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	0
58	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	0
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	0
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3694.	1800.	46.32	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	3710.	1801.	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	3709.	1801.	0.9242	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	3709.	1801.	0.6733	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	3709.	1801.	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	3709.	1801.	0.4348	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	3709.	1801.	0.3675	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	3709.	1801.	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	3709.	1801.	0.2755	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	3578.	1792.	115.1	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 139.22
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3138.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 116.51
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3160.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 97.504
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3179.3

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.09	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0
43	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
44	.17	.15	.14	.12	.10	.09	.08	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.22	.20	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	.02	0	0	0	0
46	.29	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
47	.36	.33	.30	.26	.23	.20	.17	.14	.11	.09	.07	.06	.04	0	0	0	0
48	.46	.42	.37	.33	.29	.25	.21	.17	.14	.11	.09	.07	.05	0	0	0	0
49	.57	.51	.46	.41	.36	.31	.26	.22	.18	.14	.11	.09	.07	0	0	0	0
50	.69	.63	.56	.50	.43	.37	.32	.26	.22	.17	.14	.11	.08	0	0	0	0
51	.83	.76	.68	.60	.52	.45	.38	.32	.26	.21	.17	.13	.10	0	0	0	0
52	.99	.90	.81	.71	.62	.53	.45	.38	.31	.25	.20	.16	.12	0	0	0	0
53	1.1	1.0	.94	.83	.73	.62	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
54	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.21	.16	0	0	0	0
55	1.5	1.3	1.2	1.0	.95	.82	.69	.58	.48	.39	.31	.24	.19	0	0	0	0
56	1.7	1.5	1.3	1.2	1.0	.92	.78	.65	.53	.43	.34	.27	.21	0	0	0	0
57	1.8	1.7	1.5	1.3	1.1	1.0	.86	.72	.59	.48	.38	.30	.23	0	0	0	0
58	2.0	1.8	1.6	1.4	1.2	1.1	.94	.78	.64	.52	.42	.33	.25	0	0	0	0
59	2.2	2.0	1.8	1.5	1.3	1.1	1.0	.84	.69	.56	.45	.35	.27	0	0	0	0
60	2.3	2.1	1.9	1.6	1.4	1.2	1.0	.89	.73	.59	.47	.37	.29	0	0	0	0

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4767.	1876.	27.15	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.8226	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	4782.	1877.	0.5417	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	4782.	1877.	0.3946	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	4782.	1877.	0.3108	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	4782.	1877.	0.2548	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	4782.	1877.	0.2154	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	4782.	1877.	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	4782.	1877.	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	4651.	1868.	67.47	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02

```
001    0 = .LT. .0000001)
```

[illegible][illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

(LEGEND... + = .LT. .01 . = .LT. .00001 0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF PCBs

SUMMARY OF PCBs DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5254

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	847.9	1600.	253.7	252.2	318.3	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5254

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1206.	1625.	461.2	459.7	439.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5254

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000004 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1563.	1650.	800.2	798.7	573.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5254

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1921.	1675.	1274.	1272.	721.1	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5254

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2278.	1700.	1906.	1904.	880.0	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5256

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2636.	1726.	2720.	2718.	1050.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5134

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2994.	1751.	3739.	3738.	1230.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5132

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3351.	1776.	4989.	4987.	1420.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5137

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3709.	1801.	6492.	6490.	1619.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5137

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4066.	1826.	8272.	8271.	1827.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5137

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4424.	1852.	0.1035E+05	0.1035E+05	2043.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.5137

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.09	.09	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0
45	.13	.12	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
46	.17	.15	.14	.12	.11	.09	.08	.06	.05	.04	.03	.03	.02	0	0	0	0
47	.22	.20	.18	.16	.14	.12	.10	.08	.07	.06	.04	.03	.03	0	0	0	0
48	.27	.25	.23	.20	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
49	.34	.31	.28	.25	.22	.19	.16	.14	.11	.09	.07	.06	.04	0	0	0	0
50	.43	.39	.35	.31	.27	.24	.20	.17	.14	.11	.09	.07	.05	0	0	0	0
51	.52	.47	.43	.38	.33	.29	.25	.21	.17	.14	.11	.09	.07	0	0	0	0
52	.62	.57	.51	.46	.40	.35	.29	.25	.20	.17	.13	.11	.08	0	0	0	0
53	.74	.68	.61	.54	.47	.41	.35	.29	.24	.20	.16	.13	.10	0	0	0	0
54	.86	.79	.71	.63	.56	.48	.41	.34	.29	.23	.19	.15	.12	0	0	0	0
55	1.0	.91	.82	.73	.64	.55	.47	.40	.33	.27	.22	.17	.13	0	0	0	0
56	1.1	1.0	.93	.83	.73	.63	.54	.45	.37	.31	.25	.20	.15	0	0	0	0
57	1.2	1.1	1.0	.93	.82	.71	.60	.51	.42	.34	.28	.22	.17	0	0	0	0
58	1.4	1.2	1.1	1.0	.90	.78	.67	.56	.46	.38	.31	.24	.19	0	0	0	0
59	1.5	1.4	1.2	1.1	.98	.85	.73	.61	.51	.41	.33	.27	.21	0	0	0	0
60	1.6	1.5	1.3	1.2	1.0	.91	.78	.66	.54	.45	.36	.29	.22	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
39	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
40	.02	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
41	.02	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0
42	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
43	.02	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0
44	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
45	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0	0
46	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	0	0	0
47	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
48	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
49	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
50	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
51	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0
52	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
53	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
54	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
55	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
56	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
57	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
58	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0
59	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0
60	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4782.	1877.	0.1276E+05	0.1276E+05	2268.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

(LEGEND... + = .LT. .01 = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
25	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
27	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
28	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
29	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
30	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
31	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0
32	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
33	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
34	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
35	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
36	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
37	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
38	.01	.01	+	+	+	+												

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.263E+00	2625.	1725.
3.00	0.0	0.735E-02	3675.	1800.
4.00	0.0	0.252E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.255E+03	1500.	1650.
2.00	0.0	0.467E+02	2550.	1725.
3.00	0.0	0.114E+02	3600.	1800.
4.00	0.0	0.336E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR PCBs

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.317E-07	0.653E-05	825.	1575.
0.67	0.0	0.175E-07	0.652E-05	1200.	1650.
1.00	0.0	0.104E-07	0.651E-05	1575.	1650.
1.33	0.0	0.651E-08	0.651E-05	1950.	1650.
1.67	0.0	0.440E-08	0.650E-05	2250.	1725.
2.00	0.0	0.313E-08	0.650E-05	2625.	1725.
2.33	0.0	0.225E-08	0.650E-05	3000.	1725.
2.67	0.0	0.169E-08	0.650E-05	3375.	1800.
3.00	0.0	0.130E-08	0.650E-05	3675.	1800.
3.33	0.0	0.102E-08	0.650E-05	4050.	1800.
3.67	0.0	0.819E-09	0.650E-05	4425.	1875.
4.00	0.0	0.665E-09	0.650E-05	4800.	1875.
0.33	6.8	0.117E-06	0.662E-05	825.	1575.
0.67	6.8	0.646E-07	0.656E-05	1200.	1650.
1.00	6.8	0.386E-07	0.654E-05	1575.	1650.
1.33	6.8	0.241E-07	0.652E-05	1950.	1650.
1.67	6.8	0.163E-07	0.652E-05	2250.	1725.
2.00	6.8	0.116E-07	0.651E-05	2625.	1725.
2.33	6.8	0.833E-08	0.651E-05	3000.	1725.
2.67	6.8	0.625E-08	0.651E-05	3375.	1800.
3.00	6.8	0.481E-08	0.650E-05	3675.	1800.
3.33	6.8	0.378E-08	0.650E-05	4050.	1800.
3.67	6.8	0.303E-08	0.650E-05	4425.	1875.
4.00	6.8	0.246E-08	0.650E-05	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF PCBs FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF PCBs IS 0.261000E-05 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.6500000E-05 MG/L.

THE WATER QUALITY STANDARD FOR PCBs IS 0.3000000E-04 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	1) = 197.4	10.91	0.2177	34.30	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	1) = 224.8	11.43	0.1157	20.28	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	1) = 232.3	11.55	0.9997E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	2) = 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	2) = 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	2) = 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	2) = 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	2) = 185.6	10.61	0.2974	8.984	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	2) = 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	2) = 207.6	11.12	0.1689	5.614	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	2) = 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	2) = 224.8	11.43	0.1157	4.102	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	2) = 232.3	11.55	0.9997E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	2) = 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	3) = 113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	3) = 134.8	8.477	1.036	9.913	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	3) = 154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	3) = 171.6	10.18	0.4327	5.259	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	3) = 185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	3) = 197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	3) = 207.6	11.12	0.1689	2.428	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	3) = 216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	3) = 224.8	11.43	0.1157	1.773	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	3) = 232.3	11.55	0.9997E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	3) = 233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	4) = 1 233.4	9.779	3.721	16.07	14.94	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 167.52

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5902.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.559

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6002.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.553

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6042.0

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	2.333	0.0000E+00	419.0	0.0000E+00	13.50
2	1563.	1650.	1.539	0.0000E+00	453.4	0.0000E+00	13.50
3	1563.	1650.	1.101	0.0000E+00	484.4	0.0000E+00	13.50
4	1563.	1650.	0.7476	0.0000E+00	510.1	0.0000E+00	13.50
5	1563.	1650.	0.5443	0.0000E+00	531.0	0.0000E+00	13.50
6	1562.	1650.	0.4158	0.0000E+00	548.3	0.0000E+00	13.50
7	1562.	1650.	0.3351	0.0000E+00	563.0	0.0000E+00	13.50
8	1562.	1650.	0.2858	0.0000E+00	576.0	0.0000E+00	13.50
9	1562.	1650.	0.2452	0.0000E+00	587.6	0.0000E+00	13.50
10	1562.	1650.	0.2115	0.0000E+00	598.2	0.0000E+00	13.50
11	1562.	1650.	19.79	0.0000E+00	599.8	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.237
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6058.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.5829
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6065.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.8691
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.7

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[illegible]

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible][illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
25	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
28	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0		

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1583	0.0000E+00	853.9	0.0000E+00	0.100000E-01
2	2636.	1726.	0.1044	0.0000E+00	898.1	0.0000E+00	0.100000E-01
3	2636.	1726.	0.7469E-01	0.0000E+00	937.5	0.0000E+00	0.100000E-01
4	2636.	1726.	0.5071E-01	0.0000E+00	970.0	0.0000E+00	0.100000E-01
5	2635.	1726.	0.3693E-01	0.0000E+00	996.2	0.0000E+00	0.100000E-01
6	2635.	1726.	0.2821E-01	0.0000E+00	1018.	0.0000E+00	0.100000E-01
7	2635.	1725.	0.2273E-01	0.0000E+00	1036.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.1939E-01	0.0000E+00	1052.	0.0000E+00	0.100000E-01
9	2635.	1725.	0.1663E-01	0.0000E+00	1067.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1435E-01	0.0000E+00	1080.	0.0000E+00	0.100000E-01
11	2634.	1725.	1.343	0.0000E+00	1082.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76229
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31089
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12679
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.1074E-01	0.0000E+00	1389.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.7081E-02	0.0000E+00	1441.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.5067E-02	0.0000E+00	1487.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3440E-02	0.0000E+00	1526.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2505E-02	0.0000E+00	1556.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1913E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1542E-02	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01
8	3708.	1801.	0.1315E-02	0.0000E+00	1622.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1128E-02	0.0000E+00	1638.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.9735E-03	0.0000E+00	1654.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.9109E-01	0.0000E+00	1656.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.51711E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21090E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.86012E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.7283E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.4803E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3437E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2334E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1699E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1298E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1046E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.8922E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7655E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6604E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.6179E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

THICKNESS (FT) OF Silt			ACCUMULATED ON BOTTOM,																													
...MULTIPLY DISPLAYED VALUES BY			14400.00 SECONDS AFTER DUMP (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)																													
M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31		
2	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000	00000000		
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	0	0	0	0	0	0		
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	0	0	0	0	0	0		
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	+	+	+	+	.	.	0	0	0	0		
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	.01	.01	.01	+	+	+	.	0	0	0	0		
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	+	+	.01	.05	.09	.08	.04	.01	+	+	.	0	0	0		
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	.01	.05	.18	.32	.28	.13	.03	+	+	.	0	0	0		
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	.01	.09	.31	.62	.53	.22	.05	+	+	.	0	0	0		
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	.01	.08	.27	.52	.45	.19	.04	+	+	.	0	0	0		
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.03	.12	.21	.18	.08	.02	+	+	.	.	0	0		
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	.01	.03	.05	.04	.02	+	+	+	.	.	0	0		
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	.01	.01	+	+	+	+	.	.	0	0		
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	0		
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	0		
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	0		
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.		
21	0000	0	0	0	0																											

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.														

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1232.1

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1392.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 435.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2189.1

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	112.6	0.0000E+00	419.0	0.0000E+00	0.200000E-02
2	1563.	1650.	5.895	0.0000E+00	453.4	0.0000E+00	0.200000E-02
3	1563.	1650.	4.298	0.0000E+00	484.4	0.0000E+00	0.200000E-02
4	1563.	1650.	3.093	0.0000E+00	510.1	0.0000E+00	0.200000E-02
5	1563.	1650.	2.260	0.0000E+00	531.0	0.0000E+00	0.200000E-02
6	1562.	1650.	1.742	0.0000E+00	548.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.388	0.0000E+00	563.0	0.0000E+00	0.200000E-02
8	1562.	1650.	1.183	0.0000E+00	576.0	0.0000E+00	0.200000E-02
9	1562.	1650.	1.025	0.0000E+00	587.6	0.0000E+00	0.200000E-02
10	1562.	1650.	0.9074	0.0000E+00	598.2	0.0000E+00	0.200000E-02
11	1438.	1641.	300.8	0.0000E+00	599.8	0.3251E-01	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 364.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2260.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2319.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 255.11
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2369.3

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.06	.03	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.12	.07	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.23	.14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.41	.24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.67	.39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	1.0	.60	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	1.5	.88	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	2.0	1.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	2.7	1.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	3.3	1.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	3.8	2.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	4.2	2.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	4.3	2.4	0	0	0	0</												

[illegible]

7200.00 SECONDS AFTER DUMP

0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	66.02	0.0000E+00	853.9	0.0000E+00	0.200000E-02
2	2636.	1726.	3.455	0.0000E+00	898.1	0.0000E+00	0.200000E-02
3	2636.	1726.	2.519	0.0000E+00	937.5	0.0000E+00	0.200000E-02
4	2636.	1726.	1.813	0.0000E+00	970.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.324	0.0000E+00	996.2	0.0000E+00	0.200000E-02
6	2635.	1726.	1.021	0.0000E+00	1018.	0.0000E+00	0.200000E-02
7	2635.	1725.	0.8135	0.0000E+00	1036.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.6936	0.0000E+00	1052.	0.0000E+00	0.200000E-02
9	2635.	1725.	0.6010	0.0000E+00	1067.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5318	0.0000E+00	1080.	0.0000E+00	0.200000E-02
11	2511.	1717.	176.3	0.0000E+00	1082.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2410.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.67
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2445.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2474.9

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33		.14	.11	.09	.07	.05	.04	.02	0	0	0	0	0	0	0	0	0	00000
34		.21	.17	.13	.10	.08	.06	.04	0	0	0	0	0					

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
40	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.16	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.16	.12	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
54	.06	.04	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
56	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.0000
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	38.69	0.0000E+00	1389.	0.0000E+00	0.200000E-02
2	3709.	1801.	2.025	0.0000E+00	1441.	0.0000E+00	0.200000E-02
3	3709.	1801.	1.476	0.0000E+00	1487.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.062	0.0000E+00	1526.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.7763	0.0000E+00	1556.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.5983	0.0000E+00	1582.	0.0000E+00	0.200000E-02
7	3708.	1801.	0.4768	0.0000E+00	1603.	0.0000E+00	0.200000E-02
8	3708.	1801.	0.4065	0.0000E+00	1622.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3522	0.0000E+00	1638.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3117	0.0000E+00	1654.	0.0000E+00	0.200000E-02
11	3583.	1792.	103.3	0.0000E+00	1656.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 125.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2499.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.71
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2519.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.632
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2535.8

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
43	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.20	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	0
46	.25	.23	.21	.18	.16	.14	.12	.10	.08	.06	.05	.04	.03	0	0	0	0
47	.32	.29	.26	.23	.20	.18	.15	.12	.10	.08	.07	.05	.04	0	0	0	0
48	.40	.37	.33	.29	.26	.22	.19	.16	.13	.10	.08	.07	.05	0	0	0	0
49	.50	.45	.41	.36	.32	.27	.23	.19	.16	.13	.10	.08	.06	0	0	0	0
50	.61	.55	.50	.44	.38	.33	.28	.23	.19	.16	.13	.10	.08	0	0	0	0
51	.73	.66	.60	.53	.46	.40	.34	.28	.23	.19	.15	.12	.09	0	0	0	0
52	.86	.79	.71	.63	.55	.47	.40	.33	.28	.22	.18	.14	.11	0	0	0	0
53	1.0	.92	.83	.73	.64	.55	.47	.39	.32	.26	.21	.17	.13	0	0	0	0
54	1.1	1.0	.96	.85	.74	.63	.54	.45	.37	.30	.24	.19	.15	0	0	0	0
55	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.22	.17	0	0	0	0
56	1.5	1.3	1.2	1.0	.94	.81	.69	.57	.47	.38	.31	.24	.19	0	0	0	0
57	1.6	1.5	1.3	1.2	1.0	.90	.76	.64	.52	.43	.34	.27	.21	0	0	0	0
58	1.8	1.6	1.4	1.3	1.1	.98	.83	.69	.57	.46	.37	.29	.23	0	0	0	0
59	1.9	1.7	1.6	1.4	1.2	1.0	.89	.75	.61	.50	.40	.31	.24	0	0	0	0
60	2.0	1.8	1.7	1.5	1.3	1.1	.95	.79	.65	.53	.42	.33	.26	0	0	0	0

[illegible]

```
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	22.68	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8653	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6227	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2795	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2382	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2064	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	4656.	1868.	60.57	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF PCBs

SUMMARY OF PCBs DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1306

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.4	1599.	287.5	286.4	339.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1291

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	510.9	509.8	462.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1562.	1650.	872.6	871.5	599.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	1373.	1372.	749.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	2037.	2036.	910.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2634.	1725.	2886.	2885.	1082.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1257

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	3946.	3945.	1264.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3350.	1776.	5240.	5239.	1455.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-08 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
34	0000	0	0	0	0	0	0	0	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.09	.10	.10	.10	.10	.10	.09	.08	.07
35	0000	0	0	0	0	0	0	0	+	+	+	.01	.01	.02	.03	.04	.05	.06	.08	.09	.11	.12	.14	.15	.15	.15	.15	.15	.14	.12
36	0000	0	0	0	0	0	0	0	+	.01	.01	.02	.03	.04	.06	.08	.10	.12	.14	.16	.19	.20	.22	.23	.23	.23	.22	.20	.19	.16
37	0000	0	0	0	0	0	0	.01	.01	.02	.03	.05	.07	.09	.11	.14	.17	.21	.24	.27	.29	.31	.33	.33	.33	.31	.29	.27	.24	
38	0000	0	0	0	0	0	0	.01	.02	.03	.05	.07	.09	.12	.16	.20	.24	.29	.33	.38	.41	.44	.46	.46	.46	.44	.41	.38	.33	
39	0000	0	0	0	0	0	0	.02	.03	.05	.07	.09	.13	.17	.22	.27	.33	.39	.46	.51	.56	.60	.62	.63	.62	.60	.56	.51	.46	
40	0000	0	0	0	0	0	0	.03	.04	.06	.09	.13	.17	.23	.29	.36	.44	.52	.61	.68	.75	.80	.83	.84	.83	.80	.75	.68	.61	
41	0000	0	0	0	0	0	0	.03	.05	.08	.12	.16	.22	.29	.38	.47	.57	.68	.78	.88	.96	1.0	1.0	1.0	1.0	1.0	.97	.88	.79	
42	0000	0	0	0	0	0	0	.05	.07	.10	.15	.21	.28	.37	.48	.59	.72	.86	.99	1.1	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.1	.99	
43	0000	0	0	0	0	0	0	.06	.09	.13	.18	.26	.35	.46	.59	.73	.89	1.0	1.2	1.3	1.4	1.5	1.6	1.6	1.6	1.6	1.5	1.3	1.2	
44	0000	0	0	0	0	0	0	.07	.11	.16	.22	.31	.42	.55	.70	.87	1.0	1.2	1.4	1.6	1.7	1.9	1.9	2.0	1.9	1.9	1.7	1.6		
45	0000	0	0	0	0	0	0	.08	.12	.18	.26	.36	.49	.64	.82	1.0	1.2	1.4	1.6	1.9	2.0	2.2	2.3	2.3	2.3	2.2	2.0	1.9		
46	0000	0	0	0	0	0	0	.09	.14	.21	.30	.41	.55	.73	.93	1.1	1.4	1.6	1.9	2.1	2.3	2.5	2.6	2.6	2.6	2.5	2.3	2.1		
47	0000	0	0	0	0	0	0	.10	.16	.23	.33	.45	.61	.80	1.0	1.2	1.5	1.8	2.1	2.3	2.6	2.7	2.9	2.9	2.9	2.8	2.6	2.4		
48	0000	0	0	0	0	0	0	.11	.17	.25	.35	.49	.66	.87	1.1	1.3	1.6	1.9	2.2	2.5	2.8	3.0	3.1	3.1	3.1	3.0	2.8	2.5		
49	0000	0	0	0	0	0	0	.12	.18	.26	.37	.51	.69	.91	1.1	1.4	1.7	2.0	2.4	2.7	2.9	3.1	3.2	3.3	3.2	3.1	2.9	2.7		
50	0000	0	0	0	0	0	0	.12	.18	.27	.38	.53	.71	.93	1.2	1.4	1.8	2.1	2.4	2.7	3.0	3.2	3.3	3.4	3.3	3.2	3.0	2.7		
51	0000	0	0	0	0	0	0	.12	.18	.27	.38	.53	.71	.93	1.1	1.4	1.8	2.1	2.4	2.7	3.0	3.2	3.3	3.4	3.3	3.2	3.0	2.7		
52	0000	0	0	0	0	0	0	.12	.18	.26	.37	.51	.69	.91	1.1	1.4	1.7	2.0	2.4	2.6	2.9	3.1	3.2	3.3	3.2	3.1	2.9	2.7		
53	0000	0	0	0	0	0	0	.11	.17	.25	.35	.49	.65	.86	1.1	1.3	1.6	1.9	2.2	2.5	2.8	2.9	3.1	3.1	3.1	2.9	2.8	2.5		
54	0000	0	0	0	0	0	0	.10	.15	.23	.32	.45	.60	.79	1.0	1.2	1.5	1.8	2.1	2.3	2.5	2.7	2.8	2.9	2.8	2.7	2.5	2.3		
55	0000	0	0	0	0	0	0	.09	.14	.20	.29	.40	.54	.71	.91	1.1	1.3	1.6	1.8	2.1	2.3	2.4	2.5	2.6	2.5	2.4	2.3	2.1		
56	0000	0	0	0	0	0	0	.08	.12	.18	.25	.35	.48	.63	.80	1.0	1.2	1.4	1.6	1.8	2.0	2.1	2.2	2.2	2.2	2.1	2.0	1.8		

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3707.	1801.	6791.	6790.	1656.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4065.	1826.	8625.	8624.	1865.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1260

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.1076E+05	0.1076E+05	2083.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.1738

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 14400.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-08 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	
3	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
4	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
5	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
6	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
7	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
8	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
9	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
10	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
11	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
12	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
13	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
14	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
15	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
16	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
17	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
18	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
19	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
20	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
21	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
22	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
23	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
24	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
25	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
26	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
27	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
28	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
29	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
30	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
31	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
32	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
33	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
34	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
35	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
36	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
37	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
38	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
39	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
40	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
41	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
42	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
43	0000	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	00	
44	0000	00	00	+	+	+	.01	.01	.01	.02	.02	.03	.04	.04	.05	.06	.06	.07	.08	.09	.09	.10	.10	.10	.10	.10	.10	.10	.09	.09
45	0000	00	00	+	+	.01	.01	.02	.02	.03	.03	.04	.05	.06	.07	.08	.09	.10	.10	.11	.12	.13	.13	.13	.13	.13	.13	.13	.12	.11
46	0000	00	00	+	.01	.01	.02	.02	.03	.04	.04	.05	.06	.08	.09	.10	.11	.12	.14	.15	.16	.16	.17	.17	.17	.17	.17	.16	.16	.15
47	0000	00	00	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.10	.11	.13	.14	.16	.17	.19	.20	.21	.22	.22	.22	.22	.22	.21	.20	.19
48	0000	00	00	.01	.02	.02	.03	.04	.05	.06	.07	.09	.11	.12	.14	.16	.18	.20	.22	.24	.25	.27	.27	.28	.28	.28	.27	.25	.24	
49	0000	00	00	.01	.02	.03	.04	.05	.06	.07	.09	.11	.13	.15	.18	.20	.23	.25	.28	.30	.32	.33	.34	.35	.35	.35	.34	.33	.32	.30
50	0000	00	00	.02	.03	.03	.05	.06	.07	.09	.11	.14	.16	.19	.22	.25	.28	.31	.34	.36	.39	.41	.42	.43	.43	.43	.42	.41	.39	.37
51	0000	00	00	.02	.03	.04	.06	.07	.09	.11	.14	.17	.20	.23	.27	.30	.34	.37	.41	.44	.47	.49	.51	.52	.52	.52	.51	.49	.47	.44
52	0000	00	00	.03	.04	.05	.07	.09	.11	.14	.17	.20	.24	.28	.32	.36	.40	.45	.49	.53	.56	.59	.61	.62	.62	.62	.61	.59	.56	.53
53	0000	00	00	.03	.05	.06	.08	.10	.13	.16	.20	.24	.28	.33	.37	.43	.48	.53	.58	.62	.66	.69	.71	.73	.73	.73	.71	.69	.66	.62
54	0000	00	00	.04	.06	.07	.09	.12	.15	.19	.23	.27	.32	.38	.44	.49	.55	.61	.67	.72	.76	.80	.83	.85	.85	.85	.83	.80	.77	.72
55	0000	00	00	.05	.06	.08	.11	.14	.17	.21	.26	.31	.37	.43	.50	.57	.64	.70	.77	.83	.88	.92	.95	.97	.98	.97	.95	.92	.88	.83
56	0000	00	00	.05	.07	.10	.12	.16	.20	.24																				

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M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.08	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
45	.10	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
46	.14	.13	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0	0	0	0
47	.18	.16	.15	.13	.11	.10	.08	.07	.06	.05	.04	.03	.02	0	0	0	0
48	.22	.20	.18	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
49	.28	.25	.23	.20	.18	.16	.13	.11	.09	.08	.06	.05	.04	0	0	0	0
50	.34	.31	.28	.25	.22	.19	.16	.14	.11	.09	.08	.06	.05	0	0	0	0
51	.41	.38	.34	.30	.27	.23	.20	.17	.14	.11	.09	.07	.06	0	0	0	0
52	.49	.45	.41	.36	.32	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
53	.58	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0
54	.67	.62	.56	.50	.44	.38	.33	.28	.23	.19	.15	.12	.10	0	0	0	0
55	.77	.71	.64	.57	.50	.44	.37	.32	.26	.22	.18	.14	.11	0	0	0	0
56	.87	.80	.72	.64	.57	.49	.42	.36	.30	.25	.20	.16	.13	0	0	0	0
57	.97	.89	.81	.72	.63	.55	.47	.40	.33	.27	.22	.18	.14	0	0	0	0
58	1.0	.98	.89	.79	.70	.61	.52	.44	.37	.30	.25	.20	.15	0	0	0	0
59	1.1	1.0	.96	.86	.76	.66	.57	.48	.40	.33	.27	.21	.17	0	0	0	0
60	1.2	1.1	1.0	.92	.81	.71	.61	.51	.43	.35	.29	.23	.18	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.02	.01	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.03	.02	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.05	.03	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.06	.04	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.08	.05	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.10	.06	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
35	.11	.06	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.11	.06	.04	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0
37	.11	.08	.05	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0
38	.13	.09	.06	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
39	.14	.10	.06	.03	.02	+	+	+	+	0	0	0	0	0	0	0	0
40	.15	.11	.07	.04	.03	.01	+	+	+	0	0	0	0	0	0	0	0
41	.16	.11	.07	.05	.03	.01	.01	+	+	+	+	0	0	0	0	0	0
42	.15	.11	.08	.05	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
43	.16	.12	.09	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
44	.17	.13	.09	.07	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0
45	.18	.13	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0
46	.18	.13	.10	.07	.05	.04	.03	.01	.01	+	+	+	+	0	0	0	0
47	.17	.13	.10	.08	.06	.04	.03	.02	.01	+	+	+	+	0	0	0	0
48	.16	.13	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	0	0	0	0
49	.17	.14	.11	.09	.07	.05	.03	.02	.02	.01	+	+	+	0	0	0	0
50	.18	.15	.12	.09	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
51	.18	.15	.12	.09	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
52	.17	.14	.11	.09	.07	.06	.04	.03	.02	.01	.01	+	+	0	0	0	0
53	.16	.14	.12	.09	.08	.06	.05	.03	.02	.02	.01	.01	+	0	0	0	0
54	.16	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	0	0	0	0
55	.17	.14	.12	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
56	.17	.14	.12	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
57	.16	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
58	.15	.13	.11	.10	.08	.07	.06	.04	.03	.03	.02	.02	.01	0	0	0	0
59	.15	.13	.12	.10	.09	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
60	.15	.14	.12	.10	.09	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.1323E+05	0.1323E+05	2310.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.152E+02	1575.	1650.
2.00	0.0	0.299E+00	2625.	1725.
3.00	0.0	0.840E-02	3675.	1800.
4.00	0.0	0.289E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.419E+02	2550.	1725.
3.00	0.0	0.102E+02	3675.	1800.
4.00	0.0	0.302E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR PCBs

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.210E-07	0.652E-05	825.	1575.
0.67	0.0	0.117E-07	0.651E-05	1200.	1650.
1.00	0.0	0.705E-08	0.651E-05	1575.	1650.
1.33	0.0	0.445E-08	0.650E-05	1950.	1650.
1.67	0.0	0.304E-08	0.650E-05	2250.	1725.
2.00	0.0	0.217E-08	0.650E-05	2625.	1725.
2.33	0.0	0.159E-08	0.650E-05	3000.	1725.
2.67	0.0	0.120E-08	0.650E-05	3375.	1800.
3.00	0.0	0.926E-09	0.650E-05	3675.	1800.
3.33	0.0	0.730E-09	0.650E-05	4050.	1800.
3.67	0.0	0.586E-09	0.650E-05	4425.	1875.
4.00	0.0	0.497E-09	0.650E-05	4800.	1875.
0.33	6.8	0.774E-07	0.658E-05	825.	1575.
0.67	6.8	0.432E-07	0.654E-05	1200.	1650.
1.00	6.8	0.261E-07	0.653E-05	1575.	1650.
1.33	6.8	0.165E-07	0.652E-05	1950.	1650.
1.67	6.8	0.112E-07	0.651E-05	2250.	1725.
2.00	6.8	0.803E-08	0.651E-05	2625.	1725.
2.33	6.8	0.587E-08	0.651E-05	3000.	1725.
2.67	6.8	0.443E-08	0.650E-05	3375.	1800.
3.00	6.8	0.342E-08	0.650E-05	3675.	1800.
3.33	6.8	0.270E-08	0.650E-05	4050.	1800.
3.67	6.8	0.216E-08	0.650E-05	4425.	1875.
4.00	6.8	0.184E-08	0.650E-05	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

AA							
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*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF PCBs FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF PCBs IS 0.261000E-05 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.6500000E-05 MG/L.

THE WATER QUALITY STANDARD FOR PCBs IS 0.3000000E-04 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	1) = 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	1) = 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	1) = 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	1) = 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	1) = 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	1) = 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	1) = 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	1) = 201.4	11.31	0.1341	8.588	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	1) = 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	1) = 214.3	11.55	0.9280E-01	6.297	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	1) = 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	2) = 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	2) = 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	2) = 144.6	9.538	0.6070	13.14	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	2) = 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	2) = 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	2) = 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	2) = 193.7	11.14	0.1709	4.997	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	2) = 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	2) = 208.2	11.44	0.1096	3.434	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	2) = 214.3	11.55	0.9280E-01	2.986	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	2) = 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0 1575.	3) = 114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7 1575.	3) = 128.4	8.827	0.7117	5.741	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5 1575.	3) = 144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4 1575.	3) = 160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3 1575.	3) = 173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3 1575.	3) = 184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3 1575.	3) = 193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3 1575.	3) = 201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3 1575.	3) = 208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3 1575.	3) = 214.3	11.55	0.9280E-01	1.260	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3 1575.	3) = 214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0 1575.	4) = 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7 1575.	4) = 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5 1575.	4) = 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4 1575.	4) = 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3 1575.	4) = 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3 1575.	4) = 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3 1575.	4) = 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3 1575.	4) = 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3 1575.	4) = 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3 1575.	4) = 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3 1575.	4) = 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	5) = 1 214.5	10.08	3.420	10.74	9.373	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 128.12

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4904.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 51.587

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4981.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 21.039

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5011.7

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.250	0.0000E+00	420.7	0.0000E+00	13.50
2	1563.	1650.	0.9148	0.0000E+00	443.1	0.0000E+00	13.50
3	1563.	1650.	0.8659	0.0000E+00	468.8	0.0000E+00	13.50
4	1563.	1650.	0.6671	0.0000E+00	492.8	0.0000E+00	13.50
5	1562.	1650.	0.5040	0.0000E+00	512.9	0.0000E+00	13.50
6	1562.	1650.	0.3810	0.0000E+00	529.3	0.0000E+00	13.50
7	1562.	1650.	0.2980	0.0000E+00	542.7	0.0000E+00	13.50
8	1562.	1650.	0.2459	0.0000E+00	554.0	0.0000E+00	13.50
9	1562.	1650.	0.2051	0.0000E+00	563.8	0.0000E+00	13.50
10	1561.	1650.	0.1706	0.0000E+00	572.5	0.0000E+00	13.50
11	1561.	1650.	15.54	0.0000E+00	572.8	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 8.5805
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5024.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.4994
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.4272
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.8483E-01	0.0000E+00	856.1	0.0000E+00	0.100000E-01
2	2636.	1726.	0.6206E-01	0.0000E+00	884.9	0.0000E+00	0.100000E-01
3	2636.	1726.	0.5874E-01	0.0000E+00	917.7	0.0000E+00	0.100000E-01
4	2635.	1726.	0.4525E-01	0.0000E+00	948.2	0.0000E+00	0.100000E-01
5	2635.	1726.	0.3419E-01	0.0000E+00	973.5	0.0000E+00	0.100000E-01
6	2635.	1726.	0.2584E-01	0.0000E+00	994.1	0.0000E+00	0.100000E-01
7	2635.	1726.	0.2022E-01	0.0000E+00	1011.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.1668E-01	0.0000E+00	1025.	0.0000E+00	0.100000E-01
9	2634.	1725.	0.1391E-01	0.0000E+00	1037.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1157E-01	0.0000E+00	1048.	0.0000E+00	0.100000E-01
11	2634.	1725.	1.054	0.0000E+00	1048.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.58207
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.23739
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.96817E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.5754E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.4210E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.3985E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3070E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2319E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1753E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1371E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1132E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.9436E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.7852E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7149E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.39486E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.16104E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65677E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.3904E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2856E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.2703E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2082E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1573E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1189E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.9304E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.7677E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.6401E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.5326E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4850E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

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[illegible]

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BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 938.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1183.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.09

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1694.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 343.50

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1778.7

0.00 FT BELOW THE WATER SURFACE

[illegible]

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SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	96.43	0.0000E+00	420.7	0.0000E+00	0.200000E-02
2	1563.	1650.	3.412	0.0000E+00	443.1	0.0000E+00	0.200000E-02
3	1563.	1650.	3.268	0.0000E+00	468.8	0.0000E+00	0.200000E-02
4	1563.	1650.	2.684	0.0000E+00	492.8	0.0000E+00	0.200000E-02
5	1562.	1650.	2.040	0.0000E+00	512.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.556	0.0000E+00	529.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.188	0.0000E+00	542.7	0.0000E+00	0.200000E-02
8	1562.	1650.	0.9942	0.0000E+00	554.0	0.0000E+00	0.200000E-02
9	1562.	1650.	0.8375	0.0000E+00	563.8	0.0000E+00	0.200000E-02
10	1561.	1650.	0.7256	0.0000E+00	572.5	0.0000E+00	0.200000E-02
11	1435.	1641.	230.4	0.0000E+00	572.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 287.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 240.57
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1881.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 201.32
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1920.9

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
19		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
20		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
21		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
24		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
26	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
27	.02	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
28	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
29	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
30	.03	.01	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
31	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
32	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
33	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
34	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
35	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
36	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
37	.03	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	56.52	0.0000E+00	856.1	0.0000E+00	0.200000E-02
2	2636.	1726.	2.000	0.0000E+00	884.9	0.0000E+00	0.200000E-02
3	2636.	1726.	1.915	0.0000E+00	917.7	0.0000E+00	0.200000E-02
4	2635.	1726.	1.573	0.0000E+00	948.2	0.0000E+00	0.200000E-02
5	2635.	1726.	1.195	0.0000E+00	973.5	0.0000E+00	0.200000E-02
6	2635.	1726.	0.9122	0.0000E+00	994.1	0.0000E+00	0.200000E-02
7	2635.	1726.	0.6960	0.0000E+00	1011.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.5827	0.0000E+00	1025.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.4908	0.0000E+00	1037.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.4253	0.0000E+00	1048.	0.0000E+00	0.200000E-02
11	2508.	1717.	135.0	0.0000E+00	1048.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 168.48
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1953.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1981.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 117.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2004.2

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.09	.07	.06	.04	.03	.02	.01	0	0	0	0	0	0	0	0	0	0
34		.14	.12	.09	.07	.05	.03	.02	0	0	0	0	0	0	0	0	0	0
35		.22	.17	.14	.10	.08	.05	.04	0	0	0	0	0					

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
30	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
34	.08	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.09	.05	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
37	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
38	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
40	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
41	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
42	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.0000
43	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
44	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
45	.12	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
46	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
47	.11	.08	.06	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
48	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
50	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
51	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
52	.06	.05	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
53	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
54	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
55	.03	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
56	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.0000
57	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.0000
58	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.0000
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	33.12	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.9218	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7006	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5347	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4079	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	3707. 1801.	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.2877	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	3581. 1792.	79.13	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 98.744
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2023.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 82.635
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2039.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 69.155
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2052.3

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
43	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	00000
44	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	00000
45	.15	.13	.12	.10	.09	.08	.06	.05	.04	.03	.03	.02	.01	0	0	0	00000
46	.19	.17	.15	.14	.12	.10	.08	.07	.06	.04	.04	.03	.02	0	0	0	00000
47	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	00000
48	.31	.28	.25	.22	.19	.16	.14	.11	.09	.07	.06	.05	.03	0	0	0	00000
49	.38	.35	.31	.27	.24	.20	.17	.14	.12	.09	.07	.06	.04	0	0	0	00000
50	.47	.43	.38	.34	.29	.25	.21	.17	.14	.12	.09	.07	.05	0	0	0	00000
51	.57	.52	.46	.41	.35	.30	.25	.21	.17	.14	.11	.09	.07	0	0	0	00000
52	.68	.61	.55	.49	.42	.36	.30	.25	.21	.17	.13	.10	.08	0	0	0	00000
53	.80	.72	.65	.57	.50	.42	.36	.30	.24	.20	.16	.12	.09	0	0	0	00000
54	.93	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	.11	0	0	0	00000
55	1.0	.96	.86	.76	.66	.56	.47	.39	.32	.26	.21	.16	.12	0	0	0	00000
56	1.1	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	.14	0	0	0	00000
57	1.3	1.2	1.0	.95	.82	.70	.59	.49	.40	.32	.26	.20	.16	0	0	0	00000
58	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.36	.28	.22	.17	0	0	0	00000
59	1.5	1.4	1.2	1.1	.97	.83	.70	.58	.48	.38	.30	.24	.18	0	0	0	00000
60	1.6	1.5	1.3	1.1	1.0	.88	.74	.62	.51	.41	.32	.25	.19	0	0	0	00000

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
32	.06	.03	.01	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	19.41	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.6580	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4106	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.2391	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2002	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1686	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	4654.	1868.	46.38	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

```

. .0001      0 = .LT. .000001)

```

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF PCBs

SUMMARY OF PCBs DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3649

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	846.3	1599.	252.1	250.8	317.4	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3633

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1204.	1625.	459.0	457.6	438.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3633

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1561.	1650.	797.0	795.7	572.8	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3634

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1919.	1675.	1270.	1268.	719.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3634

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	1900.	1899.	878.7	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3633

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2634.	1725.	2713.	2711.	1048.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3511

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	3731.	3729.	1228.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3511

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3349.	1776.	4978.	4977.	1418.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3511

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-08 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
35	0000	0	0	0	0	0	0	+	+	.01	.01	.02	.03	.04	.05	.07	.08	.10	.12	.13	.15	.16	.17	.17	.17	.16	.15	.13	.12	.10	
36	0000	0	0	0	0	0	0	+	.01	.01	.02	.03	.05	.06	.08	.10	.13	.15	.18	.20	.22	.24	.25	.25	.25	.24	.22	.20	.18	.15	
37	0000	0	0	0	0	0	0	.01	.01	.02	.03	.05	.07	.09	.12	.15	.19	.23	.26	.30	.33	.35	.37	.37	.37	.35	.33	.30	.26	.23	
38	0000	0	0	0	0	0	0	.01	.02	.03	.05	.07	.10	.13	.17	.22	.27	.32	.38	.43	.47	.50	.52	.53	.52	.50	.47	.43	.38	.32	
39	0000	0	0	0	0	0	0	.02	.03	.05	.07	.10	.14	.19	.24	.31	.37	.45	.52	.59	.65	.69	.72	.73	.72	.70	.65	.59	.52	.45	
40	0000	0	0	0	0	0	0	.03	.04	.06	.10	.14	.19	.25	.33	.41	.51	.60	.70	.79	.87	.93	.97	.99	.97	.94	.87	.80	.70	.61	
41	0000	0	0	0	0	0	0	.04	.06	.09	.13	.18	.25	.33	.43	.54	.66	.79	.92	1.0	1.1	1.2	1.2	1.2	1.2	1.2	1.1	1.0	.92	.79	
42	0000	0	0	0	0	0	0	.05	.07	.11	.16	.23	.32	.42	.55	.69	.84	1.0	1.1	1.3	1.4	1.5	1.6	1.6	1.6	1.5	1.4	1.3	1.1	1.0	
43	0000	0	0	0	0	0	0	.06	.09	.14	.20	.29	.39	.52	.68	.85	1.0	1.2	1.4	1.6	1.8	1.9	2.0	2.0	2.0	1.9	1.8	1.6	1.4	1.2	
44	0000	0	0	0	0	0	0	.07	.11	.17	.25	.35	.47	.63	.82	1.0	1.2	1.5	1.7	1.9	2.1	2.3	2.4	2.4	2.4	2.3	2.1	1.9	1.7	1.5	
45	0000	0	0	0	0	0	0	.09	.13	.20	.29	.41	.56	.74	.96	1.2	1.4	1.7	2.0	2.3	2.5	2.7	2.8	2.8	2.8	2.7	2.5	2.3	2.0	1.7	
46	0000	0	0	0	0	0	0	.10	.15	.23	.33	.47	.64	.85	1.1	1.3	1.7	2.0	2.3	2.6	2.9	3.1	3.2	3.3	3.2	3.1	2.9	2.6	2.3	2.0	
47	0000	0	0	0	0	0	0	.11	.17	.25	.37	.52	.71	.94	1.2	1.5	1.8	2.2	2.6	2.9	3.2	3.4	3.6	3.6	3.6	3.4	3.2	2.9	2.6	2.2	
48	0000	0	0	0	0	0	0	.12	.18	.28	.40	.56	.77	1.0	1.3	1.6	2.0	2.4	2.8	3.2	3.5	3.7	3.9	3.9	3.9	3.7	3.5	3.2	2.8	2.4	
49	0000	0	0	0	0	0	0	.13	.19	.29	.42	.59	.81	1.0	1.3	1.7	2.1	2.5	2.9	3.3	3.7	3.9	4.1	4.1	4.1	4.1	3.9	3.7	3.3	3.0	2.5
50	0000	0	0	0	0	0	0	.13	.20	.30	.43	.61	.83	1.1	1.4	1.8	2.2	2.6	3.0	3.4	3.8	4.0	4.2	4.3	4.2	4.0	3.8	3.4	3.0	2.6	
51	0000	0	0	0	0	0	0	.13	.20	.30	.43	.61	.83	1.1	1.4	1.8	2.2	2.6	3.0	3.4	3.7	4.0	4.2	4.2	4.2	4.0	3.8	3.4	3.0	2.6	
52	0000	0	0	0	0	0	0	.13	.19	.29	.42	.59	.80	1.0	1.3	1.7	2.1	2.5	2.9	3.3	3.6	3.9	4.1	4.1	4.1	3.9	3.6	3.3	2.9	2.5	
53	0000	0	0	0	0	0	0	.12	.18	.27	.39	.56	.76	1.0	1.3	1.6	2.0	2.4	2.8	3.1	3.4	3.7	3.8	3.9	3.8	3.7	3.4	3.1	2.8	2.4	
54	0000	0	0	0	0	0	0	.11	.17	.25	.36	.51	.70	.93	1.2	1.5	1.8	2.2	2.5	2.9	3.2	3.4	3.5	3.6	3.5	3.4	3.2	2.9	2.5	2.2	
55	0000	0	0	0	0	0	0	.10	.15	.22	.32	.46	.63	.83	1.0	1.3	1.6	1.9	2.3	2.6	2.8	3.0	3.2	3.2	3.2	3.0	2.8	2.6	2.3	2.0	
56	0000	0	0	0	0	0	0	.08	.13	.19	.28	.40	.55	.73	.94	1.1	1.4	1.7	2.0	2.2	2.5	2.6	2.7	2.8	2.7	2.6	2.5	2.2	2.0	1.7	

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3707.	1801.	6479.	6478.	1617.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3506

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4065.	1826.	8257.	8256.	1825.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3506

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.1034E+05	0.1034E+05	2041.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 1.3506

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
45	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
46	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
47	.19	.18	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
48	.25	.22	.20	.18	.16	.13	.11	.10	.08	.06	.05	.04	.03	0	0	0	0
49	.31	.28	.25	.22	.20	.17	.14	.12	.10	.08	.06	.05	.04	0	0	0	0
50	.38	.35	.31	.28	.24	.21	.18	.15	.12	.10	.08	.06	.05	0	0	0	0
51	.46	.42	.38	.34	.30	.26	.22	.18	.15	.12	.10	.08	.06	0	0	0	0
52	.56	.51	.46	.41	.36	.31	.26	.22	.18	.15	.12	.09	.07	0	0	0	0
53	.66	.60	.54	.48	.42	.37	.31	.26	.22	.18	.14	.11	.09	0	0	0	0
54	.77	.71	.64	.57	.50	.43	.37	.31	.25	.21	.17	.13	.10	0	0	0	0
55	.89	.81	.73	.65	.57	.49	.42	.35	.29	.24	.19	.15	.12	0	0	0	0
56	1.0	.92	.83	.74	.65	.56	.48	.40	.33	.27	.22	.17	.14	0	0	0	0
57	1.1	1.0	.93	.83	.73	.63	.54	.45	.37	.31	.25	.20	.15	0	0	0	0
58	1.2	1.1	1.0	.92	.81	.70	.59	.50	.41	.34	.27	.22	.17	0	0	0	0
59	1.3	1.2	1.1	1.0	.88	.76	.65	.54	.45	.37	.30	.24	.18	0	0	0	0
60	1.4	1.3	1.2	1.0	.94	.82	.70	.59	.49	.40	.32	.25	.20	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
40	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
41	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0
42	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0	0	0
43	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
44	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
45	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
46	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
47	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0	0
48	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
49	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
50	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
51	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
52	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
53	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
54	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
55	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
56	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
57	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
58	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
59	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0
60	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4780.	1877.	0.1274E+05	0.1274E+05	2266.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....


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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.122E+02	1575.	1650.
2.00	0.0	0.236E+00	2625.	1725.
3.00	0.0	0.659E-02	3675.	1800.
4.00	0.0	0.226E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.200E+03	1500.	1650.
2.00	0.0	0.346E+02	2550.	1725.
3.00	0.0	0.834E+01	3675.	1800.
4.00	0.0	0.246E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR PCBs

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.287E-07	0.653E-05	825.	1575.
0.67	0.0	0.157E-07	0.652E-05	1200.	1650.
1.00	0.0	0.936E-08	0.651E-05	1575.	1650.
1.33	0.0	0.583E-08	0.651E-05	1950.	1650.
1.67	0.0	0.395E-08	0.650E-05	2250.	1725.
2.00	0.0	0.280E-08	0.650E-05	2625.	1725.
2.33	0.0	0.202E-08	0.650E-05	3000.	1725.
2.67	0.0	0.151E-08	0.650E-05	3375.	1800.
3.00	0.0	0.116E-08	0.650E-05	3675.	1800.
3.33	0.0	0.915E-09	0.650E-05	4050.	1800.
3.67	0.0	0.732E-09	0.650E-05	4425.	1875.
4.00	0.0	0.594E-09	0.650E-05	4800.	1875.
0.33	6.8	0.106E-06	0.661E-05	825.	1575.
0.67	6.8	0.580E-07	0.656E-05	1200.	1650.
1.00	6.8	0.346E-07	0.653E-05	1575.	1650.
1.33	6.8	0.216E-07	0.652E-05	1950.	1650.
1.67	6.8	0.146E-07	0.651E-05	2250.	1725.
2.00	6.8	0.104E-07	0.651E-05	2625.	1725.
2.33	6.8	0.746E-08	0.651E-05	3000.	1725.
2.67	6.8	0.559E-08	0.651E-05	3375.	1800.
3.00	6.8	0.430E-08	0.650E-05	3675.	1800.
3.33	6.8	0.338E-08	0.650E-05	4050.	1800.
3.67	6.8	0.270E-08	0.650E-05	4425.	1875.
4.00	6.8	0.220E-08	0.650E-05	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME		SNAPSHOT		ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF PCBs FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF PCBs IS 0.600000E-04 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR PCBs IS 0.300000E-04 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0 1575.	1) = 1 109.2	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8 1575.	1) = 2 130.9	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6 1575.	1) = 3 152.5	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5 1575.	1) = 4 171.5	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5 1575.	1) = 5 187.3	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5 1575.	1) = 6 200.5	10.89	0.2393	53.70	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5 1575.	1) = 7 211.8	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5 1575.	1) = 8 221.7	11.31	0.1469	35.76	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5 1575.	1) = 9 230.7	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5 1575.	1) = 10 238.9	11.58	0.1054	27.19	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5 1575.	1) = 11 239.2	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	2) = 1 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	2) = 2 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	2) = 3 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	2) = 4 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	2) = 5 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	2) = 6 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	2) = 7 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	2) = 8 221.7	11.31	0.1469	0.4822	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	2) = 9 230.7	11.46	0.1227	0.4153	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	2) = 10 238.9	11.58	0.1054	0.3668	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	2) = 11 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0 1575.	3) = 109.2	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8 1575.	3) = 130.9	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6 1575.	3) = 152.5	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5 1575.	3) = 171.5	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5 1575.	3) = 187.3	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5 1575.	3) = 200.5	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5 1575.	3) = 211.8	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5 1575.	3) = 221.7	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5 1575.	3) = 230.7	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5 1575.	3) = 238.9	11.58	0.1054	0.1514	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5 1575.	3) = 239.2	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	4) = 1 239.2	9.685	3.815	16.16	0.0000E+00	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.411

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 493.19

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 38.912

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 549.69

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 15.870

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 572.73

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.488	0.0000E+00	411.8	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	0.1670	0.0000E+00	447.2	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	0.1244	0.0000E+00	481.0	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.8470E-01	0.0000E+00	509.8	0.0000E+00	13.50	0.100000E-01
5	1562.	1650.	0.6077E-01	0.0000E+00	533.4	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.4553E-01	0.0000E+00	552.7	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.3587E-01	0.0000E+00	569.0	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	13.50	0.100000E-01
9	1562.	1650.	0.2516E-01	0.0000E+00	596.0	0.0000E+00	13.50	0.100000E-01
10	1562.	1650.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	13.50	0.100000E-01
11	1562.	1650.	13.79	0.0000E+00	607.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.4723
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 582.12

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.6397
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.96

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.0766
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.52
MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1009	0.0000E+00	844.6	0.0000E+00	0.100000E-01
2	2636.	1726.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	0.100000E-01
3	2636.	1726.	0.8436E-02	0.0000E+00	933.3	0.0000E+00	0.100000E-01
4	2635.	1726.	0.5746E-02	0.0000E+00	969.7	0.0000E+00	0.100000E-01
5	2635.	1726.	0.4122E-02	0.0000E+00	999.2	0.0000E+00	0.100000E-01
6	2635.	1726.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	0.100000E-01
7	2635.	1725.	0.2433E-02	0.0000E+00	1044.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	0.100000E-01
9	2635.	1725.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	0.100000E-01
11	2634.	1725.	0.9353	0.0000E+00	1092.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.43906
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.16

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17907
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.42

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73030E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.52
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
55	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
56	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
57	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
58	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
59	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
60	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.6846E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.7684E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3898E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2796E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2095E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	3708.	1801.	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1004E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.6345E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.29784E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.57

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12147E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.49541E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.59
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4644E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3882E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2644E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1421E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7853E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6808E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4304E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.871

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.29

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.710

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 136.65

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 106.35

[illegible]

[illegible]

[illegible]


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0 = .LT. .0000001)
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[illegible][illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	13.35	0.0000E+00	411.8	0.0000E+00	13.50	0.200000E-02
2	1563.	1650.	0.5799	0.0000E+00	447.2	0.0000E+00	13.50	0.200000E-02
3	1563.	1650.	0.4376	0.0000E+00	481.0	0.0000E+00	13.50	0.200000E-02
4	1563.	1650.	0.3164	0.0000E+00	509.8	0.0000E+00	13.50	0.200000E-02
5	1562.	1650.	0.2289	0.0000E+00	533.4	0.0000E+00	13.50	0.200000E-02
6	1562.	1650.	0.1739	0.0000E+00	552.7	0.0000E+00	13.50	0.200000E-02
7	1562.	1650.	0.1387	0.0000E+00	569.0	0.0000E+00	13.50	0.200000E-02
8	1562.	1650.	0.1153	0.0000E+00	583.3	0.0000E+00	13.50	0.200000E-02
9	1562.	1650.	0.9923E-01	0.0000E+00	596.0	0.0000E+00	13.50	0.200000E-02
10	1562.	1650.	0.8740E-01	0.0000E+00	607.5	0.0000E+00	13.50	0.200000E-02
11	1562.	1650.	121.1	0.0000E+00	607.9	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.64

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.702
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 147.30

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.91

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	7.825	0.0000E+00	844.6	0.0000E+00	13.50
2	2636.	1726.	0.3399	0.0000E+00	890.2	0.0000E+00	13.50
3	2636.	1726.	0.2564	0.0000E+00	933.3	0.0000E+00	13.50
4	2635.	1726.	0.1854	0.0000E+00	969.7	0.0000E+00	13.50
5	2635.	1726.	0.1342	0.0000E+00	999.2	0.0000E+00	13.50
6	2635.	1726.	0.1019	0.0000E+00	1023.	0.0000E+00	13.50
7	2635.	1725.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	13.50
8	2635.	1725.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	13.50
9	2635.	1725.	0.5816E-01	0.0000E+00	1077.	0.0000E+00	13.50
10	2634.	1725.	0.5122E-01	0.0000E+00	1091.	0.0000E+00	13.50
11	2634.	1725.	70.99	0.0000E+00	1092.	0.0000E+00	13.50

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.024
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.91

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 46.940
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 196.06

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

...MULTIPLY DISPLAYED VALUES BY 1.000

1.000

1.000 (LEGEND... + = .LT. .01 . = .LT.

```
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
```

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21		+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
25		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
26		+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
28	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
29	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
30	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
31	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
32	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
33	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
34	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
35	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
36	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0
37	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	0
38	.05	.03	.02	.01	+	+	+	+	+									

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	4.586	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5973E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4763E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	3708. 1801.	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.3409E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	3707. 1801.	41.61	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.282
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.69

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.874
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.511
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 215.12

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.03	.03	.03	.02	.02	.02	.01	.01	.01	.01	+	+	+	0	0	0	0
45	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	0	0	0	0
46	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0
47	.08	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
48	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
49	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
50	.16	.14	.13	.11	.10	.09	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
51	.19	.17	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
52	.23	.21	.19	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
53	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	0
54	.32	.29	.26	.23	.20	.18	.15	.13	.10	.08	.07	.05	.04	0	0	0	0
55	.36	.33	.30	.27	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
56	.41	.38	.34	.30	.27	.23	.20	.16	.14	.11	.09	.07	.06	0	0	0	0
57	.46	.42	.38	.34	.30	.26	.22	.18	.15	.13	.10	.08	.06	0	0	0	0
58	.51	.47	.42	.37	.33	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
59	.56	.51	.46	.41	.36	.31	.26	.22	.18	.15	.12	.10	.08	0	0	0	0
60	.60	.55	.49	.44	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0

[illegible]

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
24	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0000
25	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
26	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0000
28	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0000
29	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0000
30	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
31	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
32	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
33	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
34	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0000
35	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.0000
37	.05	.03																

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	2.688	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1998E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1759E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	4780.	1877.	24.38	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
24	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0000
25	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
26	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0000
28	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0000
29	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0000
30	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
31	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
32	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
33	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
34	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.0000
35	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.0000
37	.05	.03																

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	00000
23	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	00000
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
25	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
26	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	00000
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
28	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	00000
29	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
30	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
31	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
33	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.0000
34	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
37	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
38	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.	.0000
39	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
40	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
41	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
42	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
43	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
44	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
45	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
46	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+0000
50	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
51	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
52	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
53	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+0000
54	.08	.07	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
55	.08	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
56	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	+0000
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
58	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
59	.06	.05	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000
60	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	+0000

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF PCBs

SUMMARY OF PCBs DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.4	1599.	16.16	0.0000E+00	345.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	16.16	0.0000E+00	470.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1562.	1650.	16.16	0.0000E+00	607.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	16.16	0.0000E+00	758.0	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2277.	1700.	16.16	0.0000E+00	919.5	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

MAX CONC IS 0.00000003 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2634.	1725.	16.16	0.0000E+00	1092.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	16.16	0.0000E+00	1274.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3350.	1776.	16.16	0.0000E+00	1466.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000005 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-07 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0000	0	0	0	0	0	0	+	+	.01	.01	.02	.03	.04	.05	.06	.08	.09	.11	.12	.13	.14	.15	.15	.15	.14	.14	.12	.11	.09
35	0000	0	0	0	0	0	0	+	.01	.01	.02	.03	.05	.06	.08	.10	.12	.14	.17	.19	.20	.22	.23	.23	.23	.22	.21	.19	.17	.14
36	0000	0	0	0	0	0	0	.01	.01	.02	.03	.05	.07	.09	.12	.15	.18	.21	.24	.28	.30	.32	.33	.34	.33	.32	.30	.28	.25	.21
37	0000	0	0	0	0	0	0	.01	.02	.04	.05	.07	.10	.13	.17	.21	.26	.30	.35	.39	.43	.46	.48	.49	.48	.46	.43	.40	.35	.31
38	0000	0	0	0	0	0	0	.02	.03	.05	.07	.10	.14	.19	.24	.30	.36	.43	.49	.55	.60	.64	.67	.68	.67	.64	.60	.55	.49	.43
39	0000	0	0	0	0	0	0	.03	.05	.07	.10	.14	.19	.25	.32	.40	.49	.58	.67	.75	.82	.87	.91	.92	.91	.87	.82	.75	.67	.58
40	0000	0	0	0	0	0	0	.04	.06	.10	.14	.19	.26	.34	.43	.53	.65	.76	.88	.99	1.0	1.1	1.2	1.2	1.2	1.1	1.0	.99	.88	.77
41	0000	0	0	0	0	0	0	.06	.08	.12	.18	.25	.33	.43	.55	.69	.83	.98	1.1	1.2	1.3	1.4	1.5	1.5	1.5	1.4	1.3	1.2	1.1	.99
42	0000	0	0	0	0	0	0	.07	.11	.16	.22	.31	.42	.54	.70	.86	1.0	1.2	1.4	1.6	1.7	1.8	1.9	1.9	1.9	1.8	1.7	1.6	1.4	1.2
43	0000	0	0	0	0	0	0	.09	.13	.19	.27	.38	.51	.67	.85	1.0	1.2	1.5	1.7	1.9	2.1	2.2	2.3	2.4	2.3	2.2	2.1	1.9	1.7	1.5
44	0000	0	0	0	0	0	0	.11	.16	.23	.33	.45	.61	.80	1.0	1.2	1.5	1.8	2.0	2.3	2.5	2.7	2.8	2.8	2.8	2.7	2.5	2.3	2.0	1.8
45	0000	0	0	0	0	0	0	.12	.19	.27	.38	.53	.71	.93	1.1	1.4	1.7	2.1	2.4	2.7	2.9	3.1	3.2	3.3	3.2	3.1	2.9	2.7	2.4	2.1
46	0000	0	0	0	0	0	0	.14	.21	.31	.43	.60	.80	1.0	1.3	1.6	2.0	2.3	2.7	3.0	3.3	3.5	3.7	3.7	3.7	3.5	3.3	3.0	2.7	2.3
47	0000	0	0	0	0	0	0	.16	.23	.34	.48	.66	.89	1.1	1.4	1.8	2.2	2.6	3.0	3.4	3.7	3.9	4.1	4.1	4.1	3.9	3.7	3.4	3.0	2.6
48	0000	0	0	0	0	0	0	.17	.25	.37	.52	.71	.96	1.2	1.6	1.9	2.4	2.8	3.2	3.6	4.0	4.2	4.4	4.5	4.4	4.2	4.0	3.6	3.2	2.8
49	0000	0	0	0	0	0	0	.18	.26	.38	.54	.75	1.0	1.3	1.6	2.0	2.5	2.9	3.4	3.8	4.2	4.4	4.6	4.7	4.6	4.4	4.2	3.8	3.4	2.9
50	0000	0	0	0	0	0	0	.18	.27	.39	.56	.77	1.0	1.3	1.7	2.1	2.5	3.0	3.5	3.9	4.3	4.5	4.7	4.8	4.7	4.6	4.3	3.9	3.5	3.0
51	0000	0	0	0	0	0	0	.18	.27	.39	.56	.77	1.0	1.3	1.7	2.1	2.5	3.0	3.5	3.9	4.3	4.5	4.7	4.8	4.7	4.5	4.3	3.9	3.5	3.0
52	0000	0	0	0	0	0	0	.18	.26	.38	.54	.75	1.0	1.3	1.6	2.0	2.5	2.9	3.4	3.8	4.1	4.4	4.6	4.7	4.6	4.4	4.1	3.8	3.4	2.9
53	0000	0	0	0	0	0	0	.17	.25	.36	.51	.71	.95	1.2	1.5	1.9	2.3	2.8	3.2	3.6	3.9	4.2	4.4	4.4	4.4	4.2	3.9	3.6	3.2	2.8
54	0000	0	0	0	0	0	0	.15	.23	.33	.47	.65	.88	1.1	1.4	1.8	2.2	2.6	2.9	3.3	3.6	3.9	4.0	4.1	4.0	3.9	3.6	3.3	3.0	2.6
55	0000	0	0	0	0	0	0	.14	.21	.30	.43	.59	.79	1.0	1.3	1.6	1.9	2.3	2.7	3.0	3.3	3.5	3.6	3.7	3.6	3.5	3.3	3.0	2.7	2.3
56	0000	0	0	0	0	0	0	.12	.18	.26	.37	.52	.69	.91	1.1	1.4	1.7	2.0	2.3	2.6	2.9	3.1	3.2	3.2	3.2	3.1	2.9	2.6	2.3	2.0

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3707.	1801.	16.16	0.0000E+00	1667.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	16.16	0.0000E+00	1878.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	16.16	0.0000E+00	2096.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 16.156

MAX CONC IS 0.00000001 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 6.75 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 14400.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

		...MULTIPLY DISPLAYED VALUES BY 0.1000E-07										(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)																			
M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	0000	0	0	+	.01	.01	.01	.02	.02	.03	.04	.04	.05	.06	.07	.08	.09	.10	.11	.12	.13	.14	.14	.14	.14	.14	.14	.14	.13	.12	
45	0000	0	0	.01	.01	.01	.02	.02	.03	.04	.05	.06	.07	.08	.10	.11	.12	.14	.15	.16	.17	.18	.18	.19	.19	.19	.19	.18	.17	.16	
46	0000	0	0	.01	.01	.02	.02	.03	.04	.05	.06	.08	.09	.11	.13	.14	.16	.18	.19	.21	.22	.23	.24	.24	.25	.24	.24	.23	.22	.21	
47	0000	0	0	.01	.02	.02	.03	.04	.05	.07	.08	.10	.12	.14	.16	.18	.20	.23	.25	.27	.28	.30	.31	.31	.31	.31	.31	.30	.28	.27	
48	0000	0	0	.02	.02	.03	.04	.05	.07	.09	.11	.13	.15	.18	.20	.23	.26	.28	.31	.33	.35	.37	.38	.39	.39	.39	.38	.37	.36	.33	
49	0000	0	0	.02	.03	.04	.05	.07	.09	.11	.13	.16	.19	.22	.25	.28	.32	.35	.38	.41	.44	.46	.48	.49	.49	.49	.48	.46	.44	.42	
50	0000	0	0	.03	.04	.05	.07	.09	.11	.13	.16	.19	.23	.27	.31	.35	.39	.43	.47	.51	.54	.56	.58	.59	.60	.59	.58	.56	.54	.51	
51	0000	0	0	.04	.05	.06	.08	.10	.13	.16	.20	.23	.28	.32	.37	.42	.47	.52	.57	.61	.65	.68	.70	.72	.72	.72	.70	.68	.65	.61	
52	0000	0	0	.04	.06	.08	.10	.12	.16	.19	.23	.28	.33	.39	.44	.50	.56	.62	.68	.73	.77	.81	.84	.85	.86	.85	.84	.81	.77	.73	
53	0000	0	0	.05	.07	.09	.12	.15	.18	.23	.27	.33	.39	.45	.52	.59	.66	.73	.80	.86	.91	.95	.98	1.0	1.0	1.0	.98	.95	.91	.86	
54	0000	0	0	.06	.08	.10	.14	.17	.21	.26	.32	.38	.45	.53	.60	.68	.77	.85	.92	.99	1.0	1.1	1.1	1.1	1.1	1.1	1.1	1.1	1		

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.11	.10	.09	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	0	0	0	0
45	.15	.14	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
46	.19	.18	.16	.14	.13	.11	.09	.08	.06	.05	.04	.03	.03	0	0	0	0
47	.25	.23	.21	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	0	0	0	0
48	.31	.29	.26	.23	.20	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	0
49	.39	.35	.32	.29	.25	.22	.19	.16	.13	.11	.09	.07	.05	0	0	0	0
50	.47	.43	.39	.35	.31	.27	.23	.20	.16	.13	.11	.09	.07	0	0	0	0
51	.57	.52	.47	.42	.37	.33	.28	.24	.20	.16	.13	.11	.08	0	0	0	0
52	.68	.62	.56	.50	.45	.39	.33	.28	.24	.19	.16	.13	.10	0	0	0	0
53	.80	.73	.66	.59	.52	.46	.39	.33	.28	.23	.19	.15	.12	0	0	0	0
54	.93	.85	.77	.69	.61	.53	.45	.39	.32	.27	.22	.17	.14	0	0	0	0
55	1.0	.97	.88	.79	.70	.61	.52	.44	.37	.30	.25	.20	.16	0	0	0	0
56	1.2	1.1	1.0	.89	.79	.68	.59	.50	.42	.34	.28	.22	.18	0	0	0	0
57	1.3	1.2	1.1	.99	.88	.76	.66	.56	.47	.38	.31	.25	.20	0	0	0	0
58	1.4	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.28	.22	0	0	0	0
59	1.5	1.4	1.3	1.1	1.0	.91	.78	.66	.56	.46	.37	.30	.24	0	0	0	0
60	1.7	1.5	1.4	1.2	1.1	.98	.84	.71	.60	.49	.40	.32	.25	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0
35	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0
36	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0
37	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0
38	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0
40	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0	0	0	0
41	.02	.01	.01	+	+	+	+	+	+	0	0	0	0	0	0	0	0
42	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
43	.02	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0	0
44	.02	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0	0	0
45	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
46	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0
47	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0
48	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	0	0	0	0
49	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
50	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
51	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
52	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
53	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
54	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
55	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
56	.02	.02	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0
57	.02	.02	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0
58	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0
59	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0
60	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	16.16	0.0000E+00	2323.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
31	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
33	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
34	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
35	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.
36	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.
37	+	+	+	+	+													

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
37	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
38	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
39	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
40	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
41	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
42	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
43	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
44	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
45	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
46	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
47	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
48	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
49	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
50	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
51	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
52	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0
53	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
54	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
55	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
56	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
57	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
58	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
59	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0
60	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.819E+01	1575.	1650.
2.00	0.0	0.164E+00	2625.	1725.
3.00	0.0	0.467E-02	3675.	1800.
4.00	0.0	0.162E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.702E+02	1575.	1650.
2.00	0.0	0.122E+02	2625.	1725.
3.00	0.0	0.299E+01	3675.	1800.
4.00	0.0	0.896E+00	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR PCBs

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.289E-06	0.289E-06	825.	1575.
0.67	0.0	0.162E-06	0.162E-06	1200.	1650.
1.00	0.0	0.985E-07	0.985E-07	1575.	1650.
1.33	0.0	0.625E-07	0.625E-07	1950.	1650.
1.67	0.0	0.428E-07	0.428E-07	2250.	1725.
2.00	0.0	0.306E-07	0.306E-07	2625.	1725.
2.33	0.0	0.224E-07	0.224E-07	3000.	1725.
2.67	0.0	0.169E-07	0.169E-07	3375.	1800.
3.00	0.0	0.131E-07	0.131E-07	3675.	1800.
3.33	0.0	0.103E-07	0.103E-07	4050.	1800.
3.67	0.0	0.830E-08	0.830E-08	4425.	1875.
4.00	0.0	0.676E-08	0.676E-08	4800.	1875.
0.33	6.8	0.107E-05	0.107E-05	825.	1575.
0.67	6.8	0.599E-06	0.599E-06	1200.	1650.
1.00	6.8	0.364E-06	0.364E-06	1575.	1650.
1.33	6.8	0.231E-06	0.231E-06	1950.	1650.
1.67	6.8	0.158E-06	0.158E-06	2250.	1725.
2.00	6.8	0.113E-06	0.113E-06	2625.	1725.
2.33	6.8	0.829E-07	0.829E-07	3000.	1725.
2.67	6.8	0.625E-07	0.625E-07	3375.	1800.
3.00	6.8	0.484E-07	0.484E-07	3675.	1800.
3.33	6.8	0.382E-07	0.382E-07	4050.	1800.
3.67	6.8	0.307E-07	0.307E-07	4425.	1875.
4.00	6.8	0.250E-07	0.250E-07	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF PCBs FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF PCBs IS 0.555000E-04 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.6500000E-05 MG/L.

THE WATER QUALITY STANDARD FOR PCBs IS 0.3000000E-04 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.000	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 72.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 235.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	1) = 123.6	9.291	0.6767E-01	140.1	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	1) = 137.3	9.359	0.5698	2.383	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	1) = 151.3	9.929	0.4586	2.134	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	1) = 163.7	10.39	0.3367	1.710	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	1) = 174.2	10.72	0.2440	1.325	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	1) = 182.8	10.97	0.1815	1.038	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	1) = 190.1	11.15	0.1404	0.8352	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	1) = 196.3	11.29	0.1129	0.6941	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	1) = 201.8	11.40	0.9417E-01	0.5948	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	1) = 206.8	11.50	0.8092E-01	0.5234	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	1) = 207.7	10.19	3.312	847.7	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	2) = 1 123.6	9.291	0.6767E-01	1135.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	2) = 2 137.3	9.359	0.5698	19.31	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	2) = 3 151.3	9.929	0.4586	17.29	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	2) = 4 163.7	10.39	0.3367	13.86	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	2) = 5 174.2	10.72	0.2440	10.74	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	2) = 6 182.8	10.97	0.1815	8.406	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	2) = 7 190.1	11.15	0.1404	6.765	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	2) = 8 196.3	11.29	0.1129	5.626	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	2) = 9 201.8	11.40	0.9417E-01	4.820	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	2) = 10 206.8	11.50	0.8092E-01	4.242	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	2) = 11 207.7	10.19	3.312	6869.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0 1575.	3) = 123.6	9.291	0.6767E-01	446.7	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7 1575.	3) = 137.3	9.359	0.5698	7.601	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5 1575.	3) = 151.3	9.929	0.4586	6.806	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4 1575.	3) = 163.7	10.39	0.3367	5.455	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2 1575.	3) = 174.2	10.72	0.2440	4.227	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1 1575.	3) = 182.8	10.97	0.1815	3.309	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1 1575.	3) = 190.1	11.15	0.1404	2.663	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0 1575.	3) = 196.3	11.29	0.1129	2.214	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0 1575.	3) = 201.8	11.40	0.9417E-01	1.897	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0 1575.	3) = 206.8	11.50	0.8092E-01	1.670	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0 1575.	3) = 207.7	10.19	3.312	2703.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	4) = 123.6	13.50	0.1000E-02	3949.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	4) = 137.3	13.50	0.1000E-02	3128.	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	4) = 151.3	13.50	0.1000E-02	2120.	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	4) = 163.7	13.50	0.1000E-02	1343.	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	4) = 174.2	13.50	0.1000E-02	798.7	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	4) = 182.8	13.50	0.1000E-02	450.2	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	4) = 190.1	13.50	0.1000E-02	243.2	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	4) = 196.3	13.50	0.1000E-02	126.9	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	4) = 201.8	13.50	0.1000E-02	64.40	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	4) = 206.8	13.50	0.1000E-02	31.89	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	4) = 207.7	10.19	3.312	29.13	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	5) = 1 207.7	10.19	3.312	53.85	7.588	235	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.31

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7954.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 55.287

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8039.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.548

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8072.0

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.588	0.0000E+00	435.4	0.0000E+00	13.50
2	1563.	1650.	1.229	0.0000E+00	457.2	0.0000E+00	13.50
3	1563.	1650.	1.037	0.0000E+00	479.1	0.0000E+00	13.50
4	1563.	1650.	0.8205	0.0000E+00	498.2	0.0000E+00	13.50
5	1562.	1650.	0.6312	0.0000E+00	513.9	0.0000E+00	13.50
6	1562.	1650.	0.4945	0.0000E+00	526.7	0.0000E+00	13.50
7	1562.	1650.	0.3970	0.0000E+00	537.4	0.0000E+00	13.50
8	1562.	1650.	0.3360	0.0000E+00	546.5	0.0000E+00	13.50
9	1561.	1650.	0.2856	0.0000E+00	554.5	0.0000E+00	13.50
10	1561.	1650.	0.2423	0.0000E+00	561.7	0.0000E+00	13.50
11	1561.	1650.	15.49	0.0000E+00	562.9	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.1960
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.7505
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5296
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.1
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1077	0.0000E+00	875.0	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.8339E-01	0.0000E+00	903.0	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.7035E-01	0.0000E+00	930.9	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.5566E-01	0.0000E+00	955.0	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.4282E-01	0.0000E+00	974.8	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.3355E-01	0.0000E+00	990.9	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2693E-01	0.0000E+00	1004.	0.0000E+00	13.50	0.100000E-01
8	2634.	1725.	0.2279E-01	0.0000E+00	1016.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1937E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1644E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.051	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.62383
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25442
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10376
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
29	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
32	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
56	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
57	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
58	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
60	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.7308E-02	0.0000E+00	1414.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.5657E-02	0.0000E+00	1447.	0.0000E+00	13.50	0.100000E-01
3	3708.	1801.	0.4772E-02	0.0000E+00	1480.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3776E-02	0.0000E+00	1508.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2905E-02	0.0000E+00	1531.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2276E-02	0.0000E+00	1550.	0.0000E+00	13.50	0.100000E-01
7	3707.	1801.	0.1827E-02	0.0000E+00	1566.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1546E-02	0.0000E+00	1579.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1314E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1115E-02	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7127E-01	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.42318E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17259E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.70389E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4957E-03	0.0000E+00	2037.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.3838E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3237E-03	0.0000E+00	2111.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2561E-03	0.0000E+00	2143.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1970E-03	0.0000E+00	2169.	0.0000E+00	13.50	0.100000E-01
6	4780.	1877.	0.1544E-03	0.0000E+00	2191.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.1239E-03	0.0000E+00	2208.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.1049E-03	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.8914E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.7563E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4835E-02	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.	0	0</												

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1351.5

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 562.96

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2623.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 439.38

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2746.6

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1521.	1647.	109.6	0.0000E+00	435.4	0.0000E+00	0.200000E-02
2	1563.	1650.	4.474	0.0000E+00	457.2	0.0000E+00	0.200000E-02
3	1563.	1650.	3.999	0.0000E+00	479.1	0.0000E+00	0.200000E-02
4	1563.	1650.	3.201	0.0000E+00	498.2	0.0000E+00	0.200000E-02
5	1562.	1650.	2.453	0.0000E+00	513.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.918	0.0000E+00	526.7	0.0000E+00	0.200000E-02
7	1562.	1650.	1.539	0.0000E+00	537.4	0.0000E+00	0.200000E-02
8	1562.	1650.	1.281	0.0000E+00	546.5	0.0000E+00	0.200000E-02
9	1561.	1650.	1.097	0.0000E+00	554.5	0.0000E+00	0.200000E-02
10	1561.	1650.	0.9626	0.0000E+00	561.7	0.0000E+00	0.200000E-02
11	1420.	1640.	308.8	0.0000E+00	562.9	0.2463	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 367.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2818.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 307.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2878.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 257.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2928.5

[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
24	.01	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
26	.02	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
27	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0000
28	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
29	.04	.02	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0000
30	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
31	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
32	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
33	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
34	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
35	.05	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0000
36	.05	.02	.01	+	+	+	+	+										

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2594.	1723.	64.26	0.0000E+00	875.0	0.0000E+00	0.200000E-02
2	2636.	1726.	2.622	0.0000E+00	903.0	0.0000E+00	0.200000E-02
3	2636.	1726.	2.344	0.0000E+00	930.9	0.0000E+00	0.200000E-02
4	2635.	1726.	1.876	0.0000E+00	955.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.438	0.0000E+00	974.8	0.0000E+00	0.200000E-02
6	2635.	1726.	1.124	0.0000E+00	990.9	0.0000E+00	0.200000E-02
7	2635.	1726.	0.9021	0.0000E+00	1004.	0.0000E+00	0.200000E-02
8	2634.	1725.	0.7508	0.0000E+00	1016.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.6427	0.0000E+00	1026.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5642	0.0000E+00	1035.	0.0000E+00	0.200000E-02
11	2493.	1716.	181.0	0.0000E+00	1036.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 215.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2970.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.34
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3005.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 150.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.1

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.13	.11	.08	.06	.04	.03	.02	0	0	0	0	0	0	0	0	0	0
34		.20	.16	.13	.10	.07	.05	.03	0	0	0	0	0	0	0	0	0	0
35		.31	.25	.19	.15	.11	.08	.05	0	0	0	0	0					

[illegible]

0 = .LT. .0000001)

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	00000
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	00000
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	00000
30	.06	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
40	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
43	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
44	.16	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.11	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.10	.08	.06	.04	.03	.02	.01	.	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
54	.05	.04	.03	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	.0000
55	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
56	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3666.	1798.	37.66	0.0000E+00	1414.	0.0000E+00	0.200000E-02
2	3709.	1801.	1.537	0.0000E+00	1447.	0.0000E+00	0.200000E-02
3	3708.	1801.	1.374	0.0000E+00	1480.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.099	0.0000E+00	1508.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.8428	0.0000E+00	1531.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.6587	0.0000E+00	1550.	0.0000E+00	0.200000E-02
7	3707.	1801.	0.5287	0.0000E+00	1566.	0.0000E+00	0.200000E-02
8	3707.	1801.	0.4401	0.0000E+00	1579.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3767	0.0000E+00	1591.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3307	0.0000E+00	1601.	0.0000E+00	0.200000E-02
11	3566.	1791.	106.1	0.0000E+00	1603.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.30
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3059.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3080.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.453
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3096.7

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0	0
43	.12	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0	0
45	.20	.18	.16	.14	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0	0
46	.26	.24	.21	.19	.16	.14	.12	.10	.08	.06	.05	.04	0	0	0	0	0
47	.34	.31	.27	.24	.21	.18	.15	.12	.10	.08	.06	.05	0	0	0	0	0
48	.42	.38	.34	.30	.26	.23	.19	.16	.13	.10	.08	.06	0	0	0	0	0
49	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0	0
50	.64	.58	.52	.46	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	0	0
51	.78	.70	.63	.55	.48	.41	.35	.29	.24	.19	.15	.12	0	0	0	0	0
52	.92	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	0	0	0	0	0
53	1.0	.98	.88	.77	.67	.57	.48	.40	.33	.26	.21	.16	0	0	0	0	0
54	1.2	1.1	1.0	.89	.77	.66	.56	.46	.38	.31	.24	.19	0	0	0	0	0
55	1.4	1.2	1.1	1.0	.88	.75	.63	.53	.43	.35	.28	.22	0	0	0	0	0
56	1.5	1.4	1.2	1.1	.99	.84	.71	.59	.48	.39	.31	.24	0	0	0	0	0
57	1.7	1.6	1.4	1.2	1.0	.93	.79	.65	.53	.43	.34	.27	0	0	0	0	0
58	1.9	1.7	1.5	1.3	1.1	1.0	.86	.71	.58	.47	.37	.29	0	0	0	0	0
59	2.0	1.8	1.6	1.4	1.2	1.0	.92	.76	.62	.50	.40	.31	0	0	0	0	0
60	2.1	1.9	1.7	1.5	1.3	1.1	.97	.81	.66	.53	.42	.33	0	0	0	0	0

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4739.	1874.	22.07	0.0000E+00	2037.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.9008	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8050	0.0000E+00	2111.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6444	0.0000E+00	2143.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4939	0.0000E+00	2169.	0.0000E+00	13.50	0.200000E-02
6	4780.	1877.	0.3861	0.0000E+00	2191.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.3099	0.0000E+00	2208.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2579	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2208	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1938	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
11	4639.	1867.	62.17	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF PCBs

SUMMARY OF PCBs DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.259

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.0	1599.	284.5	238.3	309.5	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.260

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	485.5	439.2	429.3	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.260

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1561.	1650.	814.9	768.6	562.9	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.260

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	1277.	1231.	709.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.260

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2276.	1700.	1896.	1850.	867.2	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.260

MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	2695.	2649.	1036.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	3698.	3651.	1215.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3349.	1776.	4928.	4882.	1404.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

MAX CONC IS 0.00000004 OUTPUT SUPPRESSED AT 0.00 FT

CONCENTRATIONS ABOVE BACKGROUND OF PCBs (MG/L) IN THE CLOUD 10800.00 SECONDS AFTER DUMP

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

...MULTIPLY DISPLAYED VALUES BY 0.1000E-06 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	
3	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
4	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
5	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
6	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
7	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
8	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
9	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
10	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
11	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
12	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
13	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
14	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
15	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
16	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
17	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
18	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
19	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
20	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
21	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
22	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
23	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
24	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
25	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
26	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
27	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
28	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
29	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
30	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
31	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
32	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
33	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
34	0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
35	0000	0	0	0	0	0	0	+	+	+	+	+	.01	.01	.01	.02	.02	.03	.04	.04	.05	.05	.05	.05	.05	.05	.05	.04	.03	
36	0000	0	0	0	0	0	0	+	+	+	+	.01	.01	.02	.02	.03	.04	.05	.06	.06	.07	.08	.08	.08	.08	.08	.07	.06	.05	
37	0000	0	0	0	0	0	0	+	+	+	.01	.01	.02	.03	.04	.05	.06	.07	.08	.10	.11	.11	.12	.12	.12	.11	.11	.10	.08	
38	0000	0	0	0	0	0	0	+	+	.01	.01	.02	.03	.04	.05	.07	.09	.10	.12	.14	.15	.17	.17	.17	.17	.17	.15	.14	.12	
39	0000	0	0	0	0	0	0	+	.01	.01	.02	.03	.04	.06	.08	.10	.12	.15	.17	.20	.22	.23	.24	.24	.24	.23	.22	.20	.17	
40	0000	0	0	0	0	0	0	+	.01	.02	.03	.04	.06	.08	.11	.13	.17	.20	.23	.27	.29	.31	.33	.33	.33	.31	.29	.27	.23	
41	0000	0	0	0	0	0	0	.01	.01	.02	.04	.06	.08	.11	.14	.18	.22	.26	.31	.35	.39	.41	.43	.44	.43	.41	.39	.35	.31	
42	0000	0	0	0	0	0	0	.01	.02	.03	.05	.07	.10	.14	.18	.23	.28	.34	.40	.45	.49	.53	.55	.56	.55	.53	.50	.45	.40	
43	0000	0	0	0	0	0	0	.02	.03	.04	.06	.09	.13	.17	.23	.29	.35	.42	.49	.56	.62	.66	.69	.70	.69	.66	.62	.56	.50	
44	0000	0	0	0	0	0	0	.02	.03	.05	.08	.11	.16	.21	.27	.35	.43	.51	.60	.68	.75	.80	.84	.85	.84	.80	.75	.68	.60	
45	0000	0	0	0	0	0	0	.02	.04	.06	.09	.13	.18	.25	.32	.41	.50	.61	.70	.80	.88	.94	.98	1.0	.99	.95	.88	.80	.71	
46	0000	0	0	0	0	0	0	.03	.05	.07	.11	.15	.21	.28	.37	.47	.58	.69	.81	.92	1.0	1.0	1.1	1.1	1.1	1.0	1.0	.92	.81	
47	0000	0	0	0	0	0	0	.03	.05	.08	.12	.17	.24	.32	.41	.52	.65	.77	.90	1.0	1.1	1.2	1.2	1.2	1.2	1.2	1.1	1.0	.90	
48	0000	0	0	0	0	0	0	.04	.06	.09	.13	.19	.26	.34	.45	.57	.70	.84	.98	1.1	1.2	1.3	1.3	1.3	1.3	1.3	1.2	1.1	.98	
49	0000	0	0	0	0	0	0	.04	.06	.09	.14	.20	.27	.36	.47	.60	.74	.88	1.0	1.1	1.2	1.3	1.4	1.4	1.4	1.3	1.2	1.1	.89	
50	0000	0	0	0	0	0	0	.04	.06	.10	.14	.20	.28	.37	.49	.62	.76	.91	1.0	1.2	1.3	1.4	1.4	1.5	1.4	1.4	1.3	1.2	1.0	
51	0000	0	0	0	0	0	0	.04	.06	.10	.14	.20	.28	.37	.48	.61	.76	.91	1.0	1.1	1.3	1.4	1.4	1.4	1.4	1.4	1.3	1.2	1.0	
52	0000	0	0	0	0	0	0	.04	.06	.09	.14	.19	.27	.36	.47	.60	.73	.88	1.0	1.1	1.2	1.3	1.4	1.4	1.4	1.3	1.2	1.1	.88	
53	0000	0	0	0	0	0	0	.04	.06	.09	.13	.18	.25	.34	.44	.56	.69	.83	.97	1.0	1.2	1.2	1.3	1.3	1.3	1.3	1.2	1.1	.97	
54	0000	0	0	0	0	0	0	.03	.05	.08	.12	.17	.23	.31	.41	.52	.64	.76	.89	1.0	1.1	1.1	1.2	1.2	1.2	1.1	1.1	1.0	.89	
55	0000	0	0	0	0	0	0	.03	.05	.07	.10	.15	.21	.28	.36	.46	.57	.68	.79	.90	.99	1.0	1.1	1.1	1.1	1.0	.99	.90	.80	
56	0000	0	0	0	0	0	0	.02	.04	.06	.09	.13	.18	.24	.32	.40	.49	.59	.69	.78	.86	.92	.96	.98	.96	.92	.86	.78	.69	

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3707.	1801.	6410.	6364.	1603.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4064.	1826.	8168.	8122.	1810.	0.00000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.1023E+05	0.1018E+05	2026.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF PCBs DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 46.261

MAX CONC IS 0.00000002 OUTPUT SUPPRESSED AT 0.00 FT

MAX CONC IS 0.00000008 OUTPUT SUPPRESSED AT 6.75 FT

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.29	.27	.24	.21	.18	.16	.13	.11	.09	.07	.06	.05	0	0	0	0	0
45	.39	.35	.32	.28	.25	.21	.18	.15	.12	.10	.08	.06	0	0	0	0	0
46	.51	.46	.42	.37	.32	.28	.24	.20	.16	.13	.11	.08	0	0	0	0	0
47	.66	.60	.54	.48	.42	.36	.31	.26	.21	.17	.14	.11	0	0	0	0	0
48	.84	.77	.69	.61	.54	.46	.39	.33	.27	.22	.18	.14	0	0	0	0	0
49	1.0	.96	.87	.77	.67	.58	.49	.41	.34	.28	.22	.18	0	0	0	0	0
50	1.3	1.1	1.0	.95	.83	.72	.61	.51	.42	.35	.28	.22	0	0	0	0	0
51	1.5	1.4	1.3	1.1	1.0	.88	.75	.63	.52	.42	.34	.27	0	0	0	0	0
52	1.9	1.7	1.5	1.4	1.2	1.0	.90	.76	.62	.51	.41	.32	0	0	0	0	0
53	2.2	2.0	1.8	1.6	1.4	1.2	1.0	.90	.74	.61	.49	.39	0	0	0	0	0
54	2.6	2.4	2.1	1.9	1.7	1.4	1.2	1.0	.87	.71	.57	.45	0	0	0	0	0
55	3.0	2.8	2.5	2.2	1.9	1.6	1.4	1.2	1.0	.82	.66	.52	0	0	0	0	0
56	3.4	3.1	2.8	2.5	2.2	1.9	1.6	1.3	1.1	.93	.75	.59	0	0	0	0	0
57	3.9	3.5	3.2	2.8	2.5	2.1	1.8	1.5	1.2	1.0	.84	.67	0	0	0	0	0
58	4.3	3.9	3.5	3.1	2.7	2.3	2.0	1.7	1.4	1.1	.93	.74	0	0	0	0	0
59	4.7	4.3	3.8	3.4	3.0	2.6	2.2	1.8	1.5	1.2	1.0	.81	0	0	0	0	0
60	5.0	4.6	4.1	3.7	3.2	2.8	2.3	2.0	1.6	1.3	1.0	.87	0	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.03	+	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.04	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.04	.03	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0
39	.05	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0	0
40	.06	.04	.02	.01	.01	+	+	+	0	0	0	0	0	0	0	0	0
41	.06	.04	.02	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0
42	.06	.04	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
43	.06	.04	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
44	.07	.05	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0
45	.07	.05	.04	.02	.01	.01	+	+	+	+	+	0	0	0	0	0	0
46	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
47	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
48	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0	0	0	0	0
49	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	0	0
50	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	0	0
51	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	0	0	0	0	0
52	.07	.06	.04	.03	.03	.02	.01	.01	+	+	+	+	0	0	0	0	0
53	.07	.05	.04	.04	.03	.02	.01	.01	.01	+	+	+	0	0	0	0	0
54	.07	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0	0
55	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	0	0	0	0	0
56	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	0	0	0	0	0
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	0	0	0	0	0
58	.06	.05	.05	.04	.03	.03	.02	.01	.01	.01	+	+	0	0	0	0	0
59	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0
60	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR PCBs

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.1261E+05	0.1256E+05	2250.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.		0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.		0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.		0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.		0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	.		0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	.	.		0	0	0	0	0	0	0	0	0
24	+	+	+	+	.	.	.	.	.		0	0	0	0	0	0	0	0
25	+	+	+	+	.	.	.	.	.	.		0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	.	.	.		0	0	0	0	0	0
27	+	+	+	+	+	.	.	.	.	.	.	.		0	0	0	0	0
28	+	+	+	+	+	.	.	.	.	.	.	.	.		0	0	0	0
29	+	+	+	+	+	+	.	.	.	.	.	.	.	.		0	0	0
30	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.		0	0
31	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.		0
32	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.
33	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.
34	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
35	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
36	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.
37	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.
38	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.
39	.01																	

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.259E+00	2625.	1725.
3.00	0.0	0.718E-02	3675.	1800.
4.00	0.0	0.245E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.442E+02	2550.	1725.
3.00	0.0	0.106E+02	3600.	1800.
4.00	0.0	0.312E+01	4650.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR PCBs

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.102E-05	0.752E-05	825.	1575.
0.67	0.0	0.555E-06	0.705E-05	1200.	1650.
1.00	0.0	0.329E-06	0.683E-05	1575.	1650.
1.33	0.0	0.204E-06	0.670E-05	1950.	1650.
1.67	0.0	0.138E-06	0.664E-05	2250.	1725.
2.00	0.0	0.973E-07	0.660E-05	2625.	1725.
2.33	0.0	0.706E-07	0.657E-05	3000.	1725.
2.67	0.0	0.528E-07	0.655E-05	3375.	1800.
3.00	0.0	0.406E-07	0.654E-05	3675.	1800.
3.33	0.0	0.319E-07	0.653E-05	4050.	1800.
3.67	0.0	0.254E-07	0.653E-05	4425.	1875.
4.00	0.0	0.206E-07	0.652E-05	4800.	1875.
0.33	6.8	0.377E-05	0.103E-04	825.	1575.
0.67	6.8	0.205E-05	0.855E-05	1200.	1650.
1.00	6.8	0.121E-05	0.771E-05	1575.	1650.
1.33	6.8	0.753E-06	0.725E-05	1950.	1650.
1.67	6.8	0.508E-06	0.701E-05	2250.	1725.
2.00	6.8	0.360E-06	0.686E-05	2625.	1725.
2.33	6.8	0.261E-06	0.676E-05	3000.	1725.
2.67	6.8	0.195E-06	0.670E-05	3375.	1800.
3.00	6.8	0.150E-06	0.665E-05	3675.	1800.
3.33	6.8	0.118E-06	0.662E-05	4050.	1800.
3.67	6.8	0.940E-07	0.659E-05	4425.	1875.
4.00	6.8	0.763E-07	0.658E-05	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED			
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)	
1200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
2400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
3600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
4800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
6000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
7200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
8400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
9600.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
10800.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
12000.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
13200.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	
14400.0	0.000000E+00	0.	0.	0.000000E+00	0.	0.	

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF DDx FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF DDx IS 1.68000 MG/L
AND ITS BACKGROUND CONCENTRATION IS 1.300000 MG/L.

THE WATER QUALITY STANDARD FOR DDx IS 1.000000 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	1) = 1 143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	1) = 2 159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	1) = 3 171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	1) = 4 181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	1) = 5 189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	1) = 6 195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	1) = 7 201.6	11.25	0.9467E-01	2.327	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	1) = 8 206.7	11.34	0.7957E-01	2.003	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	1) = 9 211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	1) = 10 215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	2) = 1 143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	2) = 2 159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	2) = 3 171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	2) = 4 181.1	10.80	0.1911	7.461	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	2) = 5 189.1	10.99	0.1448	5.884	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	2) = 6 195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	2) = 7 201.6	11.25	0.9467E-01	4.083	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	2) = 8 206.7	11.34	0.7957E-01	3.512	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	2) = 9 211.1	11.42	0.6810E-01	3.066	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	2) = 10 215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	3) = 143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	3) = 159.3	10.08	0.4471	6.960	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	3) = 171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	3) = 181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	3) = 189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	3) = 195.8	11.13	0.1152	2.190	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	3) = 201.6	11.25	0.9467E-01	1.849	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	3) = 206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	3) = 211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	3) = 215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	500.3 1575.	4) = 1 143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	500.2 1575.	4) = 2 159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	500.2 1575.	4) = 3 171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	500.2 1575.	4) = 4 181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	500.2 1575.	4) = 5 189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	500.2 1575.	4) = 6 195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	500.2 1575.	4) = 7 201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	500.2 1575.	4) = 8 206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	500.2 1575.	4) = 9 211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2 1575.	4) = 10 215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	500.2	1575.	5) = 1 215.1	10.07	3.431	0.3082E+07	0.1906E+07	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 144.63

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7091.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.868

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7178.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.601

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7212.4

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	3.674	0.0000E+00	466.9	0.0000E+00	13.50
2	1564.	1650.	0.9189	0.0000E+00	491.6	0.0000E+00	13.50
3	1564.	1650.	0.6027	0.0000E+00	509.9	0.0000E+00	13.50
4	1564.	1650.	0.4163	0.0000E+00	524.4	0.0000E+00	13.50
5	1564.	1650.	0.3492	0.0000E+00	536.2	0.0000E+00	13.50
6	1563.	1650.	0.2863	0.0000E+00	546.1	0.0000E+00	13.50
7	1563.	1650.	0.2448	0.0000E+00	554.5	0.0000E+00	13.50
8	1563.	1650.	0.2099	0.0000E+00	561.8	0.0000E+00	13.50
9	1563.	1650.	0.1815	0.0000E+00	568.2	0.0000E+00	13.50
10	1563.	1650.	16.72	0.0000E+00	573.9	0.0000E+00	13.50

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.6253
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9256
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6010
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.4
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

BOTTOM ACCUMULATION OF Silt (CU FT/GRID SQUARE) , 7200.00 SECONDS AFTER DUMP

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...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
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[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
21		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
22		+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
24		+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
25		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
26		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
27		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
28		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0000
29		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
30		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0000
31		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0000
32		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
33		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
34		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
35		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
36		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.2492	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2637.	1726.	0.6233E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2637.	1726.	0.4089E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2636.	1726.	0.2824E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2636.	1726.	0.2369E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2636.	1726.	0.1942E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2636.	1726.	0.1660E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2636.	1726.	0.1424E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2636.	1726.	0.1231E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2636.	1726.	1.134	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65294
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26630
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10861
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
32	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
56	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
57	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
58	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
60	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3710.	1801.	0.1691E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	3710.	1801.	0.4229E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.2774E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	3709.	1801.	0.1916E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	3709.	1801.	0.1607E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	3709.	1801.	0.1317E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	3709.	1801.	0.1126E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	3709.	1801.	0.9658E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	3709.	1801.	0.8352E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	3709.	1801.	0.7693E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44293E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18065E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73674E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT


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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.1147E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2869E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	4782.	1877.	0.1882E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	4782.	1877.	0.1300E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	4782.	1877.	0.1090E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	4782.	1877.	0.8937E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	4782.	1877.	0.7641E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	4782.	1877.	0.6552E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	4782.	1877.	0.5666E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	4782.	1877.	0.5219E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1419.2

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1858.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 611.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2665.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 484.33

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2793.5

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1548.	1649.	134.9	0.0000E+00	466.9	0.0000E+00	0.200000E-02
2	1564.	1650.	4.086	0.0000E+00	491.6	0.0000E+00	0.200000E-02
3	1564.	1650.	2.691	0.0000E+00	509.9	0.0000E+00	0.200000E-02
4	1564.	1650.	1.960	0.0000E+00	524.4	0.0000E+00	0.200000E-02
5	1564.	1650.	1.544	0.0000E+00	536.2	0.0000E+00	0.200000E-02
6	1563.	1650.	1.266	0.0000E+00	546.1	0.0000E+00	0.200000E-02
7	1563.	1650.	1.070	0.0000E+00	554.5	0.0000E+00	0.200000E-02
8	1563.	1650.	0.9198	0.0000E+00	561.8	0.0000E+00	0.200000E-02
9	1563.	1650.	0.8021	0.0000E+00	568.2	0.0000E+00	0.200000E-02
10	1433.	1641.	335.1	0.0000E+00	573.9	0.1115	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 405.31
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2872.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 339.19
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2938.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 283.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2993.9

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

0 = .LT. .000001)

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
19		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
20		+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21		+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
26	.02	.01	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
27	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
29	.05	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
30	.06	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
31	.06	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
32	.07	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
33	.07	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
34	.07	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
35	.07	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
36	.06	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
37	.05	.03	.01	+	+	+	+	+	.	.	.	.	.	0	0	0		

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2621.	1724.	79.04	0.0000E+00	915.3	0.0000E+00	0.200000E-02
2	2637.	1726.	2.395	0.0000E+00	946.7	0.0000E+00	0.200000E-02
3	2637.	1726.	1.577	0.0000E+00	969.8	0.0000E+00	0.200000E-02
4	2636.	1726.	1.149	0.0000E+00	987.9	0.0000E+00	0.200000E-02
5	2636.	1726.	0.9049	0.0000E+00	1003.	0.0000E+00	0.200000E-02
6	2636.	1726.	0.7418	0.0000E+00	1015.	0.0000E+00	0.200000E-02
7	2636.	1726.	0.6271	0.0000E+00	1026.	0.0000E+00	0.200000E-02
8	2636.	1726.	0.5391	0.0000E+00	1035.	0.0000E+00	0.200000E-02
9	2636.	1726.	0.4701	0.0000E+00	1043.	0.0000E+00	0.200000E-02
10	2505.	1716.	196.4	0.0000E+00	1050.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 237.55
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3040.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 198.79
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3079.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 166.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3111.4

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.14	.12	.09	.07	.05	.03	.02	0	0	0	0	0	0	0	0	0	0
34		.22	.18	.14	.11	.08	.06	.04	0	0	0	0	0	0	0	0	0	0
35		.33	.27	.21	.16	.12	.09	.06	0	0	0	0	0					

[illegible]

(CU FT/GRID SQUARE) , 10800.00 SECONDS AFTER DUMP

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	00000
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	00000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	00000
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.13	.08	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.15	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.17	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.17	.12	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	.0000
40	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
41	.18	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.17	.13	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.17	.12	.09	.06	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.16	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.14	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.13	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
51	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
52	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
53	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
54	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
56	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
57	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.0000
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.0000
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3694. 1800.	46.32	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	3710. 1801.	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	0.9242	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	3709. 1801.	0.6733	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	3709. 1801.	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	3709. 1801.	0.4348	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	3709. 1801.	0.3675	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	3709. 1801.	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	3709. 1801.	0.2755	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	3578. 1792.	115.1	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 139.22
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3138.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 116.51
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3160.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 97.504
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3179.3

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.09	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0
43	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
44	.17	.15	.14	.12	.10	.09	.08	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.22	.20	.18	.16	.14	.12	.10	.08	.07	.05	.04	.03	.02	0	0	0	0
46	.29	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
47	.36	.33	.30	.26	.23	.20	.17	.14	.11	.09	.07	.06	.04	0	0	0	0
48	.46	.42	.37	.33	.29	.25	.21	.17	.14	.11	.09	.07	.05	0	0	0	0
49	.57	.51	.46	.41	.36	.31	.26	.22	.18	.14	.11	.09	.07	0	0	0	0
50	.69	.63	.56	.50	.43	.37	.32	.26	.22	.17	.14	.11	.08	0	0	0	0
51	.83	.76	.68	.60	.52	.45	.38	.32	.26	.21	.17	.13	.10	0	0	0	0
52	.99	.90	.81	.71	.62	.53	.45	.38	.31	.25	.20	.16	.12	0	0	0	0
53	1.1	1.0	.94	.83	.73	.62	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
54	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.21	.16	0	0	0	0
55	1.5	1.3	1.2	1.0	.95	.82	.69	.58	.48	.39	.31	.24	.19	0	0	0	0
56	1.7	1.5	1.3	1.2	1.0	.92	.78	.65	.53	.43	.34	.27	.21	0	0	0	0
57	1.8	1.7	1.5	1.3	1.1	1.0	.86	.72	.59	.48	.38	.30	.23	0	0	0	0
58	2.0	1.8	1.6	1.4	1.2	1.1	.94	.78	.64	.52	.42	.33	.25	0	0	0	0
59	2.2	2.0	1.8	1.5	1.3	1.1	1.0	.84	.69	.56	.45	.35	.27	0	0	0	0
60	2.3	2.1	1.9	1.6	1.4	1.2	1.0	.89	.73	.59	.47	.37	.29	0	0	0	0

[illegible]

```
001    0 = .LT. .0000001)
```

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4767.	1876.	27.15	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.8226	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	4782.	1877.	0.5417	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	4782.	1877.	0.3946	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	4782.	1877.	0.3108	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	4782.	1877.	0.2548	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	4782.	1877.	0.2154	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	4782.	1877.	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	4782.	1877.	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	4651.	1868.	67.47	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.07	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.14	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
36	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.16	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
38	.17	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.18	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.19	.13	.09	.06	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.20	.14	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.20	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.20	.15	.11	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.21	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.21	.16	.12	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+0000
46	.21	.16	.12	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.21	.16	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.21	.16	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
51	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.19	.16	.13	.10	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.18	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
54	.18	.15	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
55	.17	.14	.12	.10	.08	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
56	.16	.14	.12	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
57	.16	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.15	.13	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000

[illegible]

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF DDx

SUMMARY OF DDx DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11759E+07

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	847.9	1600.	0.5161E+08	0.5044E+08	318.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11759E+07

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1206.	1625.	0.9311E+08	0.9194E+08	439.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11759E+07

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1563.	1650.	0.1609E+09	0.1597E+09	573.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11759E+07

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1921.	1675.	0.2556E+09	0.2545E+09	721.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11758E+07

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2278.	1700.	0.3820E+09	0.3809E+09	880.0	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11759E+07

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2636.	1726.	0.5448E+09	0.5436E+09	1050.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11727E+07

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2994.	1751.	0.7488E+09	0.7476E+09	1230.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11727E+07

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3351.	1776.	0.9986E+09	0.9974E+09	1420.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11726E+07

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3709.	1801.	0.1299E+10	0.1298E+10	1619.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11726E+07

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4066.	1826.	0.1655E+10	0.1654E+10	1827.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11726E+07

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4424.	1852.	0.2072E+10	0.2071E+10	2043.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.11725E+07

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.20	.19	.17	.15	.13	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	0
45	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
46	.35	.32	.29	.26	.23	.20	.17	.14	.12	.09	.07	.06	.04	0	0	0	0
47	.46	.42	.38	.33	.29	.25	.22	.18	.15	.12	.10	.08	.06	0	0	0	0
48	.58	.53	.48	.43	.37	.32	.27	.23	.19	.16	.12	.10	.08	0	0	0	0
49	.73	.66	.60	.53	.47	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	0
50	.90	.82	.74	.66	.58	.50	.43	.36	.30	.24	.19	.15	.12	0	0	0	0
51	1.0	1.0	.90	.80	.70	.61	.52	.44	.36	.30	.24	.19	.15	0	0	0	0
52	1.3	1.2	1.0	.96	.85	.73	.62	.52	.44	.36	.29	.23	.18	0	0	0	0
53	1.5	1.4	1.2	1.1	1.0	.87	.74	.62	.52	.42	.34	.27	.21	0	0	0	0
54	1.8	1.6	1.5	1.3	1.1	1.0	.86	.73	.60	.49	.40	.32	.25	0	0	0	0
55	2.0	1.9	1.7	1.5	1.3	1.1	.99	.84	.69	.57	.46	.36	.29	0	0	0	0
56	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.95	.79	.65	.52	.41	.33	0	0	0	0
57	2.6	2.4	2.2	1.9	1.7	1.4	1.2	1.0	.89	.72	.58	.47	.36	0	0	0	0
58	2.9	2.6	2.4	2.1	1.8	1.6	1.4	1.1	.98	.80	.65	.51	.40	0	0	0	0
59	3.2	2.9	2.6	2.3	2.0	1.7	1.5	1.2	1.0	.87	.71	.56	.44	0	0	0	0
60	3.4	3.1	2.8	2.5	2.2	1.9	1.6	1.3	1.1	.94	.76	.60	.47	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.07	.07	.06	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0
45	.10	.09	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0
46	.13	.12	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
47	.17	.15	.14	.12	.11	.09	.08	.06	.05	.04	.03	.03	.02	0	0	0	0
48	.21	.19	.17	.15	.13	.12	.10	.08	.07	.05	.04	.03	.03	0	0	0	0
49	.27	.24	.22	.19	.17	.15	.12	.10	.09	.07	.05	.04	.03	0	0	0	0
50	.33	.30	.27	.24	.21	.18	.15	.13	.11	.09	.07	.05	.04	0	0	0	0
51	.40	.37	.33	.29	.26	.22	.19	.16	.13	.11	.08	.07	.05	0	0	0	0
52	.48	.44	.40	.35	.31	.27	.23	.19	.16	.13	.10	.08	.06	0	0	0	0
53	.57	.52	.47	.42	.37	.32	.27	.23	.19	.15	.12	.10	.07	0	0	0	0
54	.67	.61	.55	.49	.43	.37	.32	.27	.22	.18	.14	.11	.09	0	0	0	0
55	.77	.70	.63	.56	.49	.43	.36	.31	.25	.21	.17	.13	.10	0	0	0	0
56	.87	.80	.72	.64	.56	.49	.41	.35	.29	.24	.19	.15	.12	0	0	0	0
57	.98	.90	.81	.72	.63	.55	.47	.39	.32	.26	.21	.17	.13	0	0	0	0
58	1.0	.99	.89	.79	.70	.60	.51	.43	.36	.29	.24	.19	.15	0	0	0	0
59	1.1	1.0	.97	.87	.76	.66	.56	.47	.39	.32	.26	.20	.16	0	0	0	0
60	1.2	1.1	1.0	.93	.82	.71	.60	.51	.42	.34	.28	.22	.17	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.03	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.04	.01	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.06	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.08	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.09	.03	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.11	.04	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.11	.06	.04	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.11	.07	.05	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0
38	.13	.09	.06	.02	.01	+	+	+	0	0	0	0	0	0	0	0	0
39	.15	.10	.06	.03	.02	+	+	+	0	0	0	0	0	0	0	0	0
40	.16	.11	.07	.04	.02	.01	+	+	+	0	0	0	0	0	0	0	0
41	.16	.11	.07	.05	.03	.01	.01	+	+	+	+	0	0	0	0	0	0
42	.16	.11	.08	.05	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
43	.16	.12	.09	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
44	.18	.13	.10	.07	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0
45	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0
46	.18	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	0	0	0	0
47	.18	.13	.10	.08	.06	.04	.03	.01	.01	+	+	+	+	0	0	0	0
48	.17	.14	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	0	0	0	0
49	.18	.15	.12	.09	.07	.05	.03	.02	.02	.01	+	+	+	0	0	0	0
50	.19	.15	.12	.09	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
51	.19	.15	.12	.09	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
52	.18	.15	.12	.09	.07	.06	.04	.03	.02	.01	.01	+	+	0	0	0	0
53	.17	.14	.12	.10	.08	.06	.05	.03	.02	.02	.01	.01	+	0	0	0	0
54	.18	.15	.13	.10	.08	.06	.05	.04	.03	.02	.01	.01	+	0	0	0	0
55	.18	.15	.13	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	0	0	0	0
56	.18	.15	.13	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
57	.17	.15	.12	.10	.08	.07	.06	.04	.03	.02	.02	.01	.01	0	0	0	0
58	.16	.14	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	0	0	0	0
59	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
60	.16	.14	.13	.11	.09	.07	.06	.05	.04	.03	.02	.02	.01	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4782.	1877.	0.2553E+10	0.2552E+10	2268.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
25	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
27	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
28	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
29	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
30	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
31	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0
32	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
33	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
34	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
35	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
36	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
37	.01	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
38	.01	.01	+	+	+	+												

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.263E+00	2625.	1725.
3.00	0.0	0.735E-02	3675.	1800.
4.00	0.0	0.252E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.255E+03	1500.	1650.
2.00	0.0	0.467E+02	2550.	1725.
3.00	0.0	0.114E+02	3600.	1800.
4.00	0.0	0.336E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR DDx

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.245E-01	0.132E+01	825.	1575.
0.67	0.0	0.135E-01	0.131E+01	1200.	1650.
1.00	0.0	0.805E-02	0.131E+01	1575.	1650.
1.33	0.0	0.502E-02	0.131E+01	1950.	1650.
1.67	0.0	0.339E-02	0.130E+01	2250.	1725.
2.00	0.0	0.241E-02	0.130E+01	2625.	1725.
2.33	0.0	0.175E-02	0.130E+01	3000.	1725.
2.67	0.0	0.131E-02	0.130E+01	3375.	1800.
3.00	0.0	0.101E-02	0.130E+01	3675.	1800.
3.33	0.0	0.793E-03	0.130E+01	4050.	1800.
3.67	0.0	0.634E-03	0.130E+01	4425.	1875.
4.00	0.0	0.515E-03	0.130E+01	4800.	1875.
0.33	6.8	0.904E-01	0.139E+01	825.	1575.
0.67	6.8	0.498E-01	0.135E+01	1200.	1650.
1.00	6.8	0.297E-01	0.133E+01	1575.	1650.
1.33	6.8	0.185E-01	0.132E+01	1950.	1650.
1.67	6.8	0.125E-01	0.131E+01	2250.	1725.
2.00	6.8	0.891E-02	0.131E+01	2625.	1725.
2.33	6.8	0.646E-02	0.131E+01	3000.	1725.
2.67	6.8	0.484E-02	0.130E+01	3375.	1800.
3.00	6.8	0.373E-02	0.130E+01	3675.	1800.
3.33	6.8	0.293E-02	0.130E+01	4050.	1800.
3.67	6.8	0.234E-02	0.130E+01	4425.	1875.
4.00	6.8	0.190E-02	0.130E+01	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
2400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
3600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
4800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
6000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
7200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
8400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
9600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
10800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
12000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
13200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
14400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF DDx FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF DDx IS 1.68000 MG/L
AND ITS BACKGROUND CONCENTRATION IS 1.300000 MG/L.

THE WATER QUALITY STANDARD FOR DDx IS 1.000000 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	1) = 197.4	10.91	0.2177	34.30	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	1) = 224.8	11.43	0.1157	20.28	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	1) = 232.3	11.55	0.9997E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	2) = 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	2) = 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	2) = 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	2) = 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	2) = 185.6	10.61	0.2974	8.984	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	2) = 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	2) = 207.6	11.12	0.1689	5.614	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	2) = 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	2) = 224.8	11.43	0.1157	4.102	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	2) = 232.3	11.55	0.9997E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	2) = 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	500.1	1575.	3) = 113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.8	1575.	3) = 134.8	8.477	1.036	9.913	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	499.6	1575.	3) = 154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	499.5	1575.	3) = 171.6	10.18	0.4327	5.259	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	499.5	1575.	3) = 185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	499.5	1575.	3) = 197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	499.5	1575.	3) = 207.6	11.12	0.1689	2.428	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	499.5	1575.	3) = 216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	499.5	1575.	3) = 224.8	11.43	0.1157	1.773	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	499.5	1575.	3) = 232.3	11.55	0.9997E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	3) = 233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	499.5	1575.	4) = 1 233.4	9.779	3.721	0.3715E+07	0.2987E+07	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 167.52

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5902.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.559

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6002.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.553

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6042.0

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	2.333	0.0000E+00	419.0	0.0000E+00	0.100000E-01
2	1563.	1650.	1.539	0.0000E+00	453.4	0.0000E+00	0.100000E-01
3	1563.	1650.	1.101	0.0000E+00	484.4	0.0000E+00	0.100000E-01
4	1563.	1650.	0.7476	0.0000E+00	510.1	0.0000E+00	0.100000E-01
5	1563.	1650.	0.5443	0.0000E+00	531.0	0.0000E+00	0.100000E-01
6	1562.	1650.	0.4158	0.0000E+00	548.3	0.0000E+00	0.100000E-01
7	1562.	1650.	0.3351	0.0000E+00	563.0	0.0000E+00	0.100000E-01
8	1562.	1650.	0.2858	0.0000E+00	576.0	0.0000E+00	0.100000E-01
9	1562.	1650.	0.2452	0.0000E+00	587.6	0.0000E+00	0.100000E-01
10	1562.	1650.	0.2115	0.0000E+00	598.2	0.0000E+00	0.100000E-01
11	1562.	1650.	19.79	0.0000E+00	599.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.237
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6058.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.5829
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6065.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.8691
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.7

[illegible]

[illegible]

[illegible]

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible][illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
25	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
28	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0000
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0000
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0000
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0000
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0		

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1583	0.0000E+00	853.9	0.0000E+00	0.100000E-01
2	2636.	1726.	0.1044	0.0000E+00	898.1	0.0000E+00	0.100000E-01
3	2636.	1726.	0.7469E-01	0.0000E+00	937.5	0.0000E+00	0.100000E-01
4	2636.	1726.	0.5071E-01	0.0000E+00	970.0	0.0000E+00	0.100000E-01
5	2635.	1726.	0.3693E-01	0.0000E+00	996.2	0.0000E+00	0.100000E-01
6	2635.	1726.	0.2821E-01	0.0000E+00	1018.	0.0000E+00	0.100000E-01
7	2635.	1725.	0.2273E-01	0.0000E+00	1036.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.1939E-01	0.0000E+00	1052.	0.0000E+00	0.100000E-01
9	2635.	1725.	0.1663E-01	0.0000E+00	1067.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1435E-01	0.0000E+00	1080.	0.0000E+00	0.100000E-01
11	2634.	1725.	1.343	0.0000E+00	1082.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76229
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31089
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12679
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

0 = .LT. .000001)

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
23	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
25	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
28	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
31	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
32	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
34	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
35	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
36	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	00000
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
55	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
56	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
57	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	00000
58	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	00000
59	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	00000
60	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	00000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	0.1074E-01	0.0000E+00	1389.	0.0000E+00	13.50	0.100000E-01
2	3709. 1801.	0.7081E-02	0.0000E+00	1441.	0.0000E+00	13.50	0.100000E-01
3	3709. 1801.	0.5067E-02	0.0000E+00	1487.	0.0000E+00	13.50	0.100000E-01
4	3708. 1801.	0.3440E-02	0.0000E+00	1526.	0.0000E+00	13.50	0.100000E-01
5	3708. 1801.	0.2505E-02	0.0000E+00	1556.	0.0000E+00	13.50	0.100000E-01
6	3708. 1801.	0.1913E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
7	3708. 1801.	0.1542E-02	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01
8	3708. 1801.	0.1315E-02	0.0000E+00	1622.	0.0000E+00	13.50	0.100000E-01
9	3707. 1801.	0.1128E-02	0.0000E+00	1638.	0.0000E+00	13.50	0.100000E-01
10	3707. 1801.	0.9735E-03	0.0000E+00	1654.	0.0000E+00	13.50	0.100000E-01
11	3707. 1801.	0.9109E-01	0.0000E+00	1656.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.51711E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21090E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.86012E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.7283E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.4803E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3437E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2334E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1699E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1298E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1046E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.8922E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7655E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6604E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.6179E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.														

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1232.1

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1392.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 435.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2189.1

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

3600.00 SECONDS AFTER DUMP

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	112.6	0.0000E+00	419.0	0.0000E+00	0.200000E-02
2	1563.	1650.	5.895	0.0000E+00	453.4	0.0000E+00	0.200000E-02
3	1563.	1650.	4.298	0.0000E+00	484.4	0.0000E+00	0.200000E-02
4	1563.	1650.	3.093	0.0000E+00	510.1	0.0000E+00	0.200000E-02
5	1563.	1650.	2.260	0.0000E+00	531.0	0.0000E+00	0.200000E-02
6	1562.	1650.	1.742	0.0000E+00	548.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.388	0.0000E+00	563.0	0.0000E+00	0.200000E-02
8	1562.	1650.	1.183	0.0000E+00	576.0	0.0000E+00	0.200000E-02
9	1562.	1650.	1.025	0.0000E+00	587.6	0.0000E+00	0.200000E-02
10	1562.	1650.	0.9074	0.0000E+00	598.2	0.0000E+00	0.200000E-02
11	1438.	1641.	300.8	0.0000E+00	599.8	0.3251E-01	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 364.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2260.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.85
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2319.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 255.11
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2369.3

[illegible]

[illegible]

7200.00 SECONDS AFTER DUMP

0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	66.02	0.0000E+00	853.9	0.0000E+00	0.200000E-02
2	2636.	1726.	3.455	0.0000E+00	898.1	0.0000E+00	0.200000E-02
3	2636.	1726.	2.519	0.0000E+00	937.5	0.0000E+00	0.200000E-02
4	2636.	1726.	1.813	0.0000E+00	970.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.324	0.0000E+00	996.2	0.0000E+00	0.200000E-02
6	2635.	1726.	1.021	0.0000E+00	1018.	0.0000E+00	0.200000E-02
7	2635.	1725.	0.8135	0.0000E+00	1036.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.6936	0.0000E+00	1052.	0.0000E+00	0.200000E-02
9	2635.	1725.	0.6010	0.0000E+00	1067.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5318	0.0000E+00	1080.	0.0000E+00	0.200000E-02
11	2511.	1717.	176.3	0.0000E+00	1082.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2410.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.67
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2445.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.52
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2474.9

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33		.14	.11	.09	.07	.05	.04	.02	0	0	0	0	0	0	0	0	0	00000
34		.21	.17	.13	.10	.08	.06	.04	0	0	0	0	0					

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
23	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
24	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	00000
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	00000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.0000
39	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
40	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
43	.16	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
44	.16	.12	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.08	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.12	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
54	.06	.04	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
55	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+0000
56	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.0000
59	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
60	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	38.69	0.0000E+00	1389.	0.0000E+00	0.200000E-02
2	3709.	1801.	2.025	0.0000E+00	1441.	0.0000E+00	0.200000E-02
3	3709.	1801.	1.476	0.0000E+00	1487.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.062	0.0000E+00	1526.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.7763	0.0000E+00	1556.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.5983	0.0000E+00	1582.	0.0000E+00	0.200000E-02
7	3708.	1801.	0.4768	0.0000E+00	1603.	0.0000E+00	0.200000E-02
8	3708.	1801.	0.4065	0.0000E+00	1622.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3522	0.0000E+00	1638.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3117	0.0000E+00	1654.	0.0000E+00	0.200000E-02
11	3583.	1792.	103.3	0.0000E+00	1656.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 125.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2499.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.71
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2519.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.632
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2535.8

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
43	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
45	.20	.18	.16	.14	.12	.11	.09	.08	.06	.05	.04	.03	.02	0	0	0	0
46	.25	.23	.21	.18	.16	.14	.12	.10	.08	.06	.05	.04	.03	0	0	0	0
47	.32	.29	.26	.23	.20	.18	.15	.12	.10	.08	.07	.05	.04	0	0	0	0
48	.40	.37	.33	.29	.26	.22	.19	.16	.13	.10	.08	.07	.05	0	0	0	0
49	.50	.45	.41	.36	.32	.27	.23	.19	.16	.13	.10	.08	.06	0	0	0	0
50	.61	.55	.50	.44	.38	.33	.28	.23	.19	.16	.13	.10	.08	0	0	0	0
51	.73	.66	.60	.53	.46	.40	.34	.28	.23	.19	.15	.12	.09	0	0	0	0
52	.86	.79	.71	.63	.55	.47	.40	.33	.28	.22	.18	.14	.11	0	0	0	0
53	1.0	.92	.83	.73	.64	.55	.47	.39	.32	.26	.21	.17	.13	0	0	0	0
54	1.1	1.0	.96	.85	.74	.63	.54	.45	.37	.30	.24	.19	.15	0	0	0	0
55	1.3	1.2	1.0	.96	.84	.72	.61	.51	.42	.34	.27	.22	.17	0	0	0	0
56	1.5	1.3	1.2	1.0	.94	.81	.69	.57	.47	.38	.31	.24	.19	0	0	0	0
57	1.6	1.5	1.3	1.2	1.0	.90	.76	.64	.52	.43	.34	.27	.21	0	0	0	0
58	1.8	1.6	1.4	1.3	1.1	.98	.83	.69	.57	.46	.37	.29	.23	0	0	0	0
59	1.9	1.7	1.6	1.4	1.2	1.0	.89	.75	.61	.50	.40	.31	.24	0	0	0	0
60	2.0	1.8	1.7	1.5	1.3	1.1	.95	.79	.65	.53	.42	.33	.26	0	0	0	0

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	22.68	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8653	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6227	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2795	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2382	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2064	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	4656.	1868.	60.57	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
19	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
21	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
23	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	.02	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
26	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
29	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
30	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
31	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
32	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
33	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
34	.11	.07	.04	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.0000
35	.12	.08	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	.0000
36	.13	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
37	.14	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	+0000
38	.15	.10	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
39	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
40	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
41	.17	.12	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
42	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+0000
43	.18	.13	.10	.07	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+0000
45	.19	.14	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+0000
46	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
48	.18	.15	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+0000
49	.18	.14	.11	.09	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+0000
50	.18	.14	.11	.09	.07	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+0000
51	.18	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
53	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+0000
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
55	.15	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000
57	.14	.12	.10	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
58	.13	.11	.10	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
59	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+0000
60	.12	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+0000

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF DDx

SUMMARY OF DDx DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72775E+06

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.4	1599.	0.5801E+08	0.5728E+08	339.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72735E+06

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	0.1027E+09	0.1020E+09	462.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72734E+06

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	1562.	1650.	0.1750E+09	0.1743E+09	599.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72733E+06

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	0.2752E+09	0.2745E+09	749.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72733E+06

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2277.	1700.	0.4078E+09	0.4071E+09	910.1	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72736E+06

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	0.5778E+09	0.5770E+09	1082.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72736E+06

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	0.7897E+09	0.7890E+09	1264.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72736E+06

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3350.	1776.	0.1048E+10	0.1048E+10	1455.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72742E+06

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	.09	.08	.06	.05														

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1359E+10	0.1358E+10	1656.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72742E+06

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.1726E+10	0.1725E+10	1865.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72755E+06

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4422.	1851.	0.2153E+10	0.2153E+10	2083.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.72755E+06

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.14	.12	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0	0	0	0
45	.18	.16	.15	.13	.12	.10	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
46	.23	.21	.19	.17	.15	.13	.11	.09	.08	.06	.05	.04	.03	0	0	0	0
47	.30	.27	.25	.22	.19	.17	.14	.12	.10	.08	.07	.05	.04	0	0	0	0
48	.38	.34	.31	.28	.24	.21	.18	.15	.13	.10	.08	.07	.05	0	0	0	0
49	.47	.43	.39	.35	.30	.26	.23	.19	.16	.13	.11	.08	.07	0	0	0	0
50	.57	.52	.47	.42	.37	.32	.28	.23	.20	.16	.13	.10	.08	0	0	0	0
51	.69	.63	.57	.51	.45	.39	.34	.28	.24	.19	.16	.13	.10	0	0	0	0
52	.83	.76	.69	.61	.54	.47	.40	.34	.28	.23	.19	.15	.12	0	0	0	0
53	.97	.89	.81	.72	.64	.55	.47	.40	.33	.28	.22	.18	.14	0	0	0	0
54	1.1	1.0	.94	.84	.74	.64	.55	.47	.39	.32	.26	.21	.16	0	0	0	0
55	1.2	1.1	1.0	.96	.85	.74	.63	.53	.45	.37	.30	.24	.19	0	0	0	0
56	1.4	1.3	1.2	1.0	.96	.83	.71	.60	.50	.42	.34	.27	.21	0	0	0	0
57	1.6	1.5	1.3	1.2	1.0	.93	.80	.67	.56	.46	.38	.30	.24	0	0	0	0
58	1.8	1.6	1.4	1.3	1.1	1.0	.88	.74	.62	.51	.42	.33	.26	0	0	0	0
59	1.9	1.7	1.6	1.4	1.2	1.1	.95	.81	.67	.56	.45	.36	.29	0	0	0	0
60	2.0	1.9	1.7	1.5	1.3	1.1	1.0	.87	.72	.60	.48	.39	.31	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	0	0	0	0
45	.06	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	.01	0	0	0	0
46	.08	.08	.07	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	0	0	0	0
47	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	0	0	0	0
48	.14	.12	.11	.10	.09	.08	.06	.05	.04	.04	.03	.02	.02	0	0	0	0
49	.17	.16	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0
50	.21	.19	.17	.15	.13	.12	.10	.08	.07	.06	.04	.04	.03	0	0	0	0
51	.25	.23	.21	.19	.16	.14	.12	.10	.08	.07	.06	.04	.03	0	0	0	0
52	.30	.28	.25	.22	.20	.17	.15	.12	.10	.08	.07	.05	.04	0	0	0	0
53	.36	.33	.30	.26	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
54	.41	.38	.34	.31	.27	.23	.20	.17	.14	.12	.09	.07	.06	0	0	0	0
55	.47	.44	.39	.35	.31	.27	.23	.19	.16	.13	.11	.09	.07	0	0	0	0
56	.54	.49	.45	.40	.35	.30	.26	.22	.18	.15	.12	.10	.08	0	0	0	0
57	.60	.55	.50	.44	.39	.34	.29	.25	.21	.17	.14	.11	.09	0	0	0	0
58	.66	.61	.55	.49	.43	.37	.32	.27	.23	.19	.15	.12	.09	0	0	0	0
59	.72	.66	.60	.53	.47	.41	.35	.30	.25	.20	.16	.13	.10	0	0	0	0
60	.77	.71	.64	.57	.50	.44	.37	.32	.26	.22	.18	.14	.11	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.02	.01	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.03	.02	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.04	.02	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.05	.03	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.06	.03	.01	+	+	+	+	0	0	0	0	0	0	0	0	0	0
35	.07	.04	.02	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.07	.04	.02	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
37	.07	.05	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
38	.08	.06	.04	.01	.01	+	+	+	+	0	0	0	0	0	0	0	0
39	.09	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
40	.10	.07	.04	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
41	.10	.07	.04	.03	.02	.01	+	+	+	+	0	0	0	0	0	0	0
42	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0	0	0
43	.10	.08	.05	.04	.02	.01	.01	+	+	+	+	0	0	0	0	0	0
44	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0
45	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	+	0	0	0	0	0
46	.11	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0	0
47	.11	.08	.06	.05	.04	.02	.02	.01	+	+	+	+	0	0	0	0	0
48	.10	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0
49	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0
50	.11	.09	.07	.06	.04	.03	.02	.01	.01	+	+	+	+	0	0	0	0
51	.11	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	0	0	0	0
52	.11	.09	.07	.06	.04	.03	.03	.02	.01	.01	+	+	+	0	0	0	0
53	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	0	0	0	0
54	.10	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	0	0	0	0
55	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	0	0	0	0
56	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	0	0	0	0
57	.10	.09	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	0	0	0	0
58	.10	.08	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	+	0	0	0	0
59	.10	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
60	.10	.09	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.2647E+10	0.2647E+10	2310.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

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M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21		+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
23		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
25		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
26		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
27		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
28		+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
29		+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
30		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
31		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
32		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
33	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
34	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
35	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
36	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
37	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	0
38	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	0

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

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[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.152E+02	1575.	1650.
2.00	0.0	0.299E+00	2625.	1725.
3.00	0.0	0.840E-02	3675.	1800.
4.00	0.0	0.289E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.419E+02	2550.	1725.
3.00	0.0	0.102E+02	3675.	1800.
4.00	0.0	0.302E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR DDx

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.135E-01	0.131E+01	825.	1575.
0.67	0.0	0.753E-02	0.131E+01	1200.	1650.
1.00	0.0	0.455E-02	0.130E+01	1575.	1650.
1.33	0.0	0.288E-02	0.130E+01	1950.	1650.
1.67	0.0	0.196E-02	0.130E+01	2250.	1725.
2.00	0.0	0.140E-02	0.130E+01	2625.	1725.
2.33	0.0	0.103E-02	0.130E+01	3000.	1725.
2.67	0.0	0.773E-03	0.130E+01	3375.	1800.
3.00	0.0	0.598E-03	0.130E+01	3675.	1800.
3.33	0.0	0.472E-03	0.130E+01	4050.	1800.
3.67	0.0	0.378E-03	0.130E+01	4425.	1875.
4.00	0.0	0.308E-03	0.130E+01	4800.	1875.
0.33	6.8	0.499E-01	0.135E+01	825.	1575.
0.67	6.8	0.278E-01	0.133E+01	1200.	1650.
1.00	6.8	0.168E-01	0.132E+01	1575.	1650.
1.33	6.8	0.106E-01	0.131E+01	1950.	1650.
1.67	6.8	0.726E-02	0.131E+01	2250.	1725.
2.00	6.8	0.519E-02	0.131E+01	2625.	1725.
2.33	6.8	0.379E-02	0.130E+01	3000.	1725.
2.67	6.8	0.286E-02	0.130E+01	3375.	1800.
3.00	6.8	0.221E-02	0.130E+01	3675.	1800.
3.33	6.8	0.174E-02	0.130E+01	4050.	1800.
3.67	6.8	0.140E-02	0.130E+01	4425.	1875.
4.00	6.8	0.114E-02	0.130E+01	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
2400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
3600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
4800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
6000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
7200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
8400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
9600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
10800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
12000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
13200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
14400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF DDx FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF DDx IS 2.34000 MG/L
AND ITS BACKGROUND CONCENTRATION IS 1.300000 MG/L.

THE WATER QUALITY STANDARD FOR DDx IS 1.000000 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	1) = 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	1) = 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	1) = 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	1) = 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	1) = 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	1) = 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	1) = 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	1) = 201.4	11.31	0.1341	8.588	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	1) = 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	1) = 214.3	11.55	0.9280E-01	6.297	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	1) = 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	2) = 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	2) = 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	2) = 144.6	9.538	0.6070	13.14	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	2) = 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	2) = 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	2) = 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	2) = 193.7	11.14	0.1709	4.997	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	2) = 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	2) = 208.2	11.44	0.1096	3.434	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	2) = 214.3	11.55	0.9280E-01	2.986	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	2) = 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	3) = 114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	3) = 128.4	8.827	0.7117	5.741	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	3) = 144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	3) = 160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	3) = 173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	3) = 184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	3) = 193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	3) = 201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	3) = 208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	3) = 214.3	11.55	0.9280E-01	1.260	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	3) = 214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	500.0	1575.	4) = 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	499.7	1575.	4) = 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	499.5	1575.	4) = 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	499.4	1575.	4) = 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	499.3	1575.	4) = 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	499.3	1575.	4) = 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	499.3	1575.	4) = 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	499.3	1575.	4) = 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	499.3	1575.	4) = 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	499.3	1575.	4) = 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	4) = 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	499.3	1575.	5) = 1 214.5	10.08	3.420	0.3098E+07	0.1875E+07	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 128.12

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4904.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 51.587

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4981.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 21.039

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5011.7

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.250	0.0000E+00	420.7	0.0000E+00	0.100000E-01
2	1563.	1650.	0.9148	0.0000E+00	443.1	0.0000E+00	0.100000E-01
3	1563.	1650.	0.8659	0.0000E+00	468.8	0.0000E+00	0.100000E-01
4	1563.	1650.	0.6671	0.0000E+00	492.8	0.0000E+00	0.100000E-01
5	1562.	1650.	0.5040	0.0000E+00	512.9	0.0000E+00	0.100000E-01
6	1562.	1650.	0.3810	0.0000E+00	529.3	0.0000E+00	0.100000E-01
7	1562.	1650.	0.2980	0.0000E+00	542.7	0.0000E+00	0.100000E-01
8	1562.	1650.	0.2459	0.0000E+00	554.0	0.0000E+00	0.100000E-01
9	1562.	1650.	0.2051	0.0000E+00	563.8	0.0000E+00	0.100000E-01
10	1561.	1650.	0.1706	0.0000E+00	572.5	0.0000E+00	0.100000E-01
11	1561.	1650.	15.54	0.0000E+00	572.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 8.5805
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5024.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.4994
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.4272
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.8483E-01	0.0000E+00	856.1	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.6206E-01	0.0000E+00	884.9	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.5874E-01	0.0000E+00	917.7	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.4525E-01	0.0000E+00	948.2	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.3419E-01	0.0000E+00	973.5	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.2584E-01	0.0000E+00	994.1	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2022E-01	0.0000E+00	1011.	0.0000E+00	13.50	0.100000E-01
8	2635.	1725.	0.1668E-01	0.0000E+00	1025.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1391E-01	0.0000E+00	1037.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1157E-01	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.054	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.58207
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.23739
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.96817E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.5754E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.4210E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.3985E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3070E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2319E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.1753E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1371E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	3707.	1801.	0.1132E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.9436E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.7852E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.7149E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.39486E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.16104E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65677E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.3904E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.2856E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.2703E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2082E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1573E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1189E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.9304E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.7677E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.6401E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.5326E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4850E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 938.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1183.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.09

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1694.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 343.50

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1778.7

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	96.43	0.0000E+00	420.7	0.0000E+00	0.200000E-02
2	1563.	1650.	3.412	0.0000E+00	443.1	0.0000E+00	0.200000E-02
3	1563.	1650.	3.268	0.0000E+00	468.8	0.0000E+00	0.200000E-02
4	1563.	1650.	2.684	0.0000E+00	492.8	0.0000E+00	0.200000E-02
5	1562.	1650.	2.040	0.0000E+00	512.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.556	0.0000E+00	529.3	0.0000E+00	0.200000E-02
7	1562.	1650.	1.188	0.0000E+00	542.7	0.0000E+00	0.200000E-02
8	1562.	1650.	0.9942	0.0000E+00	554.0	0.0000E+00	0.200000E-02
9	1562.	1650.	0.8375	0.0000E+00	563.8	0.0000E+00	0.200000E-02
10	1561.	1650.	0.7256	0.0000E+00	572.5	0.0000E+00	0.200000E-02
11	1435.	1641.	230.4	0.0000E+00	572.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 287.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 240.57
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1881.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 201.32
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1920.9

[illegible]

[illegible]

[illegible]

7200.00 SECONDS AFTER DUMP

7200.00 SECONDS AFTER DUMP

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
19		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
20		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
21		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
24		+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
26	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
27	.02	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
28	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
29	.03	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
30	.03	.01	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
31	.04	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0
32	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
33	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
34	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
35	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
36	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
37	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	56.52	0.0000E+00	856.1	0.0000E+00	0.200000E-02
2	2636.	1726.	2.000	0.0000E+00	884.9	0.0000E+00	0.200000E-02
3	2636.	1726.	1.915	0.0000E+00	917.7	0.0000E+00	0.200000E-02
4	2635.	1726.	1.573	0.0000E+00	948.2	0.0000E+00	0.200000E-02
5	2635.	1726.	1.195	0.0000E+00	973.5	0.0000E+00	0.200000E-02
6	2635.	1726.	0.9122	0.0000E+00	994.1	0.0000E+00	0.200000E-02
7	2635.	1726.	0.6960	0.0000E+00	1011.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.5827	0.0000E+00	1025.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.4908	0.0000E+00	1037.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.4253	0.0000E+00	1048.	0.0000E+00	0.200000E-02
11	2508.	1717.	135.0	0.0000E+00	1048.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 168.48
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1953.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1981.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 117.99
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2004.2

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.09	.07	.06	.04	.03	.02	.01	0	0	0	0	0	0	0	0	0	0
34		.14	.12	.09	.07	.05	.03	.02	0	0	0	0	0	0	0	0	0	0
35		.22	.17	.14	.10	.08	.05	.04	0	0	0	0	0					

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	00000
28	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	0	0	00000
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	00000
30	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
34	.08	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.09	.05	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
37	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
38	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
40	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
41	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
42	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
43	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
44	.12	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
45	.12	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
46	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+0000
47	.11	.08	.06	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	+0000
48	.10	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
49	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
50	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
51	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
52	.06	.05	.03	.02	.02	.01	+	+	+	+	+	+	+	+	+	+	.0000
53	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
54	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
55	.03	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
56	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	.	.0000
57	.02	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.0000
58	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.0000
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	33.12	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.9218	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7006	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5347	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4079	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	3707. 1801.	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.2877	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	3581. 1792.	79.13	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 98.744
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2023.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 82.635
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2039.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 69.155
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2052.3

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	.08	.07	.07	.06	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0
44	.11	.10	.09	.08	.07	.06	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
45	.15	.13	.12	.10	.09	.08	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
46	.19	.17	.15	.14	.12	.10	.08	.07	.06	.04	.04	.03	.02	0	0	0	0
47	.24	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
48	.31	.28	.25	.22	.19	.16	.14	.11	.09	.07	.06	.05	.03	0	0	0	0
49	.38	.35	.31	.27	.24	.20	.17	.14	.12	.09	.07	.06	.04	0	0	0	0
50	.47	.43	.38	.34	.29	.25	.21	.17	.14	.12	.09	.07	.05	0	0	0	0
51	.57	.52	.46	.41	.35	.30	.25	.21	.17	.14	.11	.09	.07	0	0	0	0
52	.68	.61	.55	.49	.42	.36	.30	.25	.21	.17	.13	.10	.08	0	0	0	0
53	.80	.72	.65	.57	.50	.42	.36	.30	.24	.20	.16	.12	.09	0	0	0	0
54	.93	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	.11	0	0	0	0
55	1.0	.96	.86	.76	.66	.56	.47	.39	.32	.26	.21	.16	.12	0	0	0	0
56	1.1	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	.14	0	0	0	0
57	1.3	1.2	1.0	.95	.82	.70	.59	.49	.40	.32	.26	.20	.16	0	0	0	0
58	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.36	.28	.22	.17	0	0	0	0
59	1.5	1.4	1.2	1.1	.97	.83	.70	.58	.48	.38	.30	.24	.18	0	0	0	0
60	1.6	1.5	1.3	1.1	1.0	.88	.74	.62	.51	.41	.32	.25	.19	0	0	0	0

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.06	.03	.01	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	+	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	19.41	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.6580	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4106	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.2391	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2002	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1686	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	4654.	1868.	46.38	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
28	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
29	.03	.01	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
30	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
31	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.06	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.07	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.08	.05	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
35	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.10	.06	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	.	0
37	.11	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	.	0
38	.11	.07	.05	.03	.01	.01	+	+	+	+	+	+	+	+	+	+	0
39	.12	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
40	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
41	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
42	.14	.10	.07	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
43	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
44	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
45	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	0
46	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
47	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	0
48	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
49	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	+	0
50	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	+	0
51	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
52	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
53	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
54	.13	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
55	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
56	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
57	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	0
58	.10	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
59	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	0
60	.09	.08	.07	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	0

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

THICKNESS (FT) OF Clumps ACCUMULATED ON BOTTOM, 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF DDx

SUMMARY OF DDx DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12237E+07

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.3	1599.	0.5138E+08	0.5015E+08	317.4	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12233E+07

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	0.9275E+08	0.9153E+08	438.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12233E+07

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1561.	1650.	0.1604E+09	0.1591E+09	572.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12233E+07

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	0.2549E+09	0.2536E+09	719.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12233E+07

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2277.	1700.	0.3810E+09	0.3798E+09	878.7	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12233E+07

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	0.5435E+09	0.5423E+09	1048.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12201E+07

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	0.7471E+09	0.7459E+09	1228.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12201E+07

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3349.	1776.	0.9966E+09	0.9954E+09	1418.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12201E+07

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	3707.	1801.	0.1297E+10	0.1296E+10	1617.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12137E+07

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.1652E+10	0.1651E+10	1825.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12137E+07

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4422.	1851.	0.2068E+10	0.2067E+10	2041.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.12140E+07

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.21	.19	.17	.15	.13	.12	.10	.08	.07	.05	.04	.03	.03	0	0	0	0
45	.28	.26	.23	.21	.18	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	0
46	.37	.34	.30	.27	.24	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
47	.47	.43	.39	.35	.30	.26	.22	.19	.15	.13	.10	.08	.06	0	0	0	0
48	.60	.55	.50	.44	.39	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0
49	.76	.69	.62	.55	.49	.42	.36	.30	.25	.20	.16	.13	.10	0	0	0	0
50	.93	.85	.77	.68	.60	.52	.44	.37	.31	.25	.20	.16	.12	0	0	0	0
51	1.1	1.0	.94	.83	.73	.63	.54	.45	.38	.31	.25	.20	.15	0	0	0	0
52	1.3	1.2	1.1	1.0	.88	.76	.65	.54	.45	.37	.30	.24	.18	0	0	0	0
53	1.6	1.4	1.3	1.1	1.0	.90	.77	.65	.54	.44	.35	.28	.22	0	0	0	0
54	1.8	1.7	1.5	1.3	1.2	1.0	.90	.75	.63	.51	.41	.33	.26	0	0	0	0
55	2.1	1.9	1.7	1.5	1.4	1.2	1.0	.87	.72	.59	.48	.38	.30	0	0	0	0
56	2.4	2.2	2.0	1.8	1.5	1.3	1.1	.99	.82	.67	.54	.43	.34	0	0	0	0
57	2.7	2.5	2.2	2.0	1.7	1.5	1.3	1.1	.92	.75	.61	.48	.38	0	0	0	0
58	3.0	2.7	2.5	2.2	1.9	1.7	1.4	1.2	1.0	.83	.67	.53	.42	0	0	0	0
59	3.3	3.0	2.7	2.4	2.1	1.8	1.5	1.3	1.1	.90	.73	.58	.46	0	0	0	0
60	3.5	3.2	2.9	2.6	2.3	1.9	1.7	1.4	1.1	.97	.79	.62	.49	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.08	.07	.06	.05	.05	.04	.03	.03	.02	.02	.01	.01	.01	0	0	0	0
45	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
46	.13	.12	.11	.10	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
47	.17	.16	.14	.13	.11	.09	.08	.07	.05	.04	.03	.03	.02	0	0	0	0
48	.22	.20	.18	.16	.14	.12	.10	.09	.07	.06	.04	.03	.03	0	0	0	0
49	.28	.25	.23	.20	.18	.15	.13	.11	.09	.07	.06	.04	.03	0	0	0	0
50	.34	.31	.28	.25	.22	.19	.16	.13	.11	.09	.07	.06	.04	0	0	0	0
51	.42	.38	.34	.30	.27	.23	.20	.16	.14	.11	.09	.07	.05	0	0	0	0
52	.50	.46	.41	.37	.32	.28	.24	.20	.16	.13	.11	.08	.06	0	0	0	0
53	.59	.54	.49	.43	.38	.33	.28	.24	.19	.16	.13	.10	.08	0	0	0	0
54	.69	.63	.57	.51	.45	.38	.33	.28	.23	.19	.15	.12	.09	0	0	0	0
55	.80	.73	.66	.59	.51	.44	.38	.32	.26	.21	.17	.14	.11	0	0	0	0
56	.91	.83	.75	.67	.58	.50	.43	.36	.30	.24	.20	.16	.12	0	0	0	0
57	1.0	.93	.84	.75	.65	.57	.48	.41	.34	.27	.22	.17	.14	0	0	0	0
58	1.1	1.0	.93	.82	.72	.63	.53	.45	.37	.30	.24	.19	.15	0	0	0	0
59	1.2	1.1	1.0	.90	.79	.68	.58	.49	.41	.33	.27	.21	.17	0	0	0	0
60	1.3	1.2	1.0	.97	.85	.73	.63	.53	.44	.36	.29	.23	.18	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.03	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.05	.01	+	+	+	0	0	0	0	0	0	0	0	0	0	0	0
32	.06	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.08	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.10	.03	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.11	.05	.03	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.11	.06	.04	.01	.01	+	+	0	0	0	0	0	0	0	0	0	0
37	.11	.08	.05	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0
38	.14	.09	.06	.02	.01	+	+	+	+	0	0	0	0	0	0	0	0
39	.15	.10	.06	.03	.02	+	+	+	+	0	0	0	0	0	0	0	0
40	.16	.11	.07	.04	.03	.01	+	+	+	0	0	0	0	0	0	0	0
41	.17	.11	.07	.05	.03	.01	.01	+	+	+	+	0	0	0	0	0	0
42	.16	.11	.08	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
43	.17	.13	.09	.06	.04	.02	.01	+	+	+	+	0	0	0	0	0	0
44	.18	.14	.10	.07	.05	.03	.02	.01	+	+	+	+	+	0	0	0	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	0	0	0	0
46	.19	.14	.10	.07	.05	.04	.03	.01	.01	+	+	+	+	0	0	0	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	+	+	+	+	0	0	0	0
48	.18	.15	.12	.09	.07	.05	.03	.02	.01	+	+	+	+	0	0	0	0
49	.19	.16	.12	.09	.07	.05	.03	.02	.02	.01	+	+	+	0	0	0	0
50	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
51	.20	.16	.13	.10	.07	.05	.04	.03	.02	.01	.01	+	+	0	0	0	0
52	.19	.15	.12	.10	.08	.06	.04	.03	.02	.01	.01	+	+	0	0	0	0
53	.18	.15	.13	.10	.08	.06	.05	.04	.02	.02	.01	.01	+	0	0	0	0
54	.18	.16	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	0	0	0	0
55	.19	.16	.13	.11	.09	.07	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
56	.18	.16	.13	.11	.09	.07	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
57	.18	.15	.13	.10	.09	.07	.06	.05	.03	.03	.02	.01	.01	0	0	0	0
58	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	0	0	0	0
59	.17	.15	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	0	0	0	0
60	.17	.15	.13	.11	.09	.08	.06	.05	.04	.03	.02	.02	.01	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.2549E+10	0.2548E+10	2266.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.122E+02	1575.	1650.
2.00	0.0	0.236E+00	2625.	1725.
3.00	0.0	0.659E-02	3675.	1800.
4.00	0.0	0.226E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.200E+03	1500.	1650.
2.00	0.0	0.346E+02	2550.	1725.
3.00	0.0	0.834E+01	3675.	1800.
4.00	0.0	0.246E+01	4725.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR DDx

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.257E-01	0.133E+01	825.	1575.
0.67	0.0	0.141E-01	0.131E+01	1200.	1650.
1.00	0.0	0.840E-02	0.131E+01	1575.	1650.
1.33	0.0	0.523E-02	0.131E+01	1950.	1650.
1.67	0.0	0.354E-02	0.130E+01	2250.	1725.
2.00	0.0	0.251E-02	0.130E+01	2625.	1725.
2.33	0.0	0.182E-02	0.130E+01	3000.	1725.
2.67	0.0	0.137E-02	0.130E+01	3375.	1800.
3.00	0.0	0.105E-02	0.130E+01	3675.	1800.
3.33	0.0	0.822E-03	0.130E+01	4050.	1800.
3.67	0.0	0.658E-03	0.130E+01	4425.	1875.
4.00	0.0	0.534E-03	0.130E+01	4800.	1875.
0.33	6.8	0.950E-01	0.140E+01	825.	1575.
0.67	6.8	0.521E-01	0.135E+01	1200.	1650.
1.00	6.8	0.310E-01	0.133E+01	1575.	1650.
1.33	6.8	0.193E-01	0.132E+01	1950.	1650.
1.67	6.8	0.131E-01	0.131E+01	2250.	1725.
2.00	6.8	0.929E-02	0.131E+01	2625.	1725.
2.33	6.8	0.673E-02	0.131E+01	3000.	1725.
2.67	6.8	0.505E-02	0.131E+01	3375.	1800.
3.00	6.8	0.389E-02	0.130E+01	3675.	1800.
3.33	6.8	0.304E-02	0.130E+01	4050.	1800.
3.67	6.8	0.243E-02	0.130E+01	4425.	1875.
4.00	6.8	0.197E-02	0.130E+01	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
2400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
3600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
4800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
6000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
7200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
8400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
9600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
10800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
12000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
13200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
14400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF DDx FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF DDx IS 0.124000 MG/L
AND ITS BACKGROUND CONCENTRATION IS 1.300000 MG/L.

THE WATER QUALITY STANDARD FOR DDx IS 1.000000 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0 1575.	1) = 1 109.2	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8 1575.	1) = 2 130.9	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6 1575.	1) = 3 152.5	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5 1575.	1) = 4 171.5	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5 1575.	1) = 5 187.3	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5 1575.	1) = 6 200.5	10.89	0.2393	53.70	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5 1575.	1) = 7 211.8	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5 1575.	1) = 8 221.7	11.31	0.1469	35.76	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5 1575.	1) = 9 230.7	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5 1575.	1) = 10 238.9	11.58	0.1054	27.19	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5 1575.	1) = 11 239.2	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	2) = 1 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	2) = 2 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	2) = 3 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	2) = 4 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	2) = 5 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	2) = 6 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	2) = 7 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	2) = 8 221.7	11.31	0.1469	0.4822	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	2) = 9 230.7	11.46	0.1227	0.4153	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	2) = 10 238.9	11.58	0.1054	0.3668	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	2) = 11 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED	
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	500.0	1575.	3) = 109.2	1	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	499.8	1575.	3) = 130.9	2	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	499.6	1575.	3) = 152.5	3	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	499.5	1575.	3) = 171.5	4	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	499.5	1575.	3) = 187.3	5	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	499.5	1575.	3) = 200.5	6	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	499.5	1575.	3) = 211.8	7	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	499.5	1575.	3) = 221.7	8	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	499.5	1575.	3) = 230.7	9	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	499.5	1575.	3) = 238.9	10	11.58	0.1054	0.1514	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	3) = 239.2	11	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	499.5	1575.	4) = 1 239.2	9.685	3.815	0.4997E+07	0.3368E+07	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.411

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 493.19

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 38.912

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 549.69

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 15.870

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 572.73

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.488	0.0000E+00	411.8	0.0000E+00	0.100000E-01
2	1563.	1650.	0.1670	0.0000E+00	447.2	0.0000E+00	0.100000E-01
3	1563.	1650.	0.1244	0.0000E+00	481.0	0.0000E+00	0.100000E-01
4	1563.	1650.	0.8470E-01	0.0000E+00	509.8	0.0000E+00	0.100000E-01
5	1562.	1650.	0.6077E-01	0.0000E+00	533.4	0.0000E+00	0.100000E-01
6	1562.	1650.	0.4553E-01	0.0000E+00	552.7	0.0000E+00	0.100000E-01
7	1562.	1650.	0.3587E-01	0.0000E+00	569.0	0.0000E+00	0.100000E-01
8	1562.	1650.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	0.100000E-01
9	1562.	1650.	0.2516E-01	0.0000E+00	596.0	0.0000E+00	0.100000E-01
10	1562.	1650.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	0.100000E-01
11	1562.	1650.	13.79	0.0000E+00	607.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.4723
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 582.12

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.6397
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.96

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.0766
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.52
MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1009	0.0000E+00	844.6	0.0000E+00	0.100000E-01
2	2636.	1726.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	0.100000E-01
3	2636.	1726.	0.8436E-02	0.0000E+00	933.3	0.0000E+00	0.100000E-01
4	2635.	1726.	0.5746E-02	0.0000E+00	969.7	0.0000E+00	0.100000E-01
5	2635.	1726.	0.4122E-02	0.0000E+00	999.2	0.0000E+00	0.100000E-01
6	2635.	1726.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	0.100000E-01
7	2635.	1725.	0.2433E-02	0.0000E+00	1044.	0.0000E+00	0.100000E-01
8	2635.	1725.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	0.100000E-01
9	2635.	1725.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	0.100000E-01
10	2634.	1725.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	0.100000E-01
11	2634.	1725.	0.9353	0.0000E+00	1092.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.43906
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.16

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17907
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.42

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73030E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.52
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
52	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
53	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
54	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
56	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
57	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
58	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
60	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.6846E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	3709.	1801.	0.7684E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	3709.	1801.	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	3708.	1801.	0.3898E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	3708.	1801.	0.2796E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	3708.	1801.	0.2095E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	3708.	1801.	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	3708.	1801.	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	3707.	1801.	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	3707.	1801.	0.1004E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	3707.	1801.	0.6345E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.29784E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.57

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12147E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.49541E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.59
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
29	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0
36	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0
38	+	+	+	+	+</													

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4644E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3882E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2644E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	4781.	1877.	0.1421E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	4781.	1877.	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.7853E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.6808E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4304E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.871

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.29

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.710

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 136.65

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 106.35

[illegible]

[illegible]

[illegible]

[illegible]

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0 = .LT. .0000001)
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[illegible][illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	13.35	0.0000E+00	411.8	0.0000E+00	0.200000E-02
2	1563.	1650.	0.5799	0.0000E+00	447.2	0.0000E+00	0.200000E-02
3	1563.	1650.	0.4376	0.0000E+00	481.0	0.0000E+00	0.200000E-02
4	1563.	1650.	0.3164	0.0000E+00	509.8	0.0000E+00	0.200000E-02
5	1562.	1650.	0.2289	0.0000E+00	533.4	0.0000E+00	0.200000E-02
6	1562.	1650.	0.1739	0.0000E+00	552.7	0.0000E+00	0.200000E-02
7	1562.	1650.	0.1387	0.0000E+00	569.0	0.0000E+00	0.200000E-02
8	1562.	1650.	0.1153	0.0000E+00	583.3	0.0000E+00	0.200000E-02
9	1562.	1650.	0.9923E-01	0.0000E+00	596.0	0.0000E+00	0.200000E-02
10	1562.	1650.	0.8740E-01	0.0000E+00	607.5	0.0000E+00	0.200000E-02
11	1562.	1650.	121.1	0.0000E+00	607.9	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.64

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 95.702
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 147.30

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.91

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
22	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
24	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
25	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
26	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
27	.01	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0
28	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
29	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0
30	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
31	.02	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
32	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
33	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
34	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
35	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
36	.02	.01	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0	0
37	.02	.01	+	+	+	+	+	+	.	.	.	.						

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	7.825	0.0000E+00	844.6	0.0000E+00	0.200000E-02
2	2636.	1726.	0.3399	0.0000E+00	890.2	0.0000E+00	0.200000E-02
3	2636.	1726.	0.2564	0.0000E+00	933.3	0.0000E+00	0.200000E-02
4	2635.	1726.	0.1854	0.0000E+00	969.7	0.0000E+00	0.200000E-02
5	2635.	1726.	0.1342	0.0000E+00	999.2	0.0000E+00	0.200000E-02
6	2635.	1726.	0.1019	0.0000E+00	1023.	0.0000E+00	0.200000E-02
7	2635.	1725.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	0.200000E-02
8	2635.	1725.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	0.200000E-02
9	2635.	1725.	0.5816E-01	0.0000E+00	1077.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5122E-01	0.0000E+00	1091.	0.0000E+00	0.200000E-02
11	2634.	1725.	70.99	0.0000E+00	1092.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.024
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.090
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.91

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 46.940
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 196.06

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

(CU FT/GRID SQUARE) , 10800.00 SECONDS AFTER DUMP

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
22	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
23	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
24	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
25	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
26	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
27	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
28	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0
29	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0
30	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0
31	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
32	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
33	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
34	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
35	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
36	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	0
37	.04	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	0
38	.05	.03	.02	.0														

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709. 1801.	4.586	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	3709. 1801.	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	3709. 1801.	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	3708. 1801.	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	3708. 1801.	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	3708. 1801.	0.5973E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	3708. 1801.	0.4763E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	3708. 1801.	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	3707. 1801.	0.3409E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	3707. 1801.	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	3707. 1801.	41.61	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.282
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.69

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.874
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.98

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.511
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 215.12

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.03	.03	.03	.02	.02	.02	.01	.01	.01	.01	+	+	+	0	0	0	0
45	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	+	0	0	0	0
46	.06	.05	.05	.04	.04	.03	.03	.02	.02	.01	.01	.01	+	0	0	0	0
47	.08	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0
48	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	.01	0	0	0	0
49	.13	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0
50	.16	.14	.13	.11	.10	.09	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
51	.19	.17	.16	.14	.12	.11	.09	.07	.06	.05	.04	.03	.02	0	0	0	0
52	.23	.21	.19	.17	.15	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0
53	.27	.25	.22	.20	.17	.15	.13	.11	.09	.07	.06	.05	.03	0	0	0	0
54	.32	.29	.26	.23	.20	.18	.15	.13	.10	.08	.07	.05	.04	0	0	0	0
55	.36	.33	.30	.27	.23	.20	.17	.14	.12	.10	.08	.06	.05	0	0	0	0
56	.41	.38	.34	.30	.27	.23	.20	.16	.14	.11	.09	.07	.06	0	0	0	0
57	.46	.42	.38	.34	.30	.26	.22	.18	.15	.13	.10	.08	.06	0	0	0	0
58	.51	.47	.42	.37	.33	.28	.24	.20	.17	.14	.11	.09	.07	0	0	0	0
59	.56	.51	.46	.41	.36	.31	.26	.22	.18	.15	.12	.10	.08	0	0	0	0
60	.60	.55	.49	.44	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0

[illegible]

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	2.688	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	4781.	1877.	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	4781.	1877.	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.1998E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1759E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	4780.	1877.	24.38	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
24	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
25	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
27	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
28	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0
29	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
30	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
31	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
32	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
33	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	0
34	.05	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
35	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.	0
36	.07	.04	.02	.01	.01	+	+	+	+	+	+	+	+	.	.	.	0
37	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	.	.	0
38	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	.	0
39	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
40	.08	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	0
41	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	+	+	0
42	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
43	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
44	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	0
45	.09	.07	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	+	+	0
46	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
47	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
48	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
49	.09	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	+	+	+	0
50	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	0
51	.09	.07	.06	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	0
52	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	0
53	.08	.07	.05	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	0
54	.08	.07	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	0
55	.08	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	0
56	.07	.06	.05	.04	.03	.03	.02	.01	.01	.01	+	+	+	+	+	+	0
57	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	0
58	.07	.06	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	0
59	.06	.05	.05	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	0
60	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	+	+	+	+	+	+	0

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF DDx

SUMMARY OF DDx DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16297E+07

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.4	1599.	0.6115E+08	0.5952E+08	345.8	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	0.1068E+09	0.1052E+09	470.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1562.	1650.	0.1806E+09	0.1790E+09	607.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	0.2825E+09	0.2808E+09	758.0	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2277.	1700.	0.4171E+09	0.4155E+09	919.5	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	0.5893E+09	0.5877E+09	1092.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	0.8037E+09	0.8021E+09	1274.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3350.	1776.	0.1065E+10	0.1064E+10	1466.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16297E+07

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1379E+10	0.1377E+10	1667.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16296E+07

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4065.	1826.	0.1749E+10	0.1747E+10	1878.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16297E+07

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4422.	1851.	0.2180E+10	0.2179E+10	2096.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.16297E+07

CONCENTRATIONS ABOVE BACKGROUND OF DDx (MG/L) IN THE CLOUD 14400.00 SECONDS AFTER DUMP

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.32	.29	.26	.24	.21	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	0
45	.42	.38	.35	.31	.27	.24	.20	.17	.14	.12	.10	.08	.06	0	0	0	0
46	.54	.49	.45	.40	.35	.31	.26	.22	.19	.15	.12	.10	.08	0	0	0	0
47	.68	.63	.57	.51	.45	.39	.33	.28	.24	.20	.16	.13	.10	0	0	0	0
48	.86	.79	.71	.64	.56	.49	.42	.36	.30	.25	.20	.16	.13	0	0	0	0
49	1.0	.98	.88	.79	.70	.61	.52	.44	.37	.31	.25	.20	.16	0	0	0	0
50	1.3	1.1	1.0	.97	.85	.74	.64	.54	.45	.37	.30	.24	.19	0	0	0	0
51	1.5	1.4	1.3	1.1	1.0	.90	.77	.65	.55	.45	.37	.30	.23	0	0	0	0
52	1.8	1.7	1.5	1.3	1.2	1.0	.92	.78	.65	.54	.44	.35	.28	0	0	0	0
53	2.1	2.0	1.8	1.6	1.4	1.2	1.0	.91	.77	.63	.52	.41	.33	0	0	0	0
54	2.5	2.3	2.1	1.8	1.6	1.4	1.2	1.0	.89	.73	.60	.48	.38	0	0	0	0
55	2.9	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	.84	.68	.55	.44	0	0	0	0
56	3.2	3.0	2.7	2.4	2.1	1.8	1.6	1.3	1.1	.95	.77	.62	.49	0	0	0	0
57	3.6	3.3	3.0	2.7	2.4	2.0	1.8	1.5	1.2	1.0	.86	.69	.55	0	0	0	0
58	4.0	3.6	3.3	2.9	2.6	2.3	1.9	1.6	1.4	1.1	.95	.76	.61	0	0	0	0
59	4.3	4.0	3.6	3.2	2.8	2.4	2.1	1.8	1.5	1.2	1.0	.83	.66	0	0	0	0
60	4.6	4.2	3.8	3.4	3.0	2.6	2.3	1.9	1.6	1.3	1.1	.89	.70	0	0	0	0

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.11	.10	.09	.08	.07	.06	.05	.05	.04	.03	.02	.02	.01	0	0	0	0
45	.15	.14	.12	.11	.10	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0
46	.20	.18	.16	.14	.13	.11	.09	.08	.07	.05	.04	.03	.03	0	0	0	0
47	.25	.23	.21	.18	.16	.14	.12	.10	.08	.07	.06	.04	.03	0	0	0	0
48	.31	.29	.26	.23	.20	.18	.15	.13	.11	.09	.07	.06	.04	0	0	0	0
49	.39	.36	.32	.29	.25	.22	.19	.16	.13	.11	.09	.07	.06	0	0	0	0
50	.48	.44	.40	.35	.31	.27	.23	.20	.16	.13	.11	.09	.07	0	0	0	0
51	.58	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.11	.08	0	0	0	0
52	.69	.63	.57	.51	.45	.39	.34	.28	.24	.20	.16	.13	.10	0	0	0	0
53	.81	.74	.67	.60	.53	.46	.39	.33	.28	.23	.19	.15	.12	0	0	0	0
54	.93	.86	.78	.69	.61	.53	.46	.39	.32	.27	.22	.17	.14	0	0	0	0
55	1.0	.98	.89	.79	.70	.61	.52	.44	.37	.31	.25	.20	.16	0	0	0	0
56	1.2	1.1	1.0	.90	.79	.69	.59	.50	.42	.35	.28	.23	.18	0	0	0	0
57	1.3	1.2	1.1	1.0	.88	.77	.66	.56	.47	.39	.32	.25	.20	0	0	0	0
58	1.4	1.3	1.2	1.1	.97	.85	.73	.62	.52	.43	.35	.28	.22	0	0	0	0
59	1.6	1.4	1.3	1.1	1.0	.92	.79	.67	.56	.46	.38	.30	.24	0	0	0	0
60	1.7	1.5	1.4	1.2	1.1	.98	.85	.72	.60	.50	.40	.32	.26	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	+	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	+	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	+	+	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	+	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0
32	+	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0
33	+	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0
34	+	+	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0
35	+	+	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0
36	+	+	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0
37	+	+	+	+	+	.	0	0	0	0	0	0	0	0	0	0	0
38	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0
39	+	+	+	+	+	+	.	.	0	0	0	0	0	0	0	0	0
40	+	+	+	+	+	+	.	.	0	0	0	0	0	0	0	0	0
41	+	+	+	+	+	+	.	.	.	0	0	0	0	0	0	0	0
42	+	+	+	+	+	+	+	.	.	0	0	0	0	0	0	0	0
43	+	+	+	+	+	+	+	+	.	.	0	0	0	0	0	0	0
44	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
45	+	+	+	+	+	+	+	+	.	.	.	.	0	0	0	0	0
46	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0
47	+	+	+	+	+	+	+	+	+	.	.	.	0	0	0	0	0
48	+	+	+	+	+	+	+	+	+	+	.	.	0	0	0	0	0
49	+	+	+	+	+	+	+	+	+	+	.	.	0	0	0	0	0
50	+	+	+	+	+	+	+	+	+	+	.	.	0	0	0	0	0
51	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0	0
52	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
53	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
54	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
55	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
56	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
57	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
58	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
59	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
60	+	+	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.2678E+10	0.2676E+10	2323.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....


```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
23	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
24	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
25	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
28	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
29	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
33	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
35	.	.	.	.</														

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.819E+01	1575.	1650.
2.00	0.0	0.164E+00	2625.	1725.
3.00	0.0	0.467E-02	3675.	1800.
4.00	0.0	0.162E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.702E+02	1575.	1650.
2.00	0.0	0.122E+02	2625.	1725.
3.00	0.0	0.299E+01	3675.	1800.
4.00	0.0	0.896E+00	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR DDx

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.291E-01	0.133E+01	825.	1575.
0.67	0.0	0.164E-01	0.132E+01	1200.	1650.
1.00	0.0	0.993E-02	0.131E+01	1575.	1650.
1.33	0.0	0.630E-02	0.131E+01	1950.	1650.
1.67	0.0	0.431E-02	0.130E+01	2250.	1725.
2.00	0.0	0.309E-02	0.130E+01	2625.	1725.
2.33	0.0	0.226E-02	0.130E+01	3000.	1725.
2.67	0.0	0.171E-02	0.130E+01	3375.	1800.
3.00	0.0	0.132E-02	0.130E+01	3675.	1800.
3.33	0.0	0.104E-02	0.130E+01	4050.	1800.
3.67	0.0	0.838E-03	0.130E+01	4425.	1875.
4.00	0.0	0.682E-03	0.130E+01	4800.	1875.
0.33	6.8	0.108E+00	0.141E+01	825.	1575.
0.67	6.8	0.604E-01	0.136E+01	1200.	1650.
1.00	6.8	0.367E-01	0.134E+01	1575.	1650.
1.33	6.8	0.233E-01	0.132E+01	1950.	1650.
1.67	6.8	0.159E-01	0.132E+01	2250.	1725.
2.00	6.8	0.114E-01	0.131E+01	2625.	1725.
2.33	6.8	0.836E-02	0.131E+01	3000.	1725.
2.67	6.8	0.631E-02	0.131E+01	3375.	1800.
3.00	6.8	0.488E-02	0.130E+01	3675.	1800.
3.33	6.8	0.385E-02	0.130E+01	4050.	1800.
3.67	6.8	0.310E-02	0.130E+01	4425.	1875.
4.00	6.8	0.252E-02	0.130E+01	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
2400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
3600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
4800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
6000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
7200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
8400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
9600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
10800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
12000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
13200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
14400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 525.0 FT (XBARGE) OR ABOUT GRID POINT # 8 FROM THE TOP OF THE GRID
AND 1575. FT (ZBARGE) OR ABOUT GRID POINT #22 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = 0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = 0.210E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = 0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = 0.210E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF DDx FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF DDx IS 215.000 MG/L
AND ITS BACKGROUND CONCENTRATION IS 1.300000 MG/L.

THE WATER QUALITY STANDARD FOR DDx IS 1.000000 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.000	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 72.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 235.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	1) = 123.6	9.291	0.6767E-01	140.1	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	1) = 137.3	9.359	0.5698	2.383	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	1) = 151.3	9.929	0.4586	2.134	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	1) = 163.7	10.39	0.3367	1.710	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	1) = 174.2	10.72	0.2440	1.325	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	1) = 182.8	10.97	0.1815	1.038	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	1) = 190.1	11.15	0.1404	0.8352	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	1) = 196.3	11.29	0.1129	0.6941	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	1) = 201.8	11.40	0.9417E-01	0.5948	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	1) = 206.8	11.50	0.8092E-01	0.5234	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	1) = 207.7	10.19	3.312	847.7	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	2) = 1 123.6	9.291	0.6767E-01	1135.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	2) = 2 137.3	9.359	0.5698	19.31	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	2) = 3 151.3	9.929	0.4586	17.29	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	2) = 4 163.7	10.39	0.3367	13.86	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	2) = 5 174.2	10.72	0.2440	10.74	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	2) = 6 182.8	10.97	0.1815	8.406	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	2) = 7 190.1	11.15	0.1404	6.765	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	2) = 8 196.3	11.29	0.1129	5.626	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	2) = 9 201.8	11.40	0.9417E-01	4.820	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	2) = 10 206.8	11.50	0.8092E-01	4.242	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	2) = 11 207.7	10.19	3.312	6869.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	3) = 123.6	9.291	0.6767E-01	446.7	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	3) = 137.3	9.359	0.5698	7.601	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	3) = 151.3	9.929	0.4586	6.806	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	3) = 163.7	10.39	0.3367	5.455	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	3) = 174.2	10.72	0.2440	4.227	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	3) = 182.8	10.97	0.1815	3.309	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	3) = 190.1	11.15	0.1404	2.663	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	3) = 196.3	11.29	0.1129	2.214	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	3) = 201.8	11.40	0.9417E-01	1.897	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	3) = 206.8	11.50	0.8092E-01	1.670	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	3) = 207.7	10.19	3.312	2703.	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.54	500.0	1575.	4) = 123.6	13.50	0.1000E-02	3949.	0.0000E+00	24	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.09	499.7	1575.	4) = 137.3	13.50	0.1000E-02	3128.	0.0000E+00	47	24
NEW CLOUD CREATED, NTCLD(K) (K = 31.63	499.5	1575.	4) = 151.3	13.50	0.1000E-02	2120.	0.0000E+00	70	47
NEW CLOUD CREATED, NTCLD(K) (K = 32.18	499.4	1575.	4) = 163.7	13.50	0.1000E-02	1343.	0.0000E+00	93	70
NEW CLOUD CREATED, NTCLD(K) (K = 32.72	499.2	1575.	4) = 174.2	13.50	0.1000E-02	798.7	0.0000E+00	116	93
NEW CLOUD CREATED, NTCLD(K) (K = 33.27	499.1	1575.	4) = 182.8	13.50	0.1000E-02	450.2	0.0000E+00	139	116
NEW CLOUD CREATED, NTCLD(K) (K = 33.81	499.1	1575.	4) = 190.1	13.50	0.1000E-02	243.2	0.0000E+00	162	139
NEW CLOUD CREATED, NTCLD(K) (K = 34.35	499.0	1575.	4) = 196.3	13.50	0.1000E-02	126.9	0.0000E+00	185	162
NEW CLOUD CREATED, NTCLD(K) (K = 34.90	499.0	1575.	4) = 201.8	13.50	0.1000E-02	64.40	0.0000E+00	208	185
NEW CLOUD CREATED, NTCLD(K) (K = 35.44	499.0	1575.	4) = 206.8	13.50	0.1000E-02	31.89	0.0000E+00	231	208
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	4) = 207.7	10.19	3.312	29.13	0.0000E+00	235	231

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.54	499.0	1575.	5) = 1 207.7	10.19	3.312	0.1807E+09	0.1518E+07	235	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

BOTTOM ACCUMULATION OF SAND (CU FT/GRID SQUARE) , 1200.00 SECONDS AFTER DUMP

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...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 140.31

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7954.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 55.287

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8039.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.548

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8072.0

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36		0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1564.	1650.	1.588	0.0000E+00	435.4	0.0000E+00	13.50	0.100000E-01
2	1563.	1650.	1.229	0.0000E+00	457.2	0.0000E+00	13.50	0.100000E-01
3	1563.	1650.	1.037	0.0000E+00	479.1	0.0000E+00	13.50	0.100000E-01
4	1563.	1650.	0.8205	0.0000E+00	498.2	0.0000E+00	13.50	0.100000E-01
5	1562.	1650.	0.6312	0.0000E+00	513.9	0.0000E+00	13.50	0.100000E-01
6	1562.	1650.	0.4945	0.0000E+00	526.7	0.0000E+00	13.50	0.100000E-01
7	1562.	1650.	0.3970	0.0000E+00	537.4	0.0000E+00	13.50	0.100000E-01
8	1562.	1650.	0.3360	0.0000E+00	546.5	0.0000E+00	13.50	0.100000E-01
9	1561.	1650.	0.2856	0.0000E+00	554.5	0.0000E+00	13.50	0.100000E-01
10	1561.	1650.	0.2423	0.0000E+00	561.7	0.0000E+00	13.50	0.100000E-01
11	1561.	1650.	15.49	0.0000E+00	562.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.1960
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.7505
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5296
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.1
MAX CONC IS 0.00000010 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
18		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
20		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
21		+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
22		+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
23		+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
24		+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
25		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
26		+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
27		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
28		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
29		+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
30		+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	00000
31		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
32		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
33		+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
34		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
35		+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	00000
36		+	+	+	+	+	.	.	.	.	.	.	0					

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2637.	1726.	0.1077	0.0000E+00	875.0	0.0000E+00	13.50	0.100000E-01
2	2636.	1726.	0.8339E-01	0.0000E+00	903.0	0.0000E+00	13.50	0.100000E-01
3	2636.	1726.	0.7035E-01	0.0000E+00	930.9	0.0000E+00	13.50	0.100000E-01
4	2635.	1726.	0.5566E-01	0.0000E+00	955.0	0.0000E+00	13.50	0.100000E-01
5	2635.	1726.	0.4282E-01	0.0000E+00	974.8	0.0000E+00	13.50	0.100000E-01
6	2635.	1726.	0.3355E-01	0.0000E+00	990.9	0.0000E+00	13.50	0.100000E-01
7	2635.	1726.	0.2693E-01	0.0000E+00	1004.	0.0000E+00	13.50	0.100000E-01
8	2634.	1725.	0.2279E-01	0.0000E+00	1016.	0.0000E+00	13.50	0.100000E-01
9	2634.	1725.	0.1937E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
10	2634.	1725.	0.1644E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
11	2634.	1725.	1.051	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.62383
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25442
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10376
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
23	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
25	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
26	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
27	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
28	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
29	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0
30	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
31	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
32	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
36	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
37	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0
39	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
40	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0
41	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
42	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
43	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
56	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
57	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
58	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
59	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
60	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3709.	1801.	0.7308E-02	0.0000E+00	1414.	0.0000E+00	0.100000E-01
2	3709.	1801.	0.5657E-02	0.0000E+00	1447.	0.0000E+00	0.100000E-01
3	3708.	1801.	0.4772E-02	0.0000E+00	1480.	0.0000E+00	0.100000E-01
4	3708.	1801.	0.3776E-02	0.0000E+00	1508.	0.0000E+00	0.100000E-01
5	3708.	1801.	0.2905E-02	0.0000E+00	1531.	0.0000E+00	0.100000E-01
6	3708.	1801.	0.2276E-02	0.0000E+00	1550.	0.0000E+00	0.100000E-01
7	3707.	1801.	0.1827E-02	0.0000E+00	1566.	0.0000E+00	0.100000E-01
8	3707.	1801.	0.1546E-02	0.0000E+00	1579.	0.0000E+00	0.100000E-01
9	3707.	1801.	0.1314E-02	0.0000E+00	1591.	0.0000E+00	0.100000E-01
10	3707.	1801.	0.1115E-02	0.0000E+00	1601.	0.0000E+00	0.100000E-01
11	3707.	1801.	0.7127E-01	0.0000E+00	1603.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.42318E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17259E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.70389E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4782.	1877.	0.4957E-03	0.0000E+00	2037.	0.0000E+00	13.50	0.100000E-01
2	4782.	1877.	0.3838E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	4781.	1877.	0.3237E-03	0.0000E+00	2111.	0.0000E+00	13.50	0.100000E-01
4	4781.	1877.	0.2561E-03	0.0000E+00	2143.	0.0000E+00	13.50	0.100000E-01
5	4781.	1877.	0.1970E-03	0.0000E+00	2169.	0.0000E+00	13.50	0.100000E-01
6	4780.	1877.	0.1544E-03	0.0000E+00	2191.	0.0000E+00	13.50	0.100000E-01
7	4780.	1877.	0.1239E-03	0.0000E+00	2208.	0.0000E+00	13.50	0.100000E-01
8	4780.	1877.	0.1049E-03	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
9	4780.	1877.	0.8914E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
10	4780.	1877.	0.7563E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
11	4780.	1877.	0.4835E-02	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1351.5

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1834.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 562.96

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2623.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 439.38

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2746.6

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1521.	1647.	109.6	0.0000E+00	435.4	0.0000E+00	0.200000E-02
2	1563.	1650.	4.474	0.0000E+00	457.2	0.0000E+00	0.200000E-02
3	1563.	1650.	3.999	0.0000E+00	479.1	0.0000E+00	0.200000E-02
4	1563.	1650.	3.201	0.0000E+00	498.2	0.0000E+00	0.200000E-02
5	1562.	1650.	2.453	0.0000E+00	513.9	0.0000E+00	0.200000E-02
6	1562.	1650.	1.918	0.0000E+00	526.7	0.0000E+00	0.200000E-02
7	1562.	1650.	1.539	0.0000E+00	537.4	0.0000E+00	0.200000E-02
8	1562.	1650.	1.281	0.0000E+00	546.5	0.0000E+00	0.200000E-02
9	1561.	1650.	1.097	0.0000E+00	554.5	0.0000E+00	0.200000E-02
10	1561.	1650.	0.9626	0.0000E+00	561.7	0.0000E+00	0.200000E-02
11	1420.	1640.	308.8	0.0000E+00	562.9	0.2463	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 367.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2818.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 307.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2878.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 257.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2928.5

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2594.	1723.	64.26	0.0000E+00	875.0	0.0000E+00	0.200000E-02
2	2636.	1726.	2.622	0.0000E+00	903.0	0.0000E+00	0.200000E-02
3	2636.	1726.	2.344	0.0000E+00	930.9	0.0000E+00	0.200000E-02
4	2635.	1726.	1.876	0.0000E+00	955.0	0.0000E+00	0.200000E-02
5	2635.	1726.	1.438	0.0000E+00	974.8	0.0000E+00	0.200000E-02
6	2635.	1726.	1.124	0.0000E+00	990.9	0.0000E+00	0.200000E-02
7	2635.	1726.	0.9021	0.0000E+00	1004.	0.0000E+00	0.200000E-02
8	2634.	1725.	0.7508	0.0000E+00	1016.	0.0000E+00	0.200000E-02
9	2634.	1725.	0.6427	0.0000E+00	1026.	0.0000E+00	0.200000E-02
10	2634.	1725.	0.5642	0.0000E+00	1035.	0.0000E+00	0.200000E-02
11	2493.	1716.	181.0	0.0000E+00	1036.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 215.50
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2970.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.34
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3005.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 150.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.1

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
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[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.13	.11	.08	.06	.04	.03	.02	0	0	0	0	0	0	0	0	0	0
34		.20	.16	.13	.10	.07	.05	.03	0	0	0	0	0	0	0	0	0	0
35		.31	.25	.19	.15	.11	.08	.05	0	0	0	0	0					

[illegible]

$$0 \dots + = .LT. .01 \quad . = .LT.$$

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	00000
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	00000
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	00000
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	00000
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	00000
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	00000
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	00000
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0	00000
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	00000
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	00000
30	.06	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	.	.0000
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.0000
32	.08	.04	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.	.0000
33	.09	.05	.03	.01	+	+	+	+	+	+	+	+	.	.	.	.	.0000
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	.0000
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	.0000
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	.0000
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
38	.15	.09	.06	.03	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
39	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.0000
40	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	.0000
41	.16	.11	.07	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
42	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
43	.16	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.0000
44	.16	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
45	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
46	.15	.11	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
47	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
48	.13	.09	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
49	.11	.09	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+0000
50	.10	.08	.06	.04	.03	.02	.01	.	+	+	+	+	+	+	+	+	+0000
51	.09	.07	.05	.04	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
52	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+0000
53	.06	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	.0000
54	.05	.04	.03	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
55	.04	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	.0000
56	.03	.02	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.0000
57	.02	.02	.01	.01	.	+	+	+	+	+	+	+	+	+	+	+	.0000
58	.02	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.0000
59	.01	.01	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000
60	.01	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3666.	1798.	37.66	0.0000E+00	1414.	0.0000E+00	0.200000E-02
2	3709.	1801.	1.537	0.0000E+00	1447.	0.0000E+00	0.200000E-02
3	3708.	1801.	1.374	0.0000E+00	1480.	0.0000E+00	0.200000E-02
4	3708.	1801.	1.099	0.0000E+00	1508.	0.0000E+00	0.200000E-02
5	3708.	1801.	0.8428	0.0000E+00	1531.	0.0000E+00	0.200000E-02
6	3708.	1801.	0.6587	0.0000E+00	1550.	0.0000E+00	0.200000E-02
7	3707.	1801.	0.5287	0.0000E+00	1566.	0.0000E+00	0.200000E-02
8	3707.	1801.	0.4401	0.0000E+00	1579.	0.0000E+00	0.200000E-02
9	3707.	1801.	0.3767	0.0000E+00	1591.	0.0000E+00	0.200000E-02
10	3707.	1801.	0.3307	0.0000E+00	1601.	0.0000E+00	0.200000E-02
11	3566.	1791.	106.1	0.0000E+00	1603.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.30
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3059.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.70
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3080.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.453
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3096.7

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0	0
43	.12	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.01	0	0	0	0	0
44	.15	.14	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0	0
45	.20	.18	.16	.14	.13	.11	.09	.07	.06	.05	.04	.03	0	0	0	0	0
46	.26	.24	.21	.19	.16	.14	.12	.10	.08	.06	.05	.04	0	0	0	0	0
47	.34	.31	.27	.24	.21	.18	.15	.12	.10	.08	.06	.05	0	0	0	0	0
48	.42	.38	.34	.30	.26	.23	.19	.16	.13	.10	.08	.06	0	0	0	0	0
49	.53	.48	.43	.38	.33	.28	.24	.20	.16	.13	.10	.08	0	0	0	0	0
50	.64	.58	.52	.46	.40	.34	.29	.24	.20	.16	.12	.10	0	0	0	0	0
51	.78	.70	.63	.55	.48	.41	.35	.29	.24	.19	.15	.12	0	0	0	0	0
52	.92	.84	.75	.66	.57	.49	.41	.34	.28	.23	.18	.14	0	0	0	0	0
53	1.0	.98	.88	.77	.67	.57	.48	.40	.33	.26	.21	.16	0	0	0	0	0
54	1.2	1.1	1.0	.89	.77	.66	.56	.46	.38	.31	.24	.19	0	0	0	0	0
55	1.4	1.2	1.1	1.0	.88	.75	.63	.53	.43	.35	.28	.22	0	0	0	0	0
56	1.5	1.4	1.2	1.1	.99	.84	.71	.59	.48	.39	.31	.24	0	0	0	0	0
57	1.7	1.6	1.4	1.2	1.0	.93	.79	.65	.53	.43	.34	.27	0	0	0	0	0
58	1.9	1.7	1.5	1.3	1.1	1.0	.86	.71	.58	.47	.37	.29	0	0	0	0	0
59	2.0	1.8	1.6	1.4	1.2	1.0	.92	.76	.62	.50	.40	.31	0	0	0	0	0
60	2.1	1.9	1.7	1.5	1.3	1.1	.97	.81	.66	.53	.42	.33	0	0	0	0	0

[illegible]

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4739.	1874.	22.07	0.0000E+00	2037.	0.0000E+00	13.50	0.200000E-02
2	4782.	1877.	0.9008	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	4781.	1877.	0.8050	0.0000E+00	2111.	0.0000E+00	13.50	0.200000E-02
4	4781.	1877.	0.6444	0.0000E+00	2143.	0.0000E+00	13.50	0.200000E-02
5	4781.	1877.	0.4939	0.0000E+00	2169.	0.0000E+00	13.50	0.200000E-02
6	4780.	1877.	0.3861	0.0000E+00	2191.	0.0000E+00	13.50	0.200000E-02
7	4780.	1877.	0.3099	0.0000E+00	2208.	0.0000E+00	13.50	0.200000E-02
8	4780.	1877.	0.2579	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
9	4780.	1877.	0.2208	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
10	4780.	1877.	0.1938	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
11	4639.	1867.	62.17	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
18	+	+	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
20	+	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0
21	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
22	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0
24	.01	+	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0
25	.01	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0
26	.02	.01	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0
27	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
28	.04	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
29	.05	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
30	.06	.03	.01	+	+	+	+	+	+	.	.	.	.	.	.	.	0
31	.07	.03	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
32	.08	.04	.02	.01	+	+	+	+	+	+	.	.	.	.	.	.	0
33	.09	.05	.03	.01	+	+	+	+	+	+	+	.	.	.	.	.	0
34	.11	.06	.03	.02	.01	+	+	+	+	+	+	+	.	.	.	.	0
35	.12	.07	.04	.02	.01	+	+	+	+	+	+	+	+	.	.	.	0
36	.13	.08	.05	.03	.01	.01	+	+	+	+	+	+	+	+	.	.	0
37	.14	.09	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	.	0
38	.15	.10	.06	.04	.02	.01	+	+	+	+	+	+	+	+	+	+	0
39	.16	.11	.07	.04	.03	.01	.01	+	+	+	+	+	+	+	+	+	0
40	.17	.11	.08	.05	.03	.02	.01	+	+	+	+	+	+	+	+	+	0
41	.17	.12	.08	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	+	0
42	.18	.13	.09	.06	.04	.02	.01	.01	+	+	+	+	+	+	+	+	0
43	.18	.13	.09	.06	.04	.03	.02	.01	+	+	+	+	+	+	+	+	0
44	.18	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
45	.19	.14	.10	.07	.05	.03	.02	.01	.01	+	+	+	+	+	+	+	0
46	.19	.14	.11	.08	.05	.04	.02	.02	.01	+	+	+	+	+	+	+	0
47	.19	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
48	.18	.14	.11	.08	.06	.04	.03	.02	.01	.01	+	+	+	+	+	+	0
49	.18	.14	.11	.08	.06	.05	.03	.02	.01	.01	+	+	+	+	+	+	0
50	.18	.14	.11	.09	.06	.05	.03	.02	.02	.01	.01	+	+	+	+	+	0
51	.17	.14	.11	.09	.07	.05	.04	.02	.02	.01	.01	+	+	+	+	+	0
52	.17	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
53	.16	.14	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
54	.16	.13	.11	.09	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
55	.15	.13	.11	.08	.07	.05	.04	.03	.02	.01	.01	+	+	+	+	+	0
56	.15	.12	.10	.08	.07	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
57	.14	.12	.10	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
58	.13	.11	.09	.08	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
59	.12	.11	.09	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0
60	.12	.10	.08	.07	.06	.05	.04	.03	.02	.01	.01	.01	+	+	+	+	0

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF DDx

SUMMARY OF DDx DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 1200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	846.0	1599.	0.2269E+09	0.4766E+08	309.5	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 2400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 2400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1204.	1625.	0.2670E+09	0.8784E+08	429.3	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 3600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1561.	1650.	0.3329E+09	0.1537E+09	562.9	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 4800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 4800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	1919.	1675.	0.4254E+09	0.2462E+09	709.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 6000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 6000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2276.	1700.	0.5491E+09	0.3699E+09	867.2	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 7200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
```

[illegible]

[illegible]

[illegible]

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	2634.	1725.	0.7089E+09	0.5297E+09	1036.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 8400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 8400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	2992.	1751.	0.9095E+09	0.7303E+09	1215.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 9600.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 9600.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3349.	1776.	0.1156E+10	0.9764E+09	1404.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 10800.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

M	N = 32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
36	+	+	+	+	+	+	+	0	0	0	0	0	0	0	0	0	0
37	+	+	+	+													

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	3707.	1801.	0.1452E+10	0.1273E+10	1603.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 12000.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 12000.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4064.	1826.	0.1804E+10	0.1624E+10	1810.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 13200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

SMALL CLOUDS AT 13200.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	LEFT OF GRID						
1	4422.	1851.	0.2215E+10	0.2036E+10	2026.	0.0000E+00	13.50	0.000000E+00

SUMMARY OF DDx DISTRIBUTIONS AFTER 14400.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.17920E+09

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.31	.28	.25	.22	.19	.17	.14	.12	.10	.08	.06	.05	0	0	0	0	0
45	.41	.37	.33	.30	.26	.22	.19	.16	.13	.11	.08	.07	0	0	0	0	0
46	.53	.49	.44	.39	.34	.29	.25	.21	.17	.14	.11	.09	0	0	0	0	0
47	.69	.63	.57	.50	.44	.38	.32	.27	.22	.18	.15	.11	0	0	0	0	0
48	.88	.80	.72	.64	.56	.48	.41	.35	.28	.23	.19	.15	0	0	0	0	0
49	1.1	1.0	.91	.81	.71	.61	.52	.43	.36	.29	.23	.19	0	0	0	0	0
50	1.3	1.2	1.1	1.0	.87	.75	.64	.54	.44	.36	.29	.23	0	0	0	0	0
51	1.6	1.5	1.3	1.2	1.0	.92	.78	.66	.54	.44	.36	.28	0	0	0	0	0
52	2.0	1.8	1.6	1.4	1.2	1.1	.94	.79	.66	.53	.43	.34	0	0	0	0	0
53	2.3	2.1	1.9	1.7	1.5	1.3	1.1	.94	.78	.63	.51	.40	0	0	0	0	0
54	2.7	2.5	2.2	2.0	1.7	1.5	1.3	1.1	.91	.74	.60	.47	0	0	0	0	0
55	3.2	2.9	2.6	2.3	2.0	1.7	1.5	1.2	1.0	.86	.69	.55	0	0	0	0	0
56	3.6	3.3	3.0	2.6	2.3	2.0	1.7	1.4	1.2	.98	.79	.62	0	0	0	0	0
57	4.1	3.7	3.3	3.0	2.6	2.2	1.9	1.6	1.3	1.1	.88	.70	0	0	0	0	0
58	4.5	4.1	3.7	3.3	2.9	2.5	2.1	1.7	1.4	1.2	.98	.77	0	0	0	0	0
59	4.9	4.5	4.0	3.6	3.1	2.7	2.3	1.9	1.6	1.3	1.0	.85	0	0	0	0	0
60	5.3	4.8	4.3	3.8	3.4	2.9	2.5	2.1	1.7	1.4	1.1	.91	0	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM OCCURING IN THE WATER COLUMN AT THIS TIME

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	.01	.01	+	+	+	+	+	+	+	+	+	+	0	0	0	0	0
45	.01	.01	.01	.01	+	+	+	+	+	+	+	+	0	0	0	0	0
46	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	0	0	0	0	0
47	.02	.02	.02	.01	.01	.01	.01	.01	+	+	+	+	0	0	0	0	0
48	.03	.02	.02	.02	.02	.01	.01	.01	.01	+	+	+	0	0	0	0	0
49	.04	.03	.03	.02	.02	.02	.01	.01	.01	.01	+	+	0	0	0	0	0
50	.05	.04	.04	.03	.03	.02	.02	.02	.01	.01	.01	+	0	0	0	0	0
51	.06	.05	.05	.04	.03	.03	.02	.02	.02	.01	.01	.01	0	0	0	0	0
52	.07	.06	.06	.05	.04	.04	.03	.02	.02	.01	.01	.01	0	0	0	0	0
53	.08	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	.01	0	0	0	0	0
54	.10	.09	.08	.07	.06	.05	.04	.04	.03	.02	.02	.01	0	0	0	0	0
55	.11	.10	.09	.08	.07	.06	.05	.04	.03	.03	.02	.02	0	0	0	0	0
56	.13	.12	.11	.09	.08	.07	.06	.05	.04	.03	.02	.02	0	0	0	0	0
57	.15	.13	.12	.11	.09	.08	.07	.06	.04	.04	.03	.02	0	0	0	0	0
58	.16	.15	.13	.12	.10	.09	.07	.06	.05	.04	.03	.02	0	0	0	0	0
59	.18	.16	.15	.13	.11	.10	.08	.07	.06	.04	.03	.03	0	0	0	0	0
60	.19	.18	.16	.14	.12	.10	.09	.07	.06	.05	.04	.03	0	0	0	0	0

[illegible]

THESE CONCENTRATIONS ARE THE MAXIMUM THAT EVER OCCURRED IN THE WATER COLUMN DURING THE SIMULATION

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.03	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.04	+	+	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.07	.01	.01	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.09	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0	0	0
33	.12	.03	.02	+	+	0	0	0	0	0	0	0	0	0	0	0	0
34	.14	.05	.03	+	+	0	0	0	0	0	0	0	0	0	0	0	0
35	.16	.07	.04	.01	+	+	+	0	0	0	0	0	0	0	0	0	0
36	.17	.09	.06	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0
37	.17	.11	.07	.02	.01	+	+	0	0	0	0	0	0	0	0	0	0
38	.20	.13	.08	.03	.02	+	+	+	0	0	0	0	0	0	0	0	0
39	.22	.15	.09	.05	.03	.01	+	+	0	0	0	0	0	0	0	0	0
40	.24	.16	.10	.06	.04	.01	.01	+	0	0	0	0	0	0	0	0	0
41	.24	.16	.10	.07	.05	.02	.01	+	+	+	0	0	0	0	0	0	0
42	.24	.17	.12	.08	.06	.03	.02	+	+	+	0	0	0	0	0	0	0
43	.25	.19	.14	.09	.06	.03	.02	.01	+	+	+	0	0	0	0	0	0
44	.27	.20	.15	.10	.07	.04	.03	.01	+	+	+	+	0	0	0	0	0
45	.28	.21	.15	.11	.07	.05	.03	.01	+	+	+	+	0	0	0	0	0
46	.28	.21	.15	.11	.08	.06	.04	.02	.01	+	+	+	0	0	0	0	0
47	.28	.21	.16	.12	.09	.06	.04	.02	.01	.01	+	+	0	0	0	0	0
48	.27	.22	.17	.13	.10	.07	.05	.03	.01	.01	+	+	0	0	0	0	0
49	.28	.23	.18	.14	.10	.07	.05	.04	.02	.01	+	+	0	0	0	0	0
50	.29	.24	.19	.14	.11	.08	.06	.04	.02	.02	.01	+	0	0	0	0	0
51	.29	.24	.19	.14	.11	.08	.06	.05	.03	.02	.01	.01	0	0	0	0	0
52	.28	.23	.18	.14	.12	.09	.07	.05	.03	.02	.01	.01	0	0	0	0	0
53	.27	.23	.19	.15	.12	.10	.07	.05	.04	.03	.01	.01	0	0	0	0	0
54	.27	.23	.20	.16	.13	.10	.08	.06	.04	.03	.02	.01	0	0	0	0	0
55	.28	.24	.20	.16	.13	.10	.08	.06	.05	.03	.02	.02	0	0	0	0	0
56	.28	.24	.20	.16	.13	.10	.08	.06	.05	.04	.02	.02	0	0	0	0	0
57	.27	.23	.19	.16	.13	.11	.09	.07	.05	.04	.03	.02	0	0	0	0	0
58	.26	.22	.19	.16	.14	.11	.09	.07	.06	.04	.03	.02	0	0	0	0	0
59	.25	.22	.19	.17	.14	.12	.09	.07	.06	.04	.03	.03	0	0	0	0	0
60	.25	.23	.20	.17	.14	.12	.09	.07	.06	.05	.04	.03	0	0	0	0	0

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR DDx

CLOUD #	LOCATION OF CLOUD CENTROID		MASS FROM DISPOSAL (MG)	ENTRAINED MASS (MG)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
	TOP OF GRID	DISTANCE FROM LEFT OF GRID						
1	4780.	1877.	0.2691E+10	0.2512E+10	2250.	0.0000E+00	13.50	0.000000E+00

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
22	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
23	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
24	+	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0
25	+	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0
26	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0
27	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
28	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
29	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
30	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0
31	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0
32	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
33	.01	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0
34	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
35	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
36	.01	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
37	.01	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	0
38	.01	.01	+															

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.134E+02	1575.	1650.
2.00	0.0	0.259E+00	2625.	1725.
3.00	0.0	0.718E-02	3675.	1800.
4.00	0.0	0.245E-03	4800.	1875.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.237E+03	1500.	1650.
2.00	0.0	0.442E+02	2550.	1725.
3.00	0.0	0.106E+02	3600.	1800.
4.00	0.0	0.312E+01	4650.	1875.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR DDx

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.395E+01	0.525E+01	825.	1575.
0.67	0.0	0.215E+01	0.345E+01	1200.	1650.
1.00	0.0	0.127E+01	0.257E+01	1575.	1650.
1.33	0.0	0.789E+00	0.209E+01	1950.	1650.
1.67	0.0	0.533E+00	0.183E+01	2250.	1725.
2.00	0.0	0.377E+00	0.168E+01	2625.	1725.
2.33	0.0	0.273E+00	0.157E+01	3000.	1725.
2.67	0.0	0.205E+00	0.150E+01	3375.	1800.
3.00	0.0	0.157E+00	0.146E+01	3675.	1800.
3.33	0.0	0.123E+00	0.142E+01	4050.	1800.
3.67	0.0	0.986E-01	0.140E+01	4425.	1875.
4.00	0.0	0.799E-01	0.138E+01	4800.	1875.
0.33	6.8	0.146E+02	0.159E+02	825.	1575.
0.67	6.8	0.794E+01	0.924E+01	1200.	1650.
1.00	6.8	0.471E+01	0.601E+01	1575.	1650.
1.33	6.8	0.292E+01	0.422E+01	1950.	1650.
1.67	6.8	0.197E+01	0.327E+01	2250.	1725.
2.00	6.8	0.139E+01	0.269E+01	2625.	1725.
2.33	6.8	0.101E+01	0.231E+01	3000.	1725.
2.67	6.8	0.756E+00	0.206E+01	3375.	1800.
3.00	6.8	0.581E+00	0.188E+01	3675.	1800.
3.33	6.8	0.456E+00	0.176E+01	4050.	1800.
3.67	6.8	0.364E+00	0.166E+01	4425.	1875.
4.00	6.8	0.295E+00	0.160E+01	4800.	1875.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

TIME	SNAPSHOT			ACCUMULATED		
(SEC)	AREA(SQ FT)	L(FT)	W(FT)	AREA(SQ FT)	L(FT)	W(FT)
1200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
2400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
3600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
4800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
6000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
7200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
8400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
9600.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
10800.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
12000.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
13200.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.
14400.0	0.201206E+08	6594.	3051.	0.201206E+08	6594.	3051.

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1800. FT (ZBARGE) OR ABOUT GRID POINT #25 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050.	1800.	1) = 143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050.	1800.	1) = 159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050.	1800.	1) = 171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050.	1800.	1) = 181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050.	1800.	1) = 189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050.	1800.	1) = 195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050.	1800.	1) = 201.6	11.25	0.9467E-01	2.328	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050.	1800.	1) = 206.7	11.34	0.7957E-01	2.002	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050.	1800.	1) = 211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050.	1800.	1) = 215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050.	1800.	2) = 1 143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050.	1800.	2) = 2 159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050.	1800.	2) = 3 171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050.	1800.	2) = 4 181.1	10.80	0.1911	7.460	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050.	1800.	2) = 5 189.1	10.99	0.1448	5.883	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050.	1800.	2) = 6 195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050.	1800.	2) = 7 201.6	11.25	0.9467E-01	4.081	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050.	1800.	2) = 8 206.7	11.34	0.7957E-01	3.513	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050.	1800.	2) = 9 211.1	11.42	0.6810E-01	3.067	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050.	1800.	2) = 10 215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050. 1800.	3) = 143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050. 1800.	3) = 159.3	10.08	0.4471	6.961	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050. 1800.	3) = 171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050. 1800.	3) = 181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050. 1800.	3) = 189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050. 1800.	3) = 195.8	11.13	0.1152	2.191	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050. 1800.	3) = 201.6	11.25	0.9467E-01	1.850	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050. 1800.	3) = 206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050. 1800.	3) = 211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050. 1800.	3) = 215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050. 1800.	4) = 1 143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050. 1800.	4) = 2 159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050. 1800.	4) = 3 171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050. 1800.	4) = 4 181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050. 1800.	4) = 5 189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050. 1800.	4) = 6 195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050. 1800.	4) = 7 201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050. 1800.	4) = 8 206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050. 1800.	4) = 9 211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050. 1800.	4) = 10 215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID		CLOUD X-Z	DEPTH OF	CLOUD VERT.	T O T A L	ENTRAINED	TIME STEP WHEN	TIME STEP WHEN
	X-LOCATION	Z-LOCATION	DIAMETER	TOP OF CLOUD	THICKNESS	M A S S	MASS	THIS CLOUD	PREVIOUS CLOUD
	(FT)	(FT)	(FT)	(FT)	(FT)	(MG)	(MG)	WAS CREATED	WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 5) = 1 33.07	5050.	1800.	215.1	10.07	3.431	0.00000E+00	0.00000E+00	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 148.20

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7087.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 59.434

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7176.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 24.240

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7211.7

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID	LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	3.837	0.0000E+00	466.9	0.0000E+00	13.50	0.100000E-01
2	3986.	1518.	0.9250	0.0000E+00	491.6	0.0000E+00	13.50	0.100000E-01
3	3986.	1518.	0.6056	0.0000E+00	509.9	0.0000E+00	13.50	0.100000E-01
4	3986.	1518.	0.4176	0.0000E+00	524.4	0.0000E+00	13.50	0.100000E-01
5	3986.	1518.	0.3501	0.0000E+00	536.2	0.0000E+00	13.50	0.100000E-01
6	3987.	1518.	0.2869	0.0000E+00	546.1	0.0000E+00	13.50	0.100000E-01
7	3987.	1518.	0.2452	0.0000E+00	554.5	0.0000E+00	13.50	0.100000E-01
8	3987.	1518.	0.2103	0.0000E+00	561.8	0.0000E+00	13.50	0.100000E-01
9	3987.	1518.	0.1818	0.0000E+00	568.2	0.0000E+00	13.50	0.100000E-01
10	3987.	1518.	17.18	0.0000E+00	573.9	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.8858
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.0318
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6443
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.3

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913. 1234.	0.2603	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2913. 1234.	0.6275E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2913. 1234.	0.4108E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2914. 1234.	0.2833E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2914. 1234.	0.2375E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2914. 1234.	0.1946E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2914. 1234.	0.1663E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2914. 1234.	0.1426E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2914. 1234.	0.1233E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2914. 1234.	1.165	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.67062
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.27350
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.11155
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
36	.	.	.	.</														

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1840.	949.2	0.1766E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	1840.	949.2	0.4257E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	1841.	949.2	0.2787E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	1841.	949.2	0.1922E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	1841.	949.3	0.1611E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	1841.	949.3	0.1320E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	1841.	949.3	0.1128E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	1841.	949.3	0.9676E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	1841.	949.4	0.8367E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	1841.	949.4	0.7906E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.45492E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18554E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.75668E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.5	664.8	0.1198E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	767.7	664.8	0.2888E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	767.8	664.8	0.1890E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	767.9	664.8	0.1304E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	768.0	664.9	0.1093E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	768.1	664.9	0.8957E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	768.2	664.9	0.7653E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	768.3	664.9	0.6564E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	768.4	665.0	0.5676E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	768.5	665.0	0.5363E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1425.6

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1852.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 621.88

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2655.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 494.15

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2783.6

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4002.	1522.	142.4	0.0000E+00	466.9	0.0000E+00	0.200000E-02
2	3986.	1518.	4.088	0.0000E+00	491.6	0.0000E+00	0.200000E-02
3	3986.	1518.	2.691	0.0000E+00	509.9	0.0000E+00	0.200000E-02
4	3986.	1518.	1.961	0.0000E+00	524.4	0.0000E+00	0.200000E-02
5	3986.	1518.	1.544	0.0000E+00	536.2	0.0000E+00	0.200000E-02
6	3987.	1518.	1.267	0.0000E+00	546.1	0.0000E+00	0.200000E-02
7	3987.	1518.	1.070	0.0000E+00	554.5	0.0000E+00	0.200000E-02
8	3987.	1518.	0.9200	0.0000E+00	561.8	0.0000E+00	0.200000E-02
9	3987.	1518.	0.8023	0.0000E+00	568.2	0.0000E+00	0.200000E-02
10	4109.	1550.	337.4	0.0000E+00	573.9	0.4899E-01	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 413.53
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2864.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 346.07
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2931.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 289.61
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2988.2

0.00 FT BELOW THE WATER SURFACE

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M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

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M	N =	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
34	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
35	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
36	+	+	.	.														

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2929.	1238.	83.49	0.0000E+00	915.3	0.0000E+00	0.200000E-02
2	2913.	1234.	2.396	0.0000E+00	946.7	0.0000E+00	0.200000E-02
3	2913.	1234.	1.577	0.0000E+00	969.8	0.0000E+00	0.200000E-02
4	2914.	1234.	1.149	0.0000E+00	987.9	0.0000E+00	0.200000E-02
5	2914.	1234.	0.9050	0.0000E+00	1003.	0.0000E+00	0.200000E-02
6	2914.	1234.	0.7423	0.0000E+00	1015.	0.0000E+00	0.200000E-02
7	2914.	1234.	0.6273	0.0000E+00	1026.	0.0000E+00	0.200000E-02
8	2914.	1234.	0.5392	0.0000E+00	1035.	0.0000E+00	0.200000E-02
9	2914.	1234.	0.4702	0.0000E+00	1043.	0.0000E+00	0.200000E-02
10	3036.	1266.	197.7	0.0000E+00	1050.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 242.37
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 202.83
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3074.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 169.74
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3107.6

0.00 FT BELOW THE WATER SURFACE

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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1856.	953.4	48.93	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	1840.	949.2	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	1841.	949.2	0.9245	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	1841.	949.2	0.6735	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	1841.	949.3	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	1841.	949.3	0.4351	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	1841.	949.3	0.3676	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	1841.	949.3	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	1841.	949.4	0.2756	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	1963.	981.7	115.9	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 142.05
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3134.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 118.88
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3157.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 99.482
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3175.5

0.00 FT BELOW THE WATER SURFACE

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3	0000	1.2	1.3	1.5	1.6	1.7	1.7	1.8	1.8	1.8	1.7	1.7	1.7	1.6	1.5	1.4	1.3	1.1	1.0	.90	.77	.66	.55	.45	.37	.29	.23	.18	0	0	0
4	0000	1.4	1.5	1.7	1.8	1.9	2.0	2.0	2.0	2.0	2.0	1.9	1.8	1.7	1.6	1.4	1.3	1.1	1.0	.88	.75	.62	.51	.42	.33	.26	.20	0	0	0	
5	0000	1.6	1.7	1.9	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.9	1.8	1.6	1.4	1.3	1.1	.99	.84	.70	.58	.47	.37	.29	.23	0	0	0	
6	0000	1.7	1.9	2.1	2.2	2.3	2.4	2.5	2.5	2.5	2.5	2.4	2.3	2.1	2.0	1.8	1.6	1.4	1.2	1.0	.92	.77	.64	.52	.41	.33	.25	0	0	0	
7	0000	1.9	2.1	2.3	2.4	2.6	2.7	2.7	2.8	2.7	2.7	2.6	2.5	2.3	2.1	1.9	1.7	1.5	1.3	1.1	1.0	.84	.69	.56	.45	.35	.28	0	0	0	
8	0000	2.0	2.2	2.4	2.6	2.7	2.9	2.9	3.0	2.9	2.9	2.8	2.6	2.5	2.3	2.1	1.9	1.7	1.4	1.2	1.0	.90	.74	.60	.48	.38	.30	0	0	0	
9	0000	2.1	2.4	2.6	2.8	2.9	3.0	3.1	3.1	3.1	3.0	2.9	2.8	2.6	2.4	2.2	2.0	1.7	1.5	1.3	1.1	.95	.79	.64	.51	.40	.31	0	0	0	
10	0000	2.2	2.5	2.7	2.9	3.0	3.2	3.2	3.3	3.2	3.2	3.1	2.9	2.7	2.5	2.3	2.1	1.8	1.6	1.4	1.1	1.0	.82	.67	.53	.42	.33	0	0	0	
11	0000	2.3	2.5	2.8	2.9	3.1	3.2	3.3	3.3	3.3	3.3	3.2	3.0	2.8	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	.84	.69	.55	.43	.34	0	0	0	
12	0000	2.3	2.6	2.8	3.0	3.1	3.3	3.4	3.4	3.4	3.3	3.2	3.0	2.8	2.6	2.4	2.1	1.9	1.7	1.4	1.2	1.0	.85	.69	.56	.44	.34	0	0	0	
13	0000	2.3	2.6	2.8	3.0	3.1	3.3	3.3	3.4	3.4	3.3	3.2	3.0	2.8	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	.85	.69	.56	.44	.34	0	0	0	
14	0000	2.3	2.5	2.7	2.9	3.1	3.2	3.3	3.3	3.3	3.2	3.1	3.0	2.8	2.6	2.4	2.1	1.9	1.6	1.4	1.2	1.0	.84	.68	.55	.43	.34	0	0	0	
15	0000	2.2	2.4	2.6	2.8	3.0	3.1	3.2	3.2	3.2	3.1	3.0	2.9	2.7	2.5	2.3	2.0	1.8	1.6	1.3	1.1	.99	.82	.66	.53	.42	.33	0	0	0	
16	0000	2.1	2.3	2.5	2.7	2.9	3.0	3.0	3.1	3.1	3.0	2.9	2.8	2.6	2.4	2.2	2.0	1.7	1.5	1.3	1.1	.95	.78	.63	.51	.40	.31	0	0	0	
17	0000	2.0	2.2	2.4	2.5	2.7	2.8	2.9	2.9	2.9	2.8	2.7	2.6	2.4	2.2	2.0	1.8	1.6	1.4	1.2	1.0	.89	.74	.60	.48	.38	.29	0	0	0	

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M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
4		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
5		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
6		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
7		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
8		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
9		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
10		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
11		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
12		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
13		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
14		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
15		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
16		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
17		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
18		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
19		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
20		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
21		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
22		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
23		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
24		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
25		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
26		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
27		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
29		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
30		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
31		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
32		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
33		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
34		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
35		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
36		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
37		+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.0000
38		+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.0000
39		+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.0000
40		+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.0000
41		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
42		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
43		+	+															

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	783.4	669.0	28.68	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	767.7	664.8	0.8230	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	767.8	664.8	0.5418	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	767.9	664.8	0.3948	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	768.0	664.9	0.3109	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	768.1	664.9	0.2550	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	768.2	664.9	0.2155	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	768.3	664.9	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	768.4	665.0	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	890.3	697.3	67.92	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02


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. .0001    0 = .LT. .000001)

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```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
4		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
5		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
6		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
7		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
8		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
9		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
10		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
11		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
12		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
13		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
14		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
15		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
16		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
17		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
18		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
19		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
20		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
21		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
22		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
23		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
24		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
25		+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.0000
26		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
27		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
28		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
29		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
30		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
31		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
32		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
33		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
34		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
35		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
36		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
37		+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.0000
38		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
39		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
40		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
41		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
42		+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.0000
43		+	+	+														

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
12	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
13	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
14	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
15	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.
20	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
22	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
26	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
27	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
28	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
29	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
30	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
31	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
32	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
33	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
34	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
35	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
36	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
37	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
38	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
39	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
40	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
41	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
42	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
43	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
44	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
45	0000	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
46	0000	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
47	0000	.	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
48	0000	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
49	0000	0	0	.	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
50	0000	0	0	0	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
51	0000	0	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
52	0000	0	0	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
53	0000	0	0	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.
54	0000	0	0	0	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
55	0000	0	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
56	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
57	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
58	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0
59	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	0

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
36		.	0	0	0	0												

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.137E+02	3975.	1500.
2.00	0.0	0.268E+00	2925.	1200.
3.00	0.0	0.754E-02	1875.	975.
4.00	0.0	0.259E-03	750.	675.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.261E+03	4050.	1500.
2.00	0.0	0.477E+02	3000.	1275.
3.00	0.0	0.116E+02	1950.	975.
4.00	0.0	0.344E+01	825.	675.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)  L(FT)    W(FT)    AREA(SQ FT)  L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1800. FT (ZBARGE) OR ABOUT GRID POINT #25 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1800.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050.	1800.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050.	1800.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050.	1800.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051.	1800.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051.	1800.	1) = 197.4	10.91	0.2177	34.31	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051.	1800.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051.	1800.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051.	1800.	1) = 224.8	11.43	0.1157	20.29	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051.	1800.	1) = 232.3	11.55	0.9998E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051.	1800.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1800.	2) = 1 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1800.	2) = 2 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050. 1800.	2) = 3 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050. 1800.	2) = 4 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051. 1800.	2) = 5 185.6	10.61	0.2974	8.983	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051. 1800.	2) = 6 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051. 1800.	2) = 7 207.6	11.12	0.1689	5.615	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051. 1800.	2) = 8 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051. 1800.	2) = 9 224.8	11.43	0.1157	4.103	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051. 1800.	2) = 10 232.3	11.55	0.9998E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051. 1800.	2) = 11 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1800.	3) = 113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050.	1800.	3) = 134.8	8.477	1.036	9.912	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050.	1800.	3) = 154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050.	1800.	3) = 171.6	10.18	0.4327	5.258	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051.	1800.	3) = 185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051.	1800.	3) = 197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051.	1800.	3) = 207.6	11.12	0.1689	2.427	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051.	1800.	3) = 216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051.	1800.	3) = 224.8	11.43	0.1157	1.774	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051.	1800.	3) = 232.3	11.55	0.9998E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051.	1800.	3) = 233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051.	1800.	4) = 1 233.4	9.779	3.721	0.0000E+00	0.0000E+00	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 173.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5895.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 70.243

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5999.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 28.648

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6040.9

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	3986.	1518.	2.455	0.0000E+00	419.0	0.0000E+00	13.50	0.100000E-01
2	3987.	1518.	1.545	0.0000E+00	453.4	0.0000E+00	13.50	0.100000E-01
3	3987.	1518.	1.105	0.0000E+00	484.4	0.0000E+00	13.50	0.100000E-01
4	3987.	1518.	0.7501	0.0000E+00	510.1	0.0000E+00	13.50	0.100000E-01
5	3987.	1518.	0.5458	0.0000E+00	531.0	0.0000E+00	13.50	0.100000E-01
6	3988.	1518.	0.4168	0.0000E+00	548.3	0.0000E+00	13.50	0.100000E-01
7	3988.	1518.	0.3357	0.0000E+00	563.0	0.0000E+00	13.50	0.100000E-01
8	3988.	1518.	0.2861	0.0000E+00	576.0	0.0000E+00	13.50	0.100000E-01
9	3988.	1518.	0.2456	0.0000E+00	587.6	0.0000E+00	13.50	0.100000E-01
10	3988.	1518.	0.2120	0.0000E+00	598.2	0.0000E+00	13.50	0.100000E-01
11	3988.	1518.	20.75	0.0000E+00	599.8	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.684
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6057.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.7651
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6064.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.9434
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.6

[illegible]

[illegible]

[illegible]

$$\dots + = .LT. .01 \quad . = .LT.$$

0 = .LT. .000001)

[illegible]

3 0000 0

[illegible][illegible][illegible][illegible][illegible][illegible][illegible][illegible]

23	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
24	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0

[illegible][illegible][illegible][illegible][illegible]

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37 0000 . . + + + + + + + + .01 .01 .02 .02 .02 .02 .02 .02 .02 .02 .01 .01 + + + + + + .
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39 0000	.	.	+	+	+	+	+	+	+	.01	.02	.02	.03	.04	.04	.05	.04	.04	.03	.02	.02	.01	+	+	+	+	+	+	+	+
40 0000	.	.	+	+	+	+	+	+	+	.01	.02	.02	.04	.05	.06	.06	.06	.05	.04	.03	.03	.01	.01	+	+	+	+	+	+	+

41 0000	.	.	+	+	+	+	+	+	.01	.01	.02	.03	.05	.06	.07	.08	.08	.07	.06	.04	.03	.02	.01	+	+	+	+	+	+
42 0000			+	+	+	+	+	+	.01	.01	.02	.04	.06	.07	.09	.10	.10	.09	.08	.06	.04	.02	.01	+	+	+	+	+	+

44 0000	.	.	+	+	+	+	+	+	.01	.01	.03	.05	.07	.10	.13	.15	.16	.15	.13	.10	.07	.04	.02	.01	+	+	+	+	+
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46	0000	.	.	.	+	+	+	+	+	+	.01	.03	.05	.08	.12	.17	.22	.25	.26	.23	.18	.13	.08	.04	.02	.01	+	+	+	+
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48 0000	.	.	.	+	+	+	+	+	+	.01	.02	.05	.09	.15	.23	.32	.38	.41	.38	.30	.21	.13	.07	.03	.01	+	+	+	+
40 0000										.01	.02	.04	.08	.15	.24	.35	.44	.48	.46	.38	.26	.16	.08	.04	.01	+	+	+	+

50.0000	.	.	.	.	.	.	.	.	.	.01	.04	.08	.13	.23	.37	.50	.57	.57	.49	.33	.21	.11	.03	.02	.	.	.	.	
51.0000	.	.	.	.	.	+	+	+	+	+	.01	.03	.07	.13	.24	.40	.58	.72	.77	.68	.50	.30	.15	.06	.02	+	+	+	+

53 0000 0 0 + + + + + .01 .04 .11 .25 .49 .85 1.2 1.4 1.3 .98 .58 .28 .11 .04 .01 + + +

55 0000	0	0	0	.	.	.	.	+	+	+	+	+	.02	.08	.20	.45	.84	1.3	1.6	1.6	1.3	.81	.40	.15	.05	.01	+	+	+
56 0000	0	0	0	0	0	0	0	0	0	0	0	0	.02	.05	.15	.25	.71	1.0	1.3	2.0	1.0	1.1	.50	.00	.00	.01	+	+	+

57	0000	0	0	0	0	0	.	.	.	.	+	+	+	.01	.03	.10	.26	.65	1.3	2.4	3.3	3.2	2.1	1.0	.36	.09	.02	+	+	.						
58	0000	0	0	0	0	0	0					+	+	+	+	.02	.06	.22	.67	1	7	3	6	5	4	5	4	3	5	1	6	.55	.14	.02	+	+

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913. 1234.	0.1665	0.0000E+00	853.9	0.0000E+00	13.50	0.100000E-01
2	2914. 1234.	0.1048	0.0000E+00	898.1	0.0000E+00	13.50	0.100000E-01
3	2914. 1234.	0.7498E-01	0.0000E+00	937.5	0.0000E+00	13.50	0.100000E-01
4	2914. 1234.	0.5088E-01	0.0000E+00	970.0	0.0000E+00	13.50	0.100000E-01
5	2915. 1234.	0.3702E-01	0.0000E+00	996.2	0.0000E+00	13.50	0.100000E-01
6	2915. 1234.	0.2828E-01	0.0000E+00	1018.	0.0000E+00	13.50	0.100000E-01
7	2915. 1234.	0.2277E-01	0.0000E+00	1036.	0.0000E+00	13.50	0.100000E-01
8	2915. 1234.	0.1941E-01	0.0000E+00	1052.	0.0000E+00	13.50	0.100000E-01
9	2915. 1234.	0.1666E-01	0.0000E+00	1067.	0.0000E+00	13.50	0.100000E-01
10	2916. 1234.	0.1438E-01	0.0000E+00	1080.	0.0000E+00	13.50	0.100000E-01
11	2916. 1234.	1.408	0.0000E+00	1082.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.79258
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.32324
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.13183
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 949.2	0.1130E-01	0.0000E+00	1389.	0.0000E+00	13.50	0.100000E-01
2	1841. 949.3	0.7110E-02	0.0000E+00	1441.	0.0000E+00	13.50	0.100000E-01
3	1841. 949.3	0.5086E-02	0.0000E+00	1487.	0.0000E+00	13.50	0.100000E-01
4	1842. 949.3	0.3452E-02	0.0000E+00	1526.	0.0000E+00	13.50	0.100000E-01
5	1842. 949.4	0.2512E-02	0.0000E+00	1556.	0.0000E+00	13.50	0.100000E-01
6	1842. 949.4	0.1918E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
7	1842. 949.5	0.1545E-02	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01
8	1842. 949.5	0.1317E-02	0.0000E+00	1622.	0.0000E+00	13.50	0.100000E-01
9	1843. 949.5	0.1130E-02	0.0000E+00	1638.	0.0000E+00	13.50	0.100000E-01
10	1843. 949.6	0.9757E-03	0.0000E+00	1654.	0.0000E+00	13.50	0.100000E-01
11	1843. 949.6	0.9549E-01	0.0000E+00	1656.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.53766E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21928E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.89430E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	0.7663E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	768.3	664.9	0.4823E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	768.6	664.9	0.3450E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	768.9	664.9	0.2341E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	769.1	665.0	0.1704E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	769.3	665.0	0.1301E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	769.4	665.1	0.1048E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	769.6	665.1	0.8932E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	769.8	665.1	0.7666E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	769.9	665.2	0.6619E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	770.0	665.2	0.6478E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
19	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
20	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
21	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
22	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
25	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
30	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
31	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
32	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
33	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
34	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
35	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
36	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
37	.	.	.	.	.	0	0	0	0	0								

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1230.0

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1394.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.66

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 440.49

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2183.9

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	113.0	0.0000E+00	419.0	0.0000E+00	0.200000E-02
2	3987.	1518.	5.895	0.0000E+00	453.4	0.0000E+00	0.200000E-02
3	3987.	1518.	4.299	0.0000E+00	484.4	0.0000E+00	0.200000E-02
4	3987.	1518.	3.093	0.0000E+00	510.1	0.0000E+00	0.200000E-02
5	3987.	1518.	2.260	0.0000E+00	531.0	0.0000E+00	0.200000E-02
6	3988.	1518.	1.742	0.0000E+00	548.3	0.0000E+00	0.200000E-02
7	3988.	1518.	1.384	0.0000E+00	563.0	0.0000E+00	0.200000E-02
8	3988.	1518.	1.184	0.0000E+00	576.0	0.0000E+00	0.200000E-02
9	3988.	1518.	1.026	0.0000E+00	587.6	0.0000E+00	0.200000E-02
10	3988.	1518.	0.9074	0.0000E+00	598.2	0.0000E+00	0.200000E-02
11	4123.	1554.	305.7	0.0000E+00	599.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 368.63
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2255.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 308.49
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2315.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 258.17
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2366.2

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
32		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
33		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
34		+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
35		+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
36		+	+	.	.	.	.	0	0	0								

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1234.	66.23	0.0000E+00	853.9	0.0000E+00	0.200000E-02
2	2914.	1234.	3.455	0.0000E+00	898.1	0.0000E+00	0.200000E-02
3	2914.	1234.	2.520	0.0000E+00	937.5	0.0000E+00	0.200000E-02
4	2914.	1234.	1.813	0.0000E+00	970.0	0.0000E+00	0.200000E-02
5	2915.	1234.	1.325	0.0000E+00	996.2	0.0000E+00	0.200000E-02
6	2915.	1234.	1.021	0.0000E+00	1018.	0.0000E+00	0.200000E-02
7	2915.	1234.	0.8114	0.0000E+00	1036.	0.0000E+00	0.200000E-02
8	2915.	1234.	0.6937	0.0000E+00	1052.	0.0000E+00	0.200000E-02
9	2915.	1234.	0.6011	0.0000E+00	1067.	0.0000E+00	0.200000E-02
10	2916.	1234.	0.5318	0.0000E+00	1080.	0.0000E+00	0.200000E-02
11	3050.	1270.	179.2	0.0000E+00	1082.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 216.05
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2408.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.81
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2443.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 151.31
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2472.7

[illegible]

[illegible]

[illegible]

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
---	----	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----

[illegible]

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
8	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
9	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
10	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
11	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
12	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
13	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
14	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
15	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
16	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
17	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0
18	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
19	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
20	+	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0
21	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0
22	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
23	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
24	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
25	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
26	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
27	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
28	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
29	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
30	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
31	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
32	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
33	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
34	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
35	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
36	+	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0
37	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
38	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
39	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
40	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
41	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
42	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0
43	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0
44	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0
45	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0
46	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0
47	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0
48	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0
49	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
50	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
51	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
52	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
53	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
54	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
55	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
56	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
57	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
58	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
59	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
60	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	949.2	38.81	0.0000E+00	1389.	0.0000E+00	13.50	0.200000E-02
2	1841.	949.3	2.025	0.0000E+00	1441.	0.0000E+00	13.50	0.200000E-02
3	1841.	949.3	1.477	0.0000E+00	1487.	0.0000E+00	13.50	0.200000E-02
4	1842.	949.3	1.063	0.0000E+00	1526.	0.0000E+00	13.50	0.200000E-02
5	1842.	949.4	0.7763	0.0000E+00	1556.	0.0000E+00	13.50	0.200000E-02
6	1842.	949.4	0.5984	0.0000E+00	1582.	0.0000E+00	13.50	0.200000E-02
7	1842.	949.5	0.4755	0.0000E+00	1603.	0.0000E+00	13.50	0.200000E-02
8	1842.	949.5	0.4066	0.0000E+00	1622.	0.0000E+00	13.50	0.200000E-02
9	1843.	949.5	0.3523	0.0000E+00	1638.	0.0000E+00	13.50	0.200000E-02
10	1843.	949.6	0.3117	0.0000E+00	1654.	0.0000E+00	13.50	0.200000E-02
11	1977.	985.3	105.0	0.0000E+00	1656.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.63
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2496.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.97
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2516.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.681
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2533.2

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

0 = .LT. .000001)

0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	22.75	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	768.3	664.9	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	768.6	664.9	0.8655	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	768.9	664.9	0.6228	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	769.1	665.0	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	769.3	665.0	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	769.4	665.1	0.2787	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	769.6	665.1	0.2383	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	769.8	665.1	0.2065	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	769.9	665.2	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	904.7	700.9	61.55	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

0 = .LT. .000001)

0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

59	0000	0	0	0	0	0	0	.	.	.	.	+	+	+	+	.02	.10	.36	1.0	2.2	3.6	4.1	3.1	1.7	.67	.19	.03	+	+	.
----	------	---	---	---	---	---	---	---	---	---	---	---	---	---	---	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	---	---	---

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
36	.	.	.	.	0	0	0											

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.157E+02	3975.	1500.
2.00	0.0	0.308E+00	2925.	1200.
3.00	0.0	0.871E-02	1875.	975.
4.00	0.0	0.300E-03	750.	675.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.231E+03	4050.	1500.
2.00	0.0	0.420E+02	3000.	1275.
3.00	0.0	0.103E+02	1950.	975.
4.00	0.0	0.305E+01	825.	675.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)  L(FT)    W(FT)    AREA(SQ FT)  L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1800. FT (ZBARGE) OR ABOUT GRID POINT #25 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1800.	1) = 1 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1800.	1) = 2 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1800.	1) = 3 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1800.	1) = 4 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1800.	1) = 5 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1800.	1) = 6 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1800.	1) = 7 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1800.	1) = 8 201.4	11.31	0.1341	8.585	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1800.	1) = 9 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1800.	1) = 10 214.3	11.55	0.9280E-01	6.299	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1800.	1) = 11 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1800.	2) = 1 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1800.	2) = 2 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1800.	2) = 3 144.6	9.538	0.6070	13.15	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1800.	2) = 4 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1800.	2) = 5 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1800.	2) = 6 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1800.	2) = 7 193.7	11.14	0.1709	4.998	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1800.	2) = 8 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1800.	2) = 9 208.2	11.44	0.1096	3.435	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1800.	2) = 10 214.3	11.55	0.9280E-01	2.987	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1800.	2) = 11 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1800.	3) = 114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1800.	3) = 128.4	8.827	0.7117	5.740	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1800.	3) = 144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1800.	3) = 160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1800.	3) = 173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1800.	3) = 184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1800.	3) = 193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1800.	3) = 201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1800.	3) = 208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1800.	3) = 214.3	11.55	0.9280E-01	1.259	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1800.	3) = 214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1800.	4) = 1 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1800.	4) = 2 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1800.	4) = 3 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1800.	4) = 4 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1800.	4) = 5 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1800.	4) = 6 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1800.	4) = 7 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1800.	4) = 8 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1800.	4) = 9 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1800.	4) = 10 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1800.	4) = 11 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051.	1800.	5) = 1 214.5	10.08	3.420	0.00000E+00	0.00000E+00	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 135.08

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4897.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 54.478

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4978.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.218

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5010.6

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	1.309	0.0000E+00	420.7	0.0000E+00	0.100000E-01
2	3987.	1518.	0.9176	0.0000E+00	443.1	0.0000E+00	0.100000E-01
3	3987.	1518.	0.8689	0.0000E+00	468.8	0.0000E+00	0.100000E-01
4	3987.	1518.	0.6691	0.0000E+00	492.8	0.0000E+00	0.100000E-01
5	3988.	1518.	0.5054	0.0000E+00	512.9	0.0000E+00	0.100000E-01
6	3988.	1518.	0.3819	0.0000E+00	529.3	0.0000E+00	0.100000E-01
7	3988.	1518.	0.2986	0.0000E+00	542.7	0.0000E+00	0.100000E-01
8	3988.	1518.	0.2463	0.0000E+00	554.0	0.0000E+00	0.100000E-01
9	3988.	1518.	0.2053	0.0000E+00	563.8	0.0000E+00	0.100000E-01
10	3989.	1518.	0.1713	0.0000E+00	572.5	0.0000E+00	0.100000E-01
11	3989.	1518.	16.64	0.0000E+00	572.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.0614
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5023.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.6956
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5072
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1234.	0.8882E-01	0.0000E+00	856.1	0.0000E+00	13.50	0.100000E-01
2	2914.	1234.	0.6225E-01	0.0000E+00	884.9	0.0000E+00	13.50	0.100000E-01
3	2914.	1234.	0.5894E-01	0.0000E+00	917.7	0.0000E+00	13.50	0.100000E-01
4	2915.	1234.	0.4539E-01	0.0000E+00	948.2	0.0000E+00	13.50	0.100000E-01
5	2915.	1234.	0.3428E-01	0.0000E+00	973.5	0.0000E+00	13.50	0.100000E-01
6	2915.	1234.	0.2590E-01	0.0000E+00	994.1	0.0000E+00	13.50	0.100000E-01
7	2915.	1234.	0.2026E-01	0.0000E+00	1011.	0.0000E+00	13.50	0.100000E-01
8	2915.	1234.	0.1670E-01	0.0000E+00	1025.	0.0000E+00	13.50	0.100000E-01
9	2916.	1234.	0.1393E-01	0.0000E+00	1037.	0.0000E+00	13.50	0.100000E-01
10	2916.	1234.	0.1162E-01	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01
11	2916.	1234.	1.129	0.0000E+00	1048.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.61469
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25070
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10224
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	949.2	0.6026E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	1841.	949.3	0.4223E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	1841.	949.3	0.3998E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	1842.	949.3	0.3079E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	1842.	949.4	0.2326E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	1842.	949.4	0.1757E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	1842.	949.4	0.1374E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	1843.	949.5	0.1133E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	1843.	949.5	0.9449E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	1843.	949.6	0.7881E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	1843.	949.6	0.7659E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.41699E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17006E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.69358E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	0.4088E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	768.3	664.9	0.2864E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	768.7	664.9	0.2712E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	769.0	664.9	0.2089E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	769.2	665.0	0.1578E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	769.5	665.0	0.1192E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	769.6	665.0	0.9322E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	769.8	665.1	0.7687E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	770.0	665.1	0.6410E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	770.1	665.2	0.5346E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	770.1	665.2	0.5196E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 934.32

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1187.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1693.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 347.78

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1774.4

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	97.02	0.0000E+00	420.7	0.0000E+00	0.200000E-02
2	3987.	1518.	3.413	0.0000E+00	443.1	0.0000E+00	0.200000E-02
3	3987.	1518.	3.269	0.0000E+00	468.8	0.0000E+00	0.200000E-02
4	3987.	1518.	2.684	0.0000E+00	492.8	0.0000E+00	0.200000E-02
5	3988.	1518.	2.040	0.0000E+00	512.9	0.0000E+00	0.200000E-02
6	3988.	1518.	1.557	0.0000E+00	529.3	0.0000E+00	0.200000E-02
7	3988.	1518.	1.221	0.0000E+00	542.7	0.0000E+00	0.200000E-02
8	3988.	1518.	0.9941	0.0000E+00	554.0	0.0000E+00	0.200000E-02
9	3988.	1518.	0.8378	0.0000E+00	563.8	0.0000E+00	0.200000E-02
10	3989.	1518.	0.7256	0.0000E+00	572.5	0.0000E+00	0.200000E-02
11	4069.	1540.	234.0	0.0000E+00	572.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 291.04
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1831.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 243.56
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1878.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 203.83
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1918.4

[illegible]

[illegible]

[illegible]

0 = .LT. .000001)

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
35	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
36	+	.	.	.														

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1234.	56.86	0.0000E+00	856.1	0.0000E+00	0.200000E-02
2	2914.	1234.	2.000	0.0000E+00	884.9	0.0000E+00	0.200000E-02
3	2914.	1234.	1.916	0.0000E+00	917.7	0.0000E+00	0.200000E-02
4	2915.	1234.	1.573	0.0000E+00	948.2	0.0000E+00	0.200000E-02
5	2915.	1234.	1.196	0.0000E+00	973.5	0.0000E+00	0.200000E-02
6	2915.	1234.	0.9125	0.0000E+00	994.1	0.0000E+00	0.200000E-02
7	2915.	1234.	0.7159	0.0000E+00	1011.	0.0000E+00	0.200000E-02
8	2915.	1234.	0.5826	0.0000E+00	1025.	0.0000E+00	0.200000E-02
9	2916.	1234.	0.4910	0.0000E+00	1037.	0.0000E+00	0.200000E-02
10	2916.	1234.	0.4253	0.0000E+00	1048.	0.0000E+00	0.200000E-02
11	2997.	1255.	137.2	0.0000E+00	1048.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 170.58
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1951.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 142.75
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1979.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 119.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2002.4

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
10		.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0000
11		.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0000
12		.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0000
13		.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0000
14		+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0000
15		+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0000
16		+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0000
17		+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0000
18		+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0000
19		+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0000
20		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0000
21		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000
22		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000
23		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
24		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
25		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
26		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
27		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
28		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
29		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
30		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
31		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
32		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
33		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
34		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
35		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0000
36		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000
37		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000
38		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000
39		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0000

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 949.2	33.33	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	1841. 949.3	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	1841. 949.3	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	1842. 949.3	0.9219	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	1842. 949.4	0.7007	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	1842. 949.4	0.5348	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	1842. 949.4	0.4196	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	1843. 949.5	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	1843. 949.5	0.2878	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	1843. 949.6	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	1924. 971.0	80.38	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 99.974
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2021.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 83.664
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2037.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 70.016
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2050.1

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	19.53	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	768.3	664.9	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	768.7	664.9	0.6581	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	769.0	664.9	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	769.2	665.0	0.4107	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	769.5	665.0	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	769.6	665.0	0.2459	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	769.8	665.1	0.2001	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	770.0	665.1	0.1687	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	770.1	665.2	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	850.9	686.6	47.11	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

0 = .LT. .0000001)

[illegible]

[illegible]

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
12	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
13	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
14	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
15	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
20	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
22	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
26	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
27	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
28	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
29	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
30	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
31	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
32	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
33	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
34	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
35	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
36	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
37	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
38	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
39	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
40	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
41	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
42	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
43	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	0000	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	0000	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	0000	0	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	0000	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	0000	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	0000	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	0000	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	0000	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	0000	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	0000	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
56	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
57	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	.01	.01	+	+	+	+	.	.	.	.
58	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	.01	.02	.02	.01	+	+	+	+	.	.
59	0000	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	.02	.03	.04	.02	.01	+	+	+	.	.

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

3	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
4	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
5	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
6	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
7	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
8	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
9	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
10	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
11	0000	+	+	+	+	+	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+
12	0000	+	+	+	+	+.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	+	+
13	0000	+	+	+	+.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+	+
14	0000	+	+	+.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+
15	0000	+	+	+.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+	+
16	0000	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+
17	0000	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+	+
18	0000	+	+	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+	+	+
19	0000	+	+	.01	.01	.01	.01	.01	.01	.02	.02	.02	.02	.01	.01	.01	.01	.01	+	+	+	+	+	+	+	+
20	0000	+	+	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	.01	+	+	+	+	+	+
21	0000	+	+	.01	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	.01	.01	+	+	+	+	+
22	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+	+	+
23	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+	+	+	+
24	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.02	.02	.02	.02	.02	.01	.01	.01	.01	+	+	+	+	+
25	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.02	.02	.03	.03	.02	.02	.02	.02	.01	.01	.01	+	+	+	+	+
26	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	+	+
27	0000	+	+	.01	.01	.01	.01	.02	.02	.02	.03	.03	.03	.03	.03	.03	.02	.02	.02	.01	.01	.01	+	+	+	+

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.127E+02	3975.	1500.
2.00	0.0	0.247E+00	2925.	1200.
3.00	0.0	0.694E-02	1875.	975.
4.00	0.0	0.238E-03	750.	675.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.206E+03	4050.	1500.
2.00	0.0	0.353E+02	2925.	1275.
3.00	0.0	0.851E+01	1875.	975.
4.00	0.0	0.249E+01	825.	675.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)    L(FT)    W(FT)    AREA(SQ FT)    L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1800. FT (ZBARGE) OR ABOUT GRID POINT #25 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050. 1800.	1) = 1 109.2	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050. 1800.	1) = 2 130.9	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050. 1800.	1) = 3 152.5	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050. 1800.	1) = 4 171.5	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051. 1800.	1) = 5 187.3	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051. 1800.	1) = 6 200.5	10.89	0.2393	53.71	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051. 1800.	1) = 7 211.8	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051. 1800.	1) = 8 221.7	11.31	0.1469	35.75	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051. 1800.	1) = 9 230.7	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051. 1800.	1) = 10 238.9	11.58	0.1054	27.20	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051. 1800.	1) = 11 239.2	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050.	1800.	2) = 1 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050.	1800.	2) = 2 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050.	1800.	2) = 3 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050.	1800.	2) = 4 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051.	1800.	2) = 5 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051.	1800.	2) = 6 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051.	1800.	2) = 7 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051.	1800.	2) = 8 221.7	11.31	0.1469	0.4821	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051.	1800.	2) = 9 230.7	11.46	0.1227	0.4154	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051.	1800.	2) = 10 238.9	11.58	0.1054	0.3666	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051.	1800.	2) = 11 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050. 1800.	3) = 109.2	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050. 1800.	3) = 130.9	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050. 1800.	3) = 152.5	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050. 1800.	3) = 171.5	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051. 1800.	3) = 187.3	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051. 1800.	3) = 200.5	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051. 1800.	3) = 211.8	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051. 1800.	3) = 221.7	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051. 1800.	3) = 230.7	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051. 1800.	3) = 238.9	11.58	0.1054	0.1515	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051. 1800.	3) = 239.2	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051.	1800.	4) = 1 239.2	9.685	3.815	0.0000E+00	0.0000E+00	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 100.53

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 488.07

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 40.998

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 547.60

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 16.721

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 571.88

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	1.598	0.0000E+00	411.8	0.0000E+00	0.100000E-01
2	3987.	1518.	0.1670	0.0000E+00	447.2	0.0000E+00	0.100000E-01
3	3987.	1518.	0.1244	0.0000E+00	481.0	0.0000E+00	0.100000E-01
4	3987.	1518.	0.8472E-01	0.0000E+00	509.8	0.0000E+00	0.100000E-01
5	3988.	1518.	0.6078E-01	0.0000E+00	533.4	0.0000E+00	0.100000E-01
6	3988.	1518.	0.4554E-01	0.0000E+00	552.7	0.0000E+00	0.100000E-01
7	3988.	1518.	0.3588E-01	0.0000E+00	569.0	0.0000E+00	0.100000E-01
8	3988.	1518.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	0.100000E-01
9	3988.	1518.	0.2517E-01	0.0000E+00	596.0	0.0000E+00	0.100000E-01
10	3988.	1518.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	0.100000E-01
11	3988.	1518.	14.53	0.0000E+00	607.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.8193
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 581.78

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.7812
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.82

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.1343
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.46
MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1234.	0.1084	0.0000E+00	844.6	0.0000E+00	13.50	0.100000E-01
2	2914.	1234.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	13.50	0.100000E-01
3	2914.	1234.	0.8437E-02	0.0000E+00	933.3	0.0000E+00	13.50	0.100000E-01
4	2915.	1234.	0.5747E-02	0.0000E+00	969.7	0.0000E+00	13.50	0.100000E-01
5	2915.	1234.	0.4123E-02	0.0000E+00	999.2	0.0000E+00	13.50	0.100000E-01
6	2915.	1234.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	13.50	0.100000E-01
7	2915.	1234.	0.2434E-02	0.0000E+00	1044.	0.0000E+00	13.50	0.100000E-01
8	2915.	1234.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	13.50	0.100000E-01
9	2915.	1234.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	13.50	0.100000E-01
10	2916.	1234.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	13.50	0.100000E-01
11	2916.	1234.	0.9855	0.0000E+00	1092.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.46260
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.13

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18866
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.41

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76945E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.52
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
21		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
22		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
23		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
24		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
25		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
26		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
27		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
28		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
29		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
30		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
31		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
32		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
33		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
34		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
35		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
36		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
37		.	.	.	.	.	0	0	0	0	0							

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	949.2	0.7355E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	1841.	949.3	0.7685E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	1841.	949.3	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	1842.	949.3	0.3899E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	1842.	949.4	0.2797E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	1842.	949.4	0.2096E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	1842.	949.5	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	1842.	949.5	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	1843.	949.6	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	1843.	949.6	0.1003E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	1843.	949.6	0.6685E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31381E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.56

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12798E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.52197E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.59

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	0.4989E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	768.3	664.9	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	768.7	664.9	0.3883E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	768.9	664.9	0.2645E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	769.1	665.0	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	769.3	665.0	0.1422E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	769.5	665.1	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	769.7	665.1	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	769.8	665.2	0.7856E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	770.0	665.2	0.6807E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	770.0	665.2	0.4535E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5	.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
15	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
16	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
17	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
18	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
19	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
20	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
21	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
22	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
23	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
24	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
25	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
26	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
27	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
28	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
30	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
31	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
32	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
33	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0000
34	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
36	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0000
37	.	.	.</															

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36		.	.	0	0	0	0											

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.81

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.185

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.133

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 137.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 105.87

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1518.	13.39	0.0000E+00	411.8	0.0000E+00	13.50
2	3987.	1518.	0.5799	0.0000E+00	447.2	0.0000E+00	13.50
3	3987.	1518.	0.4376	0.0000E+00	481.0	0.0000E+00	13.50
4	3987.	1518.	0.3164	0.0000E+00	509.8	0.0000E+00	13.50
5	3988.	1518.	0.2289	0.0000E+00	533.4	0.0000E+00	13.50
6	3988.	1518.	0.1739	0.0000E+00	552.7	0.0000E+00	13.50
7	3988.	1518.	0.1386	0.0000E+00	569.0	0.0000E+00	13.50
8	3988.	1518.	0.1154	0.0000E+00	583.3	0.0000E+00	13.50
9	3988.	1518.	0.9921E-01	0.0000E+00	596.0	0.0000E+00	13.50
10	3988.	1518.	0.8741E-01	0.0000E+00	607.5	0.0000E+00	13.50
11	3988.	1518.	121.6	0.0000E+00	607.9	0.0000E+00	13.50

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.76
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.24

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 96.040
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 146.96

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.373
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.63

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1234.	7.846	0.0000E+00	844.6	0.0000E+00	0.200000E-02
2	2914.	1234.	0.3399	0.0000E+00	890.2	0.0000E+00	0.200000E-02
3	2914.	1234.	0.2565	0.0000E+00	933.3	0.0000E+00	0.200000E-02
4	2915.	1234.	0.1854	0.0000E+00	969.7	0.0000E+00	0.200000E-02
5	2915.	1234.	0.1342	0.0000E+00	999.2	0.0000E+00	0.200000E-02
6	2915.	1234.	0.1019	0.0000E+00	1023.	0.0000E+00	0.200000E-02
7	2915.	1234.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	0.200000E-02
8	2915.	1234.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	0.200000E-02
9	2915.	1234.	0.5815E-01	0.0000E+00	1077.	0.0000E+00	0.200000E-02
10	2916.	1234.	0.5123E-01	0.0000E+00	1091.	0.0000E+00	0.200000E-02
11	2916.	1234.	71.25	0.0000E+00	1092.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.261
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.73

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.288
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.65

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 47.106
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 195.73

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

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M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
8		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
9		.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
10		.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
11		.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
12		.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
13		.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
14		.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
15		+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
16		+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
17		+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
18		+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0
19		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
20		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
21		+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0
22		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
23		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
25		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
26		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
27		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
28		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
29		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
30		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
31		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
32		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
33		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
34		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
35		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
36		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
37		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
38		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
39		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
40		+	+	+	.	.	.	.	.	0	0	0	0	0				

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 949.2	4.599	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	1841. 949.3	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	1841. 949.3	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	1842. 949.3	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	1842. 949.4	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	1842. 949.4	0.5974E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	1842. 949.5	0.4762E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	1842. 949.5	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	1843. 949.6	0.3408E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	1843. 949.6	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	1843. 949.6	41.76	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.421
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.25

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.990
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.43

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.608
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 214.47

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[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	2.695	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	768.3	664.9	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	768.7	664.9	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	768.9	664.9	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	769.1	665.0	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	769.3	665.0	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	769.5	665.1	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	769.7	665.1	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	769.8	665.2	0.1997E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	770.0	665.2	0.1760E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	770.0	665.2	24.47	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
4	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
5	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
6	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
7	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
8	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
9	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
10	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
11	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
12	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
13	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
14	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
15	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
16	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
17	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
18	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
19	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
20	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
21	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
22	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
23	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
24	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
25	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
26	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
27	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.00000
28	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.00000
29	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.00000
30	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	.	.00000
31	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	.	.00000
32	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	.	.00000
33	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	.	.00000
34	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	.	.00000
35	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	.	.00000
36	+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	.	.00000
37	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	.	.00000
38	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	.	.00000
39	+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	.	.00000
40	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	.	.00000
41	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	.	.00000
42	+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	.	.00000
43	+	+	+	.	.	.	.	0	0	0	0	0	0	0	0	.	.00000
44	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	.	.00000
45	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	.	.00000
46	+	+	.	.	.	.	0	0	0	0	0	0	0	0	0	.	.00000
47	+	+	.	.	.	0	0	0	0	0	0	0	0	0	0	.	.00000
48	+	.	.	.	.	0	0	0	0	0	0	0	0	0	0	.	.00000
49	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	.	.00000
50	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	.	.00000
51	+	.	.	.	0	0	0	0	0	0	0	0	0	0	0	.	.00000
52	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
53	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
54	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
55	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
56	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
57	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
58	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
59	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000
60	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	.	.00000

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.858E+01	3975.	1500.
2.00	0.0	0.172E+00	2925.	1200.
3.00	0.0	0.492E-02	1875.	975.
4.00	0.0	0.170E-03	750.	675.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.699E+02	3975.	1500.
2.00	0.0	0.121E+02	2925.	1200.
3.00	0.0	0.300E+01	1875.	975.
4.00	0.0	0.899E+00	750.	675.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)    L(FT)    W(FT)    AREA(SQ FT)    L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1800. FT (ZBARGE) OR ABOUT GRID POINT #25 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 71.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23333333E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 240.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1800.	1) = 123.3	9.265	0.7970E-01	139.1	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050. 1800.	1) = 137.3	9.344	0.5833	2.434	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050. 1800.	1) = 151.7	9.928	0.4689	2.182	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051. 1800.	1) = 164.4	10.40	0.3420	1.740	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051. 1800.	1) = 175.1	10.74	0.2464	1.341	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051. 1800.	1) = 183.9	10.98	0.1826	1.047	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051. 1800.	1) = 191.3	11.17	0.1410	0.8418	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051. 1800.	1) = 197.6	11.31	0.1135	0.7001	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051. 1800.	1) = 203.3	11.42	0.9478E-01	0.6011	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051. 1800.	1) = 208.2	10.18	3.317	849.0	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1800.	2) = 1 123.3	9.265	0.7970E-01	1127.	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050.	1800.	2) = 2 137.3	9.344	0.5833	19.72	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050.	1800.	2) = 3 151.7	9.928	0.4689	17.68	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051.	1800.	2) = 4 164.4	10.40	0.3420	14.10	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051.	1800.	2) = 5 175.1	10.74	0.2464	10.87	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051.	1800.	2) = 6 183.9	10.98	0.1826	8.482	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051.	1800.	2) = 7 191.3	11.17	0.1410	6.821	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051.	1800.	2) = 8 197.6	11.31	0.1135	5.672	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051.	1800.	2) = 9 203.3	11.42	0.9478E-01	4.870	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051.	1800.	2) = 10 208.2	10.18	3.317	6880.	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1800.	3) = 123.3	9.265	0.7970E-01	443.5	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050.	1800.	3) = 137.3	9.344	0.5833	7.763	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050.	1800.	3) = 151.7	9.928	0.4689	6.958	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051.	1800.	3) = 164.4	10.40	0.3420	5.549	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051.	1800.	3) = 175.1	10.74	0.2464	4.278	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051.	1800.	3) = 183.9	10.98	0.1826	3.338	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051.	1800.	3) = 191.3	11.17	0.1410	2.685	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051.	1800.	3) = 197.6	11.31	0.1135	2.233	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051.	1800.	3) = 203.3	11.42	0.9478E-01	1.916	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051.	1800.	3) = 208.2	10.18	3.317	2708.	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1800.	4) = 1 123.3	13.50	0.1000E-02	4039.	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050. 1800.	4) = 2 137.3	13.50	0.1000E-02	3156.	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050. 1800.	4) = 3 151.7	13.50	0.1000E-02	2115.	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051. 1800.	4) = 4 164.4	13.50	0.1000E-02	1322.	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051. 1800.	4) = 5 175.1	13.50	0.1000E-02	773.2	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051. 1800.	4) = 6 183.9	13.50	0.1000E-02	427.8	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051. 1800.	4) = 7 191.3	13.50	0.1000E-02	226.5	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051. 1800.	4) = 8 197.6	13.50	0.1000E-02	115.7	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051. 1800.	4) = 9 203.3	13.50	0.1000E-02	57.42	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051. 1800.	4) = 10 208.2	10.18	3.317	52.06	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051.	1800.	5) = 1 208.2	10.18	3.317	0.0000E+00	0.0000E+00	240	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 145.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7948.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.645

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8036.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.510

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8071.1

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	3986.	1518.	1.702	0.0000E+00	435.0	0.0000E+00	13.50	0.100000E-01
2	3987.	1518.	1.265	0.0000E+00	457.3	0.0000E+00	13.50	0.100000E-01
3	3987.	1518.	1.066	0.0000E+00	479.7	0.0000E+00	13.50	0.100000E-01
4	3987.	1518.	0.8389	0.0000E+00	499.2	0.0000E+00	13.50	0.100000E-01
5	3988.	1518.	0.6411	0.0000E+00	515.2	0.0000E+00	13.50	0.100000E-01
6	3988.	1518.	0.5005	0.0000E+00	528.3	0.0000E+00	13.50	0.100000E-01
7	3988.	1518.	0.4009	0.0000E+00	539.1	0.0000E+00	13.50	0.100000E-01
8	3988.	1518.	0.3391	0.0000E+00	548.4	0.0000E+00	13.50	0.100000E-01
9	3989.	1518.	0.2881	0.0000E+00	556.6	0.0000E+00	13.50	0.100000E-01
10	3989.	1518.	16.47	0.0000E+00	563.6	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.5882
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9104
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5948
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.0

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913. 1234.	0.1155	0.0000E+00	874.5	0.0000E+00	13.50	0.100000E-01
2	2914. 1234.	0.8585E-01	0.0000E+00	903.1	0.0000E+00	13.50	0.100000E-01
3	2914. 1234.	0.7230E-01	0.0000E+00	931.6	0.0000E+00	13.50	0.100000E-01
4	2915. 1234.	0.5691E-01	0.0000E+00	956.3	0.0000E+00	13.50	0.100000E-01
5	2915. 1234.	0.4349E-01	0.0000E+00	976.5	0.0000E+00	13.50	0.100000E-01
6	2915. 1234.	0.3395E-01	0.0000E+00	992.9	0.0000E+00	13.50	0.100000E-01
7	2915. 1234.	0.2719E-01	0.0000E+00	1006.	0.0000E+00	13.50	0.100000E-01
8	2916. 1234.	0.2301E-01	0.0000E+00	1018.	0.0000E+00	13.50	0.100000E-01
9	2916. 1234.	0.1954E-01	0.0000E+00	1028.	0.0000E+00	13.50	0.100000E-01
10	2916. 1234.	1.117	0.0000E+00	1037.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65043
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26527
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10819
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	949.2	0.7833E-02	0.0000E+00	1413.	0.0000E+00	13.50	0.100000E-01
2	1841.	949.3	0.5823E-02	0.0000E+00	1447.	0.0000E+00	13.50	0.100000E-01
3	1842.	949.3	0.4905E-02	0.0000E+00	1481.	0.0000E+00	13.50	0.100000E-01
4	1842.	949.3	0.3860E-02	0.0000E+00	1510.	0.0000E+00	13.50	0.100000E-01
5	1842.	949.3	0.2950E-02	0.0000E+00	1533.	0.0000E+00	13.50	0.100000E-01
6	1842.	949.4	0.2303E-02	0.0000E+00	1552.	0.0000E+00	13.50	0.100000E-01
7	1843.	949.4	0.1845E-02	0.0000E+00	1568.	0.0000E+00	13.50	0.100000E-01
8	1843.	949.5	0.1561E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
9	1843.	949.5	0.1326E-02	0.0000E+00	1594.	0.0000E+00	13.50	0.100000E-01
10	1843.	949.5	0.7578E-01	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44123E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17995E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73390E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	664.8	0.5314E-03	0.0000E+00	2036.	0.0000E+00	13.50	0.100000E-01
2	768.3	664.9	0.3950E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	768.7	664.9	0.3327E-03	0.0000E+00	2112.	0.0000E+00	13.50	0.100000E-01
4	769.1	664.9	0.2619E-03	0.0000E+00	2145.	0.0000E+00	13.50	0.100000E-01
5	769.4	664.9	0.2001E-03	0.0000E+00	2172.	0.0000E+00	13.50	0.100000E-01
6	769.6	665.0	0.1562E-03	0.0000E+00	2193.	0.0000E+00	13.50	0.100000E-01
7	769.8	665.0	0.1251E-03	0.0000E+00	2211.	0.0000E+00	13.50	0.100000E-01
8	770.1	665.1	0.1059E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
9	770.2	665.1	0.8992E-04	0.0000E+00	2240.	0.0000E+00	13.50	0.100000E-01
10	770.4	665.1	0.5141E-02	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1356.0

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1830.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 571.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2614.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 434.54

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2751.5

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4026.	1529.	115.5	0.0000E+00	435.0	0.0000E+00	0.200000E-02
2	3987.	1518.	4.571	0.0000E+00	457.3	0.0000E+00	0.200000E-02
3	3987.	1518.	4.091	0.0000E+00	479.7	0.0000E+00	0.200000E-02
4	3987.	1518.	3.257	0.0000E+00	499.2	0.0000E+00	0.200000E-02
5	3988.	1518.	2.484	0.0000E+00	515.2	0.0000E+00	0.200000E-02
6	3988.	1518.	1.935	0.0000E+00	528.3	0.0000E+00	0.200000E-02
7	3988.	1518.	1.535	0.0000E+00	539.1	0.0000E+00	0.200000E-02
8	3988.	1518.	1.292	0.0000E+00	548.4	0.0000E+00	0.200000E-02
9	3989.	1518.	1.107	0.0000E+00	556.6	0.0000E+00	0.200000E-02
10	4115.	1552.	298.7	0.0000E+00	563.6	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 363.65
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2822.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.33
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2881.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 254.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2931.3

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2953. 1244.	67.71	0.0000E+00	874.5	0.0000E+00	13.50	0.200000E-02
2	2914. 1234.	2.679	0.0000E+00	903.1	0.0000E+00	13.50	0.200000E-02
3	2914. 1234.	2.398	0.0000E+00	931.6	0.0000E+00	13.50	0.200000E-02
4	2915. 1234.	1.909	0.0000E+00	956.3	0.0000E+00	13.50	0.200000E-02
5	2915. 1234.	1.456	0.0000E+00	976.5	0.0000E+00	13.50	0.200000E-02
6	2915. 1234.	1.134	0.0000E+00	992.9	0.0000E+00	13.50	0.200000E-02
7	2915. 1234.	0.8999	0.0000E+00	1006.	0.0000E+00	13.50	0.200000E-02
8	2916. 1234.	0.7573	0.0000E+00	1018.	0.0000E+00	13.50	0.200000E-02
9	2916. 1234.	0.6490	0.0000E+00	1028.	0.0000E+00	13.50	0.200000E-02
10	3042. 1267.	175.1	0.0000E+00	1037.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2972.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3007.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3036.4

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1880.	959.7	39.68	0.0000E+00	1413.	0.0000E+00	13.50
2	1841.	949.3	1.570	0.0000E+00	1447.	0.0000E+00	13.50
3	1842.	949.3	1.405	0.0000E+00	1481.	0.0000E+00	13.50
4	1842.	949.3	1.119	0.0000E+00	1510.	0.0000E+00	13.50
5	1842.	949.3	0.8532	0.0000E+00	1533.	0.0000E+00	13.50
6	1842.	949.4	0.6647	0.0000E+00	1552.	0.0000E+00	13.50
7	1843.	949.4	0.5274	0.0000E+00	1568.	0.0000E+00	13.50
8	1843.	949.5	0.4438	0.0000E+00	1582.	0.0000E+00	13.50
9	1843.	949.5	0.3804	0.0000E+00	1594.	0.0000E+00	13.50
10	1970.	983.0	102.6	0.0000E+00	1604.	0.0000E+00	13.50

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 124.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3060.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.54
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3080.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.483
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3096.1

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
3	0000	1.0	1.1	1.3	1.3	1.4	1.5	1.5	1.5	1.5	1.5	1.4	1.4	1.4	1.3	1.2	1.1	1.0	.89	.77	.66	.56	.46	.38	.31	.24	.19	.15	0	0	0
4	0000	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.8	1.8	1.7	1.7	1.6	1.5	1.4	1.2	1.1	1.0	.88	.76	.64	.53	.44	.35	.28	.22	.17	0	0	0	
5	0000	1.3	1.5	1.6	1.7	1.8	1.9	2.0	2.0	2.0	1.9	1.9	1.8	1.7	1.5	1.4	1.2	1.1	.99	.85	.72	.60	.49	.40	.32	.25	.19	0	0	0	
6	0000	1.5	1.7	1.8	1.9	2.1	2.1	2.2	2.2	2.2	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.95	.80	.66	.55	.44	.35	.27	.21	0	0	0	
7	0000	1.6	1.8	2.0	2.1	2.3	2.3	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.2	1.0	.87	.73	.60	.48	.38	.30	.23	0	0	0	
8	0000	1.8	2.0	2.1	2.3	2.4	2.5	2.6	2.6	2.6	2.6	2.5	2.3	2.2	2.0	1.8	1.6	1.4	1.3	1.1	.94	.78	.64	.52	.41	.32	.25	0	0	0	
9	0000	1.9	2.1	2.3	2.4	2.6	2.7	2.8	2.8	2.8	2.7	2.6	2.5	2.3	2.2	2.0	1.7	1.5	1.3	1.1	1.0	.83	.68	.55	.44	.34	.27	0	0	0	
10	0000	2.0	2.2	2.4	2.6	2.7	2.8	2.9	2.9	2.9	2.8	2.7	2.6	2.4	2.3	2.0	1.8	1.6	1.4	1.2	1.0	.87	.71	.58	.46	.36	.28	0	0	0	
11	0000	2.0	2.2	2.4	2.6	2.8	2.9	3.0	3.0	3.0	2.9	2.8	2.7	2.5	2.3	2.1	1.9	1.7	1.4	1.2	1.0	.90	.74	.60	.47	.37	.29	0	0	0	
12	0000	2.1	2.3	2.5	2.7	2.8	2.9	3.0	3.0	3.0	3.0	2.9	2.7	2.6	2.4	2.1	1.9	1.7	1.5	1.2	1.0	.91	.75	.60	.48	.38	.29	0	0	0	
13	0000	2.1	2.3	2.5	2.7	2.8	2.9	3.0	3.0	3.0	3.0	2.9	2.7	2.6	2.4	2.1	1.9	1.7	1.5	1.2	1.0	.91	.75	.61	.48	.38	.29	0	0	0	
14	0000	2.0	2.2	2.4	2.6	2.8	2.9	3.0	3.0	3.0	2.9	2.8	2.7	2.5	2.3	2.1	1.9	1.7	1.4	1.2	1.0	.90	.74	.60	.48	.37	.29	0	0	0	
15	0000	2.0	2.2	2.4	2.5	2.7	2.8	2.9	2.9	2.9	2.8	2.7	2.6	2.4	2.3	2.0	1.8	1.6	1.4	1.2	1.0	.87	.72	.58	.46	.36	.28	0	0	0	
16	0000	1.9	2.1	2.3	2.4	2.6	2.7	2.7	2.8	2.8	2.7	2.6	2.5	2.3	2.2	2.0	1.7	1.5	1.3	1.1	1.0	.84	.69	.56	.44	.35	.27	0	0	0	
17	0000	1.8	2.0	2.1	2.3	2.4	2.5	2.6	2.6	2.6	2.6	2.5	2.3	2.2	2.0	1.8	1.6	1.5	1.3	1.1	.95	.79	.65	.52	.42	.33	.25	0	0	0	
18																															

[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT.
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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	807.6	675.3	23.26	0.0000E+00	2036.	0.0000E+00	13.50	0.200000E-02
2	768.3	664.9	0.9202	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	768.7	664.9	0.8236	0.0000E+00	2112.	0.0000E+00	13.50	0.200000E-02
4	769.1	664.9	0.6558	0.0000E+00	2145.	0.0000E+00	13.50	0.200000E-02
5	769.4	664.9	0.5001	0.0000E+00	2172.	0.0000E+00	13.50	0.200000E-02
6	769.6	665.0	0.3896	0.0000E+00	2193.	0.0000E+00	13.50	0.200000E-02
7	769.8	665.0	0.3091	0.0000E+00	2211.	0.0000E+00	13.50	0.200000E-02
8	770.1	665.1	0.2601	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
9	770.2	665.1	0.2229	0.0000E+00	2240.	0.0000E+00	13.50	0.200000E-02
10	896.8	698.6	60.14	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

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[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
12	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
13	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
14	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
15	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
20	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
22	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
26	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
27	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
28	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
29	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
30	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
31	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
32	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
33	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
34	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
35	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
36	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
37	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
38	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
39	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
40	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
41	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
42	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
43	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	0000	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	0000	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	0000	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	0000	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	0000	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
54	0000	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
55	0000	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0
56	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.01	+	+	+	+	+	+	+	+	0
57	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.01	.01	.01	.01	+	+	+	+	+	0
58	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	.01	.02	.04	.04	.03	.01	+	+	+	0
59	0000	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	.01	.03	.06	.07	.04	.02	+	+	+	0

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible][illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
4	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
5	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
6	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
7	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
8	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
9	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
10	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
11	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
12	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
13	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
14	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
15	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
16	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
17	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
18	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
19	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	00000
20	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
21	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
22	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
23	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
24	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
25	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	00000
26	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
27	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
28	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
29	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
30	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
31	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
32	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
33	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
34	+	+	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
35	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	00000
36	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
37	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
38	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	00000
39	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	00000
40	+	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	00000
41	+	.	.	.	.	0												

[illegible]

TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM, 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
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22	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
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25	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
26	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
27	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
28	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
29	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
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31	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
32	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
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37	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
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47	0000	0	0	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
48	0000	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
49	0000	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
50	0000	0	0	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
51	0000	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
52	0000	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
53	0000	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
54	0000	0	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
55	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
56	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
57	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.01	.01	.	+	+	+	+	.	.	.	
58	0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.01	.02	.02	.01	.	+	+	+	.	.	
59	0000	0	0	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	.01	.03	.03	.02	.01	.	+	+	+	.	

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
36		.	0	0	0</													

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.138E+02	3975.	1500.
2.00	0.0	0.267E+00	2925.	1200.
3.00	0.0	0.746E-02	1875.	975.
4.00	0.0	0.255E-03	750.	675.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.251E+03	4050.	1575.
2.00	0.0	0.440E+02	3000.	1275.
3.00	0.0	0.106E+02	1950.	975.
4.00	0.0	0.310E+01	825.	675.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)    L(FT)    W(FT)    AREA(SQ FT)    L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1650. FT (ZBARGE) OR ABOUT GRID POINT #23 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.7640E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1340	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.6070E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2711	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.4578

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 6.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.16666667E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 1137.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #3 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.31555556E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 836.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #4 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.43914816E-02 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 701.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050.	1650.	1) = 143.3	9.063	1.013	560.3	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050.	1650.	1) = 159.3	10.08	0.4471	8.761	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050.	1650.	1) = 171.4	10.52	0.2734	5.777	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050.	1650.	1) = 181.1	10.80	0.1911	4.255	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050.	1650.	1) = 189.1	10.99	0.1448	3.355	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050.	1650.	1) = 195.8	11.13	0.1152	2.758	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050.	1650.	1) = 201.6	11.25	0.9467E-01	2.328	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050.	1650.	1) = 206.7	11.34	0.7957E-01	2.002	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050.	1650.	1) = 211.1	11.42	0.6810E-01	1.749	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050.	1650.	1) = 215.1	10.07	3.431	3534.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050. 1650.	2) = 1 143.3	9.063	1.013	982.8	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050. 1650.	2) = 2 159.3	10.08	0.4471	15.37	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050. 1650.	2) = 3 171.4	10.52	0.2734	10.13	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050. 1650.	2) = 4 181.1	10.80	0.1911	7.460	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050. 1650.	2) = 5 189.1	10.99	0.1448	5.883	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050. 1650.	2) = 6 195.8	11.13	0.1152	4.838	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050. 1650.	2) = 7 201.6	11.25	0.9467E-01	4.081	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050. 1650.	2) = 8 206.7	11.34	0.7957E-01	3.513	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050. 1650.	2) = 9 211.1	11.42	0.6810E-01	3.067	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050. 1650.	2) = 10 215.1	10.07	3.431	6199.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050.	1650.	3) = 143.3	9.063	1.013	445.2	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050.	1650.	3) = 159.3	10.08	0.4471	6.961	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050.	1650.	3) = 171.4	10.52	0.2734	4.589	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050.	1650.	3) = 181.1	10.80	0.1911	3.380	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050.	1650.	3) = 189.1	10.99	0.1448	2.665	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050.	1650.	3) = 195.8	11.13	0.1152	2.191	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050.	1650.	3) = 201.6	11.25	0.9467E-01	1.850	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050.	1650.	3) = 206.7	11.34	0.7957E-01	1.591	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050.	1650.	3) = 211.1	11.42	0.6810E-01	1.389	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050.	1650.	3) = 215.1	10.07	3.431	2808.	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.31	5050. 1650.	4) = 1 143.3	13.50	0.1000E-02	944.6	0.0000E+00	71	1
NEW CLOUD CREATED, NTCLD(K) (K = 30.61	5050. 1650.	4) = 2 159.3	13.50	0.1000E-02	3525.	0.0000E+00	141	71
NEW CLOUD CREATED, NTCLD(K) (K = 30.92	5050. 1650.	4) = 3 171.4	13.50	0.1000E-02	2797.	0.0000E+00	211	141
NEW CLOUD CREATED, NTCLD(K) (K = 31.23	5050. 1650.	4) = 4 181.1	13.50	0.1000E-02	2123.	0.0000E+00	281	211
NEW CLOUD CREATED, NTCLD(K) (K = 31.54	5050. 1650.	4) = 5 189.1	13.50	0.1000E-02	1565.	0.0000E+00	351	281
NEW CLOUD CREATED, NTCLD(K) (K = 31.84	5050. 1650.	4) = 6 195.8	13.50	0.1000E-02	1130.	0.0000E+00	421	351
NEW CLOUD CREATED, NTCLD(K) (K = 32.15	5050. 1650.	4) = 7 201.6	13.50	0.1000E-02	801.7	0.0000E+00	491	421
NEW CLOUD CREATED, NTCLD(K) (K = 32.46	5050. 1650.	4) = 8 206.7	13.50	0.1000E-02	561.0	0.0000E+00	561	491
NEW CLOUD CREATED, NTCLD(K) (K = 32.77	5050. 1650.	4) = 9 211.1	13.50	0.1000E-02	388.0	0.0000E+00	631	561
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050. 1650.	4) = 10 215.1	10.07	3.431	804.3	0.0000E+00	701	631

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 33.07	5050.	1650.	5) = 1 215.1	10.07	3.431	0.0000E+00	0.0000E+00	701	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4125.6

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 148.20

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7087.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 59.434

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7176.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 24.240

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7211.7

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	3.837	0.0000E+00	466.9	0.0000E+00	0.100000E-01
2	3986.	1368.	0.9250	0.0000E+00	491.6	0.0000E+00	0.100000E-01
3	3986.	1368.	0.6056	0.0000E+00	509.9	0.0000E+00	0.100000E-01
4	3986.	1368.	0.4176	0.0000E+00	524.4	0.0000E+00	0.100000E-01
5	3986.	1368.	0.3501	0.0000E+00	536.2	0.0000E+00	0.100000E-01
6	3987.	1368.	0.2869	0.0000E+00	546.1	0.0000E+00	0.100000E-01
7	3987.	1368.	0.2452	0.0000E+00	554.5	0.0000E+00	0.100000E-01
8	3987.	1368.	0.2103	0.0000E+00	561.8	0.0000E+00	0.100000E-01
9	3987.	1368.	0.1818	0.0000E+00	568.2	0.0000E+00	0.100000E-01
10	3987.	1368.	17.18	0.0000E+00	573.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.8858
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7226.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.0318
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7232.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.6443
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7234.3

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913. 1084.	0.2603	0.0000E+00	915.3	0.0000E+00	13.50	0.100000E-01
2	2913. 1084.	0.6275E-01	0.0000E+00	946.7	0.0000E+00	13.50	0.100000E-01
3	2913. 1084.	0.4108E-01	0.0000E+00	969.8	0.0000E+00	13.50	0.100000E-01
4	2914. 1084.	0.2833E-01	0.0000E+00	987.9	0.0000E+00	13.50	0.100000E-01
5	2914. 1084.	0.2375E-01	0.0000E+00	1003.	0.0000E+00	13.50	0.100000E-01
6	2914. 1084.	0.1946E-01	0.0000E+00	1015.	0.0000E+00	13.50	0.100000E-01
7	2914. 1084.	0.1663E-01	0.0000E+00	1026.	0.0000E+00	13.50	0.100000E-01
8	2914. 1084.	0.1426E-01	0.0000E+00	1035.	0.0000E+00	13.50	0.100000E-01
9	2914. 1084.	0.1233E-01	0.0000E+00	1043.	0.0000E+00	13.50	0.100000E-01
10	2914. 1084.	1.165	0.0000E+00	1050.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.67062
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.27350
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.11155
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1840.	799.2	0.1766E-01	0.0000E+00	1461.	0.0000E+00	13.50	0.100000E-01
2	1840.	799.2	0.4257E-02	0.0000E+00	1498.	0.0000E+00	13.50	0.100000E-01
3	1841.	799.2	0.2787E-02	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
4	1841.	799.2	0.1922E-02	0.0000E+00	1547.	0.0000E+00	13.50	0.100000E-01
5	1841.	799.3	0.1611E-02	0.0000E+00	1564.	0.0000E+00	13.50	0.100000E-01
6	1841.	799.3	0.1320E-02	0.0000E+00	1578.	0.0000E+00	13.50	0.100000E-01
7	1841.	799.3	0.1128E-02	0.0000E+00	1591.	0.0000E+00	13.50	0.100000E-01
8	1841.	799.3	0.9676E-03	0.0000E+00	1601.	0.0000E+00	13.50	0.100000E-01
9	1841.	799.4	0.8367E-03	0.0000E+00	1610.	0.0000E+00	13.50	0.100000E-01
10	1841.	799.4	0.7906E-01	0.0000E+00	1619.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.45492E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18554E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7235.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.75668E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7236.0

MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.5	514.8	0.1198E-02	0.0000E+00	2090.	0.0000E+00	13.50	0.100000E-01
2	767.7	514.8	0.2888E-03	0.0000E+00	2132.	0.0000E+00	13.50	0.100000E-01
3	767.8	514.8	0.1890E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
4	767.9	514.8	0.1304E-03	0.0000E+00	2187.	0.0000E+00	13.50	0.100000E-01
5	768.0	514.9	0.1093E-03	0.0000E+00	2206.	0.0000E+00	13.50	0.100000E-01
6	768.1	514.9	0.8957E-04	0.0000E+00	2223.	0.0000E+00	13.50	0.100000E-01
7	768.2	514.9	0.7653E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
8	768.3	514.9	0.6564E-04	0.0000E+00	2248.	0.0000E+00	13.50	0.100000E-01
9	768.4	515.0	0.5676E-04	0.0000E+00	2259.	0.0000E+00	13.50	0.100000E-01
10	768.5	515.0	0.5363E-02	0.0000E+00	2268.	0.0000E+00	13.50	0.100000E-01

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[illegible]

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[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1425.6

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1852.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 621.88

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2655.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 494.15

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2783.6

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	4002.	1372.	142.4	0.0000E+00	466.9	0.0000E+00	0.200000E-02
2	3986.	1368.	4.088	0.0000E+00	491.6	0.0000E+00	0.200000E-02
3	3986.	1368.	2.691	0.0000E+00	509.9	0.0000E+00	0.200000E-02
4	3986.	1368.	1.961	0.0000E+00	524.4	0.0000E+00	0.200000E-02
5	3986.	1368.	1.544	0.0000E+00	536.2	0.0000E+00	0.200000E-02
6	3987.	1368.	1.267	0.0000E+00	546.1	0.0000E+00	0.200000E-02
7	3987.	1368.	1.070	0.0000E+00	554.5	0.0000E+00	0.200000E-02
8	3987.	1368.	0.9200	0.0000E+00	561.8	0.0000E+00	0.200000E-02
9	3987.	1368.	0.8023	0.0000E+00	568.2	0.0000E+00	0.200000E-02
10	4109.	1400.	337.4	0.0000E+00	573.9	0.4899E-01	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 413.53
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2864.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 346.07
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2931.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 289.61
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2988.2

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[illegible]

7200.00 SECONDS AFTER DUMP

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[illegible]

[illegible]

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[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2929.	1088.	83.49	0.0000E+00	915.3	0.0000E+00	0.200000E-02
2	2913.	1084.	2.396	0.0000E+00	946.7	0.0000E+00	0.200000E-02
3	2913.	1084.	1.577	0.0000E+00	969.8	0.0000E+00	0.200000E-02
4	2914.	1084.	1.149	0.0000E+00	987.9	0.0000E+00	0.200000E-02
5	2914.	1084.	0.9050	0.0000E+00	1003.	0.0000E+00	0.200000E-02
6	2914.	1084.	0.7423	0.0000E+00	1015.	0.0000E+00	0.200000E-02
7	2914.	1084.	0.6273	0.0000E+00	1026.	0.0000E+00	0.200000E-02
8	2914.	1084.	0.5392	0.0000E+00	1035.	0.0000E+00	0.200000E-02
9	2914.	1084.	0.4702	0.0000E+00	1043.	0.0000E+00	0.200000E-02
10	3036.	1116.	197.7	0.0000E+00	1050.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 242.37
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 202.83
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3074.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 169.74
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3107.1

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1856.	803.4	48.93	0.0000E+00	1461.	0.0000E+00	13.50	0.200000E-02
2	1840.	799.2	1.404	0.0000E+00	1498.	0.0000E+00	13.50	0.200000E-02
3	1841.	799.2	0.9245	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
4	1841.	799.2	0.6735	0.0000E+00	1547.	0.0000E+00	13.50	0.200000E-02
5	1841.	799.3	0.5304	0.0000E+00	1564.	0.0000E+00	13.50	0.200000E-02
6	1841.	799.3	0.4351	0.0000E+00	1578.	0.0000E+00	13.50	0.200000E-02
7	1841.	799.3	0.3676	0.0000E+00	1591.	0.0000E+00	13.50	0.200000E-02
8	1841.	799.3	0.3160	0.0000E+00	1601.	0.0000E+00	13.50	0.200000E-02
9	1841.	799.4	0.2756	0.0000E+00	1610.	0.0000E+00	13.50	0.200000E-02
10	1963.	831.7	115.9	0.0000E+00	1619.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 142.05
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3134.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 118.88
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3156.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 99.482
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3174.2

[illegible]

[illegible]

[illegible]

1.000 (LEGEND... + = .LT. .01 . = .LT.

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

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M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
4		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
5		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
6		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
7		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
8		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
9		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
10		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
11		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
12		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
13		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
14		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
15		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
16		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
17		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
18		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
19		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
20		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
21		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
22		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
23		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
24		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
25		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
26		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
27		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
28		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
29		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	00000
30		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	00000
31		+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	00000
32		+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	00000
33		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	00000
34		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	00000
35		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	00000
36		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	00000
37		+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
38		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
39		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
40		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
41		+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
42		+	+	.	.	.	.											

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	783.4	519.0	28.68	0.0000E+00	2090.	0.0000E+00	13.50	0.200000E-02
2	767.7	514.8	0.8230	0.0000E+00	2132.	0.0000E+00	13.50	0.200000E-02
3	767.8	514.8	0.5418	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
4	767.9	514.8	0.3948	0.0000E+00	2187.	0.0000E+00	13.50	0.200000E-02
5	768.0	514.9	0.3109	0.0000E+00	2206.	0.0000E+00	13.50	0.200000E-02
6	768.1	514.9	0.2550	0.0000E+00	2223.	0.0000E+00	13.50	0.200000E-02
7	768.2	514.9	0.2155	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
8	768.3	514.9	0.1852	0.0000E+00	2248.	0.0000E+00	13.50	0.200000E-02
9	768.4	515.0	0.1615	0.0000E+00	2259.	0.0000E+00	13.50	0.200000E-02
10	890.3	547.3	67.92	0.0000E+00	2268.	0.0000E+00	13.50	0.200000E-02

1 0 = .LT. .0000001)

0 = .LT. .0000001)

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
4		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
5		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.0000
6		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
7		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
8		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
9		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
10		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
11		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
12		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
13		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
14		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
15		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
16		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
17		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
18		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
19		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
20		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
21		+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.0000
22		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
23		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.0000
24		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
25		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
26		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	00000
27		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	00000
28		+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	00000
29		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	00000
30		+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	00000
31		+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	00000
32		+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	00000
33		+	+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	00000
34		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	00000
35		+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	00000
36		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	00000
37		+	+	+	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
38		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
39		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
40		+	+	+	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
41		+	+	.	.	.	.	.	.	0	0	0	0	0	0	0	0	00000
42		+	+	.	.	.	.											

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
12	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
13	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
14	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.
15	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
20	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
22	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
26	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
27	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
28	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
29	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
30	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
31	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
32	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
33	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
34	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
35	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
36	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
37	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
38	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
39	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
40	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
41	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
42	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
43	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
44	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
45	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
46	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
47	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
48	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
49	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
50	0000	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
51	0000	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
52	0000	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
53	0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
54	0000	0	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
55	0000	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
56	0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.
57	0000	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.01	.01	.01	.01	+	+	+	+	.	.	.	.	.
58	0000	0	0	0	0	0	0	0	0	.	.	.	+	+	+	+	+	.01	.02	.03	.03	.02	.01	+	+	+	.	.	.	.
59	0000	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	.01	.03	.05	.06	.04	.02	+	+	+	.	.	.	.

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 14639.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.137E+02	3975.	1350.
2.00	0.0	0.268E+00	2925.	1050.
3.00	0.0	0.754E-02	1875.	825.
4.00	0.0	0.259E-03	750.	525.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.261E+03	4050.	1350.
2.00	0.0	0.477E+02	3000.	1125.
3.00	0.0	0.116E+02	1950.	825.
4.00	0.0	0.344E+01	825.	525.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

[illegible]

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1650. FT (ZBARGE) OR ABOUT GRID POINT #23 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.5557	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1124	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4860E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.2833

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 66.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.21666666E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 265.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1650.	1) = 113.6	7.855	0.6224	3025.	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1650.	1) = 134.8	8.477	1.036	113.3	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050. 1650.	1) = 154.7	9.513	0.6631	83.37	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050. 1650.	1) = 171.6	10.18	0.4327	60.13	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051. 1650.	1) = 185.6	10.61	0.2974	44.41	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051. 1650.	1) = 197.4	10.91	0.2177	34.31	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051. 1650.	1) = 207.6	11.12	0.1689	27.76	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051. 1650.	1) = 216.6	11.29	0.1373	23.37	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051. 1650.	1) = 224.8	11.43	0.1157	20.29	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051. 1650.	1) = 232.3	11.55	0.9998E-01	18.00	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051. 1650.	1) = 233.4	9.779	3.721	0.2656E+05	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1650.	2) = 113.6	7.855	0.6224	611.9	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050.	1650.	2) = 134.8	8.477	1.036	22.93	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050.	1650.	2) = 154.7	9.513	0.6631	16.86	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050.	1650.	2) = 171.6	10.18	0.4327	12.16	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051.	1650.	2) = 185.6	10.61	0.2974	8.983	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051.	1650.	2) = 197.4	10.91	0.2177	6.938	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051.	1650.	2) = 207.6	11.12	0.1689	5.615	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051.	1650.	2) = 216.6	11.29	0.1373	4.728	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051.	1650.	2) = 224.8	11.43	0.1157	4.103	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051.	1650.	2) = 232.3	11.55	0.9998E-01	3.642	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051.	1650.	2) = 233.4	9.779	3.721	5372.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1650.	3) = 113.6	7.855	0.6224	264.6	0.0000E+00	27	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1650.	3) = 134.8	8.477	1.036	9.912	0.0000E+00	53	27
NEW CLOUD CREATED, NTCLD(K) (K = 31.69	5050. 1650.	3) = 154.7	9.513	0.6631	7.291	0.0000E+00	79	53
NEW CLOUD CREATED, NTCLD(K) (K = 32.25	5050. 1650.	3) = 171.6	10.18	0.4327	5.258	0.0000E+00	105	79
NEW CLOUD CREATED, NTCLD(K) (K = 32.82	5051. 1650.	3) = 185.6	10.61	0.2974	3.884	0.0000E+00	131	105
NEW CLOUD CREATED, NTCLD(K) (K = 33.38	5051. 1650.	3) = 197.4	10.91	0.2177	3.000	0.0000E+00	157	131
NEW CLOUD CREATED, NTCLD(K) (K = 33.94	5051. 1650.	3) = 207.6	11.12	0.1689	2.427	0.0000E+00	183	157
NEW CLOUD CREATED, NTCLD(K) (K = 34.51	5051. 1650.	3) = 216.6	11.29	0.1373	2.044	0.0000E+00	209	183
NEW CLOUD CREATED, NTCLD(K) (K = 35.07	5051. 1650.	3) = 224.8	11.43	0.1157	1.774	0.0000E+00	235	209
NEW CLOUD CREATED, NTCLD(K) (K = 35.63	5051. 1650.	3) = 232.3	11.55	0.9998E-01	1.574	0.0000E+00	261	235
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051. 1650.	3) = 233.4	9.779	3.721	2323.	0.0000E+00	265	261

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.72	5051.	1650.	4) = 1 233.4	9.779	3.721	0.0000E+00	0.0000E+00	265	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 30008.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 173.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5895.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 70.243

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5999.4

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 28.648

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6040.9

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	2.455	0.0000E+00	419.0	0.0000E+00	0.100000E-01
2	3987.	1368.	1.545	0.0000E+00	453.4	0.0000E+00	0.100000E-01
3	3987.	1368.	1.105	0.0000E+00	484.4	0.0000E+00	0.100000E-01
4	3987.	1368.	0.7501	0.0000E+00	510.1	0.0000E+00	0.100000E-01
5	3987.	1368.	0.5458	0.0000E+00	531.0	0.0000E+00	0.100000E-01
6	3988.	1368.	0.4168	0.0000E+00	548.3	0.0000E+00	0.100000E-01
7	3988.	1368.	0.3357	0.0000E+00	563.0	0.0000E+00	0.100000E-01
8	3988.	1368.	0.2861	0.0000E+00	576.0	0.0000E+00	0.100000E-01
9	3988.	1368.	0.2456	0.0000E+00	587.6	0.0000E+00	0.100000E-01
10	3988.	1368.	0.2120	0.0000E+00	598.2	0.0000E+00	0.100000E-01
11	3988.	1368.	20.75	0.0000E+00	599.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 11.684
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6057.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 4.7651
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6064.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.9434
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6067.6

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	0.1665	0.0000E+00	853.9	0.0000E+00	0.100000E-01
2	2914.	1084.	0.1048	0.0000E+00	898.1	0.0000E+00	0.100000E-01
3	2914.	1084.	0.7498E-01	0.0000E+00	937.5	0.0000E+00	0.100000E-01
4	2914.	1084.	0.5088E-01	0.0000E+00	970.0	0.0000E+00	0.100000E-01
5	2915.	1084.	0.3702E-01	0.0000E+00	996.2	0.0000E+00	0.100000E-01
6	2915.	1084.	0.2828E-01	0.0000E+00	1018.	0.0000E+00	0.100000E-01
7	2915.	1084.	0.2277E-01	0.0000E+00	1036.	0.0000E+00	0.100000E-01
8	2915.	1084.	0.1941E-01	0.0000E+00	1052.	0.0000E+00	0.100000E-01
9	2915.	1084.	0.1666E-01	0.0000E+00	1067.	0.0000E+00	0.100000E-01
10	2916.	1084.	0.1438E-01	0.0000E+00	1080.	0.0000E+00	0.100000E-01
11	2916.	1084.	1.408	0.0000E+00	1082.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.79258
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6068.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.32324
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.13183
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.4
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 799.2	0.1130E-01	0.0000E+00	1389.	0.0000E+00	13.50	0.100000E-01
2	1841. 799.3	0.7110E-02	0.0000E+00	1441.	0.0000E+00	13.50	0.100000E-01
3	1841. 799.3	0.5086E-02	0.0000E+00	1487.	0.0000E+00	13.50	0.100000E-01
4	1842. 799.3	0.3452E-02	0.0000E+00	1526.	0.0000E+00	13.50	0.100000E-01
5	1842. 799.4	0.2512E-02	0.0000E+00	1556.	0.0000E+00	13.50	0.100000E-01
6	1842. 799.4	0.1918E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
7	1842. 799.5	0.1545E-02	0.0000E+00	1603.	0.0000E+00	13.50	0.100000E-01
8	1842. 799.5	0.1317E-02	0.0000E+00	1622.	0.0000E+00	13.50	0.100000E-01
9	1843. 799.5	0.1130E-02	0.0000E+00	1638.	0.0000E+00	13.50	0.100000E-01
10	1843. 799.6	0.9757E-03	0.0000E+00	1654.	0.0000E+00	13.50	0.100000E-01
11	1843. 799.6	0.9549E-01	0.0000E+00	1656.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.53766E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.21928E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.89430E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 6069.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	0.7663E-03	0.0000E+00	2008.	0.0000E+00	13.50	0.100000E-01
2	768.3	514.9	0.4823E-03	0.0000E+00	2067.	0.0000E+00	13.50	0.100000E-01
3	768.6	514.9	0.3450E-03	0.0000E+00	2120.	0.0000E+00	13.50	0.100000E-01
4	768.9	514.9	0.2341E-03	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	769.1	515.0	0.1704E-03	0.0000E+00	2198.	0.0000E+00	13.50	0.100000E-01
6	769.3	515.0	0.1301E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
7	769.4	515.1	0.1048E-03	0.0000E+00	2250.	0.0000E+00	13.50	0.100000E-01
8	769.6	515.1	0.8932E-04	0.0000E+00	2271.	0.0000E+00	13.50	0.100000E-01
9	769.8	515.1	0.7666E-04	0.0000E+00	2290.	0.0000E+00	13.50	0.100000E-01
10	769.9	515.2	0.6619E-04	0.0000E+00	2307.	0.0000E+00	13.50	0.100000E-01
11	770.0	515.2	0.6478E-02	0.0000E+00	2310.	0.0000E+00	13.50	0.100000E-01

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	.	.	.	0	0													

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1230.0

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1394.4

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 551.66

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2072.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 440.49

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2183.9

0.00 FT BELOW THE WATER SURFACE

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(LEGEND... + = .LT. .01    . = .LT. .0001    0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	113.0	0.0000E+00	419.0	0.0000E+00	13.50	0.200000E-02
2	3987.	1368.	5.895	0.0000E+00	453.4	0.0000E+00	13.50	0.200000E-02
3	3987.	1368.	4.299	0.0000E+00	484.4	0.0000E+00	13.50	0.200000E-02
4	3987.	1368.	3.093	0.0000E+00	510.1	0.0000E+00	13.50	0.200000E-02
5	3987.	1368.	2.260	0.0000E+00	531.0	0.0000E+00	13.50	0.200000E-02
6	3988.	1368.	1.742	0.0000E+00	548.3	0.0000E+00	13.50	0.200000E-02
7	3988.	1368.	1.384	0.0000E+00	563.0	0.0000E+00	13.50	0.200000E-02
8	3988.	1368.	1.184	0.0000E+00	576.0	0.0000E+00	13.50	0.200000E-02
9	3988.	1368.	1.026	0.0000E+00	587.6	0.0000E+00	13.50	0.200000E-02
10	3988.	1368.	0.9074	0.0000E+00	598.2	0.0000E+00	13.50	0.200000E-02
11	4123.	1404.	305.7	0.0000E+00	599.8	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 368.63
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2255.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 308.49
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2315.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 258.17
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2366.2

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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	66.23	0.0000E+00	853.9	0.0000E+00	0.200000E-02
2	2914.	1084.	3.455	0.0000E+00	898.1	0.0000E+00	0.200000E-02
3	2914.	1084.	2.520	0.0000E+00	937.5	0.0000E+00	0.200000E-02
4	2914.	1084.	1.813	0.0000E+00	970.0	0.0000E+00	0.200000E-02
5	2915.	1084.	1.325	0.0000E+00	996.2	0.0000E+00	0.200000E-02
6	2915.	1084.	1.021	0.0000E+00	1018.	0.0000E+00	0.200000E-02
7	2915.	1084.	0.8114	0.0000E+00	1036.	0.0000E+00	0.200000E-02
8	2915.	1084.	0.6937	0.0000E+00	1052.	0.0000E+00	0.200000E-02
9	2915.	1084.	0.6011	0.0000E+00	1067.	0.0000E+00	0.200000E-02
10	2916.	1084.	0.5318	0.0000E+00	1080.	0.0000E+00	0.200000E-02
11	3050.	1120.	179.2	0.0000E+00	1082.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 216.05
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2408.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 180.81
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2443.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 151.31
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2472.2

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0
10		.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0
11		.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
12		.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0
13		.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
14		.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0	0
15		.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
16		+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0	0
17		+	.	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
18		+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
19		+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0	0
20		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
21		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
22		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
23		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
24		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
25		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
26		+	+	+	+	.	.	.	.	.	.	0	0	0	0	0	0	0
27		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
28		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
29		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
30		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
31		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
32		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
33		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
34		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
35		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
36		+	+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0
37		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
38		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
39		+	+	+	.	.	.	.	.	.	.	0	0	0	0	0	0	0
40		+	+	+	.													

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	799.2	38.81	0.0000E+00	1389.	0.0000E+00	0.200000E-02
2	1841.	799.3	2.025	0.0000E+00	1441.	0.0000E+00	0.200000E-02
3	1841.	799.3	1.477	0.0000E+00	1487.	0.0000E+00	0.200000E-02
4	1842.	799.3	1.063	0.0000E+00	1526.	0.0000E+00	0.200000E-02
5	1842.	799.4	0.7763	0.0000E+00	1556.	0.0000E+00	0.200000E-02
6	1842.	799.4	0.5984	0.0000E+00	1582.	0.0000E+00	0.200000E-02
7	1842.	799.5	0.4755	0.0000E+00	1603.	0.0000E+00	0.200000E-02
8	1842.	799.5	0.4066	0.0000E+00	1622.	0.0000E+00	0.200000E-02
9	1843.	799.5	0.3523	0.0000E+00	1638.	0.0000E+00	0.200000E-02
10	1843.	799.6	0.3117	0.0000E+00	1654.	0.0000E+00	0.200000E-02
11	1977.	835.3	105.0	0.0000E+00	1656.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 126.63
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2496.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 105.97
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2515.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 88.681
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2532.0

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	22.75	0.0000E+00	2008.	0.0000E+00	13.50	0.200000E-02
2	768.3	514.9	1.187	0.0000E+00	2067.	0.0000E+00	13.50	0.200000E-02
3	768.6	514.9	0.8655	0.0000E+00	2120.	0.0000E+00	13.50	0.200000E-02
4	768.9	514.9	0.6228	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	769.1	515.0	0.4550	0.0000E+00	2198.	0.0000E+00	13.50	0.200000E-02
6	769.3	515.0	0.3507	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
7	769.4	515.1	0.2787	0.0000E+00	2250.	0.0000E+00	13.50	0.200000E-02
8	769.6	515.1	0.2383	0.0000E+00	2271.	0.0000E+00	13.50	0.200000E-02
9	769.8	515.1	0.2065	0.0000E+00	2290.	0.0000E+00	13.50	0.200000E-02
10	769.9	515.2	0.1827	0.0000E+00	2307.	0.0000E+00	13.50	0.200000E-02
11	904.7	550.9	61.55	0.0000E+00	2310.	0.0000E+00	13.50	0.200000E-02

[illegible]

[illegible]

[illegible]

THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6	0000	.	.	.	.	.	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7	0000	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
12	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
13	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
14	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
15	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
16	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
17	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
18	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
19	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
20	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
21	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
22	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
23	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
24	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
25	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
26	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
27	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
28	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
29	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
30	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
31	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
32	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
33	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
34	0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
35	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
36	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
37	0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
38	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
39	0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
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42	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
43	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
44	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
45	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
46	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
47	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
48	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
49	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
50	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
51	0000	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
52	0000	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
53	0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
54	0000	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
55	0000	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
56	0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
57	0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	.01	.01	.01	.01	.	+	+	+	+	.	.	.	
58	0000	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.	.01	.02	.03	.02	.01	+	+	+	.	.	.	
59	0000	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	.01	.02	.04	.04	.03	.02	+	+	+	.	.	.	

[illegible]

[illegible]

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BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

[illegible]

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TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM, 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
6	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0
7	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
8	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0
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17	0000	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
18	0000	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
19	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
20	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
21	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
22	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
23	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
24	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
25	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
26	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
27	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
28	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
29	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
30	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
31	0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
32	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
33	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
34	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
35	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
36	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
37	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
38	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
39	0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
40	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
41	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
42	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
43	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
44	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
45	0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
46	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
47	0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
48	0000	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
49	0000	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
50	0000	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
51	0000	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
52	0000	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
53	0000	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
54	0000	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
55	0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
56	0000	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
57	0000	0	0	0	0	0	0	0	.	.	.	.	.	.	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
58	0000	0	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0
59	0000	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	.01	.01	.01	.01	+	+	+	+	.	.	.	0	0

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SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.157E+02	3975.	1350.
2.00	0.0	0.308E+00	2925.	1050.
3.00	0.0	0.871E-02	1875.	825.
4.00	0.0	0.300E-03	750.	525.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.231E+03	4050.	1350.
2.00	0.0	0.420E+02	3000.	1125.
3.00	0.0	0.103E+02	1950.	825.
4.00	0.0	0.305E+01	825.	525.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)    L(FT)    W(FT)    AREA(SQ FT)    L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1650. FT (ZBARGE) OR ABOUT GRID POINT #23 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1965	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.9320E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.3930E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.3290	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.3420

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 69.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22666667E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 252.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1650.	1) = 114.6	8.790	0.3623E-01	1303.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1650.	1) = 128.4	8.827	0.7117	28.70	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1650.	1) = 144.6	9.538	0.6070	27.72	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1650.	1) = 160.2	10.15	0.4487	22.81	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1650.	1) = 173.5	10.59	0.3172	17.52	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1650.	1) = 184.5	10.91	0.2280	13.41	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1650.	1) = 193.7	11.14	0.1709	10.54	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1650.	1) = 201.4	11.31	0.1341	8.585	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1650.	1) = 208.2	11.44	0.1096	7.243	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1650.	1) = 214.3	11.55	0.9280E-01	6.299	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1650.	1) = 214.5	10.08	3.420	9165.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1650.	2) = 1 114.6	8.790	0.3623E-01	617.9	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1650.	2) = 2 128.4	8.827	0.7117	13.61	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1650.	2) = 3 144.6	9.538	0.6070	13.15	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1650.	2) = 4 160.2	10.15	0.4487	10.82	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1650.	2) = 5 173.5	10.59	0.3172	8.311	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1650.	2) = 6 184.5	10.91	0.2280	6.357	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1650.	2) = 7 193.7	11.14	0.1709	4.998	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1650.	2) = 8 201.4	11.31	0.1341	4.072	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1650.	2) = 9 208.2	11.44	0.1096	3.435	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1650.	2) = 10 214.3	11.55	0.9280E-01	2.987	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1650.	2) = 11 214.5	10.08	3.420	4347.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050. 1650.	3) = 114.6	8.790	0.3623E-01	260.5	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050. 1650.	3) = 128.4	8.827	0.7117	5.740	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050. 1650.	3) = 144.6	9.538	0.6070	5.543	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051. 1650.	3) = 160.2	10.15	0.4487	4.561	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051. 1650.	3) = 173.5	10.59	0.3172	3.505	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051. 1650.	3) = 184.5	10.91	0.2280	2.681	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051. 1650.	3) = 193.7	11.14	0.1709	2.107	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051. 1650.	3) = 201.4	11.31	0.1341	1.717	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051. 1650.	3) = 208.2	11.44	0.1096	1.449	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051. 1650.	3) = 214.3	11.55	0.9280E-01	1.259	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051. 1650.	3) = 214.5	10.08	3.420	1833.	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.57	5050.	1650.	4) = 114.6	13.50	0.1000E-02	5382.	0.0000E+00	26	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.13	5050.	1650.	4) = 128.4	13.50	0.1000E-02	4381.	0.0000E+00	51	26
NEW CLOUD CREATED, NTCLD(K) (K = 31.70	5050.	1650.	4) = 144.6	13.50	0.1000E-02	3116.	0.0000E+00	76	51
NEW CLOUD CREATED, NTCLD(K) (K = 32.27	5051.	1650.	4) = 160.2	13.50	0.1000E-02	2066.	0.0000E+00	101	76
NEW CLOUD CREATED, NTCLD(K) (K = 32.83	5051.	1650.	4) = 173.5	13.50	0.1000E-02	1271.	0.0000E+00	126	101
NEW CLOUD CREATED, NTCLD(K) (K = 33.40	5051.	1650.	4) = 184.5	13.50	0.1000E-02	732.3	0.0000E+00	151	126
NEW CLOUD CREATED, NTCLD(K) (K = 33.97	5051.	1650.	4) = 193.7	13.50	0.1000E-02	400.7	0.0000E+00	176	151
NEW CLOUD CREATED, NTCLD(K) (K = 34.53	5051.	1650.	4) = 201.4	13.50	0.1000E-02	210.5	0.0000E+00	201	176
NEW CLOUD CREATED, NTCLD(K) (K = 35.10	5051.	1650.	4) = 208.2	13.50	0.1000E-02	106.9	0.0000E+00	226	201
NEW CLOUD CREATED, NTCLD(K) (K = 35.67	5051.	1650.	4) = 214.3	13.50	0.1000E-02	52.85	0.0000E+00	251	226
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051.	1650.	4) = 214.5	10.08	3.420	47.69	0.0000E+00	252	251

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.69	5051.	1650.	5) = 1 214.5	10.08	3.420	0.00000E+00	0.00000E+00	252	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 10611.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 135.08

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4897.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 54.478

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 4978.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 22.218

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5010.6

0.00 FT BELOW THE WATER SURFACE

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	1.309	0.0000E+00	420.7	0.0000E+00	0.100000E-01
2	3987.	1368.	0.9176	0.0000E+00	443.1	0.0000E+00	0.100000E-01
3	3987.	1368.	0.8689	0.0000E+00	468.8	0.0000E+00	0.100000E-01
4	3987.	1368.	0.6691	0.0000E+00	492.8	0.0000E+00	0.100000E-01
5	3988.	1368.	0.5054	0.0000E+00	512.9	0.0000E+00	0.100000E-01
6	3988.	1368.	0.3819	0.0000E+00	529.3	0.0000E+00	0.100000E-01
7	3988.	1368.	0.2986	0.0000E+00	542.7	0.0000E+00	0.100000E-01
8	3988.	1368.	0.2463	0.0000E+00	554.0	0.0000E+00	0.100000E-01
9	3988.	1368.	0.2053	0.0000E+00	563.8	0.0000E+00	0.100000E-01
10	3989.	1368.	0.1713	0.0000E+00	572.5	0.0000E+00	0.100000E-01
11	3989.	1368.	16.64	0.0000E+00	572.8	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.0614
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5023.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.6956
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5029.1

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5072
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5031.3
MAX CONC IS 0.00000009 OUTPUT SUPPRESSED AT 0.00 FT

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	0.8882E-01	0.0000E+00	856.1	0.0000E+00	0.100000E-01
2	2914.	1084.	0.6225E-01	0.0000E+00	884.9	0.0000E+00	0.100000E-01
3	2914.	1084.	0.5894E-01	0.0000E+00	917.7	0.0000E+00	0.100000E-01
4	2915.	1084.	0.4539E-01	0.0000E+00	948.2	0.0000E+00	0.100000E-01
5	2915.	1084.	0.3428E-01	0.0000E+00	973.5	0.0000E+00	0.100000E-01
6	2915.	1084.	0.2590E-01	0.0000E+00	994.1	0.0000E+00	0.100000E-01
7	2915.	1084.	0.2026E-01	0.0000E+00	1011.	0.0000E+00	0.100000E-01
8	2915.	1084.	0.1670E-01	0.0000E+00	1025.	0.0000E+00	0.100000E-01
9	2916.	1084.	0.1393E-01	0.0000E+00	1037.	0.0000E+00	0.100000E-01
10	2916.	1084.	0.1162E-01	0.0000E+00	1048.	0.0000E+00	0.100000E-01
11	2916.	1084.	1.129	0.0000E+00	1048.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.61469
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.2

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.25070
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10224
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 799.2	0.6026E-02	0.0000E+00	1391.	0.0000E+00	13.50	0.100000E-01
2	1841. 799.3	0.4223E-02	0.0000E+00	1425.	0.0000E+00	13.50	0.100000E-01
3	1841. 799.3	0.3998E-02	0.0000E+00	1464.	0.0000E+00	13.50	0.100000E-01
4	1842. 799.3	0.3079E-02	0.0000E+00	1500.	0.0000E+00	13.50	0.100000E-01
5	1842. 799.4	0.2326E-02	0.0000E+00	1530.	0.0000E+00	13.50	0.100000E-01
6	1842. 799.4	0.1757E-02	0.0000E+00	1554.	0.0000E+00	13.50	0.100000E-01
7	1842. 799.4	0.1374E-02	0.0000E+00	1573.	0.0000E+00	13.50	0.100000E-01
8	1843. 799.5	0.1133E-02	0.0000E+00	1590.	0.0000E+00	13.50	0.100000E-01
9	1843. 799.5	0.9449E-03	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01
10	1843. 799.6	0.7881E-03	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01
11	1843. 799.6	0.7659E-01	0.0000E+00	1617.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.41699E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17006E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.69358E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 5032.8
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	0.4088E-03	0.0000E+00	2011.	0.0000E+00	13.50	0.100000E-01
2	768.3	514.9	0.2864E-03	0.0000E+00	2050.	0.0000E+00	13.50	0.100000E-01
3	768.7	514.9	0.2712E-03	0.0000E+00	2094.	0.0000E+00	13.50	0.100000E-01
4	769.0	514.9	0.2089E-03	0.0000E+00	2134.	0.0000E+00	13.50	0.100000E-01
5	769.2	515.0	0.1578E-03	0.0000E+00	2168.	0.0000E+00	13.50	0.100000E-01
6	769.5	515.0	0.1192E-03	0.0000E+00	2195.	0.0000E+00	13.50	0.100000E-01
7	769.6	515.0	0.9322E-04	0.0000E+00	2217.	0.0000E+00	13.50	0.100000E-01
8	769.8	515.1	0.7687E-04	0.0000E+00	2236.	0.0000E+00	13.50	0.100000E-01
9	770.0	515.1	0.6410E-04	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01
10	770.1	515.2	0.5346E-04	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01
11	770.1	515.2	0.5196E-02	0.0000E+00	2266.	0.0000E+00	13.50	0.100000E-01

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 934.32

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1187.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 428.28

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1693.9

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 347.78

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1774.4

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	97.02	0.0000E+00	420.7	0.0000E+00	0.200000E-02
2	3987.	1368.	3.413	0.0000E+00	443.1	0.0000E+00	0.200000E-02
3	3987.	1368.	3.269	0.0000E+00	468.8	0.0000E+00	0.200000E-02
4	3987.	1368.	2.684	0.0000E+00	492.8	0.0000E+00	0.200000E-02
5	3988.	1368.	2.040	0.0000E+00	512.9	0.0000E+00	0.200000E-02
6	3988.	1368.	1.557	0.0000E+00	529.3	0.0000E+00	0.200000E-02
7	3988.	1368.	1.221	0.0000E+00	542.7	0.0000E+00	0.200000E-02
8	3988.	1368.	0.9941	0.0000E+00	554.0	0.0000E+00	0.200000E-02
9	3988.	1368.	0.8378	0.0000E+00	563.8	0.0000E+00	0.200000E-02
10	3989.	1368.	0.7256	0.0000E+00	572.5	0.0000E+00	0.200000E-02
11	4069.	1390.	234.0	0.0000E+00	572.8	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 291.04
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1831.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 243.56
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1878.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 203.83
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1918.4

[illegible]

[illegible]

[illegible]

[illegible]

$$\dots + = .LT. .01 \quad . = .LT.$$

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	56.86	0.0000E+00	856.1	0.0000E+00	0.200000E-02
2	2914.	1084.	2.000	0.0000E+00	884.9	0.0000E+00	0.200000E-02
3	2914.	1084.	1.916	0.0000E+00	917.7	0.0000E+00	0.200000E-02
4	2915.	1084.	1.573	0.0000E+00	948.2	0.0000E+00	0.200000E-02
5	2915.	1084.	1.196	0.0000E+00	973.5	0.0000E+00	0.200000E-02
6	2915.	1084.	0.9125	0.0000E+00	994.1	0.0000E+00	0.200000E-02
7	2915.	1084.	0.7159	0.0000E+00	1011.	0.0000E+00	0.200000E-02
8	2915.	1084.	0.5826	0.0000E+00	1025.	0.0000E+00	0.200000E-02
9	2916.	1084.	0.4910	0.0000E+00	1037.	0.0000E+00	0.200000E-02
10	2916.	1084.	0.4253	0.0000E+00	1048.	0.0000E+00	0.200000E-02
11	2997.	1105.	137.2	0.0000E+00	1048.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 170.58
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1951.5

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 142.75
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1979.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 119.46
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2002.1

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	1841.	799.2	33.33	0.0000E+00	1391.	0.0000E+00	13.50	0.200000E-02
2	1841.	799.3	1.172	0.0000E+00	1425.	0.0000E+00	13.50	0.200000E-02
3	1841.	799.3	1.123	0.0000E+00	1464.	0.0000E+00	13.50	0.200000E-02
4	1842.	799.3	0.9219	0.0000E+00	1500.	0.0000E+00	13.50	0.200000E-02
5	1842.	799.4	0.7007	0.0000E+00	1530.	0.0000E+00	13.50	0.200000E-02
6	1842.	799.4	0.5348	0.0000E+00	1554.	0.0000E+00	13.50	0.200000E-02
7	1842.	799.4	0.4196	0.0000E+00	1573.	0.0000E+00	13.50	0.200000E-02
8	1843.	799.5	0.3415	0.0000E+00	1590.	0.0000E+00	13.50	0.200000E-02
9	1843.	799.5	0.2878	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02
10	1843.	799.6	0.2493	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02
11	1924.	821.0	80.38	0.0000E+00	1617.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 99.974
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2021.0

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 83.664
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2036.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 70.016
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2049.2

0.00 FT BELOW THE WATER SURFACE

M	N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	
2	0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00		
3	0000	1.1	1.2	1.2	1.3	1.3	1.3	1.3	1.3	1.3	1.2	1.2	1.1	1.0	.95	.85	.75	.65	.56	.47	.39	.32	.26	.20	.16	.12	0	0	0	0	0	
4	0000	1.2	1.3	1.4	1.5	1.5	1.5	1.5	1.5	1.5	1.4	1.3	1.2	1.1	1.0	.97	.85	.74	.63	.53	.44	.36	.29	.23	.18	.14	0	0	0	0	0	
5	0000	1.4	1.5	1.6	1.6	1.7	1.7	1.7	1.7	1.6	1.6	1.5	1.4	1.3	1.2	1.0	.95	.82	.71	.59	.49	.40	.32	.26	.20	.16	0	0	0	0	0	
6	0000	1.5	1.7	1.7	1.8	1.9	1.9	1.9	1.9	1.8	1.7	1.7	1.5	1.4	1.3	1.1	1.0	.91	.78	.65	.54	.44	.36	.28	.22	.17	0	0	0	0	0	
7	0000	1.7	1.8	1.9	2.0	2.0	2.0	2.0	2.0	2.0	1.9	1.8	1.7	1.5	1.4	1.2	1.1	.99	.84	.71	.59	.48	.39	.31	.24	.19	0	0	0	0	0	
8	0000	1.8	1.9	2.0	2.1	2.2	2.2	2.2	2.2	2.1	2.0	1.9	1.8	1.7	1.5	1.3	1.2	1.0	.90	.76	.63	.52	.42	.33	.26	.20	0	0	0	0	0	
9	0000	1.9	2.0	2.1	2.2	2.3	2.3	2.3	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.95	.80	.66	.54	.44	.35	.27	.21	0	0	0	0	0	0	
10	0000	2.0	2.1	2.2	2.3	2.4	2.4	2.4	2.3	2.2	2.1	2.0	1.8	1.6	1.5	1.3	1.1	.98	.83	.69	.56	.45	.36	.28	.22	0	0	0	0	0	0	
11	0000	2.0	2.1	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.8	1.7	1.5	1.3	1.1	1.0	.85	.70	.58	.46	.37	.29	.22	0	0	0	0	0	0	
12	0000	2.0	2.2	2.3	2.4	2.4	2.4	2.4	2.4	2.3	2.2	2.0	1.9	1.7	1.5	1.3	1.1	1.0	.85	.71	.58	.47	.37	.29	.22	0	0	0	0	0	0	
13	0000	2.0	2.1	2.3	2.3	2.4	2.4	2.4	2.4	2.3	2.3	2.1	2.0	1.8	1.7	1.5	1.3	1.1	1.0	.84	.70	.57	.46	.37	.29	.22	0	0	0	0	0	0
14	0000	1.9	2.1	2.2	2.3	2.3	2.4	2.3	2.3	2.2	2.1	2.0	1.8	1.6	1.4	1.3	1.1	.98	.83	.69	.56	.45	.36	.28	.22	0	0	0	0	0	0	
15	0000	1.9	2.0	2.1	2.2	2.2	2.3	2.3	2.2	2.1	2.0	1.9	1.7	1.6	1.4	1.2	1.1	.94	.79	.66	.54	.44	.35	.27	.21	0	0	0	0	0	0	
16	0000	1.8	1.9	2.0	2.1	2.1	2.1	2.1	2.1	2.0	1.9	1.8	1.6	1.5	1.3	1.2	1.0	.89	.75	.63	.51	.41	.33	.26	.20	0	0	0	0	0	0	
17	0000	1.6	1.8	1.9	1.9	2.0	2.0	2.0	2.0	1.9	1.9	1.8	1.7	1.5	1.4	1.2	1.1	.98	.84	.71	.59	.48	.39	.31	.24	.19	0	0	0	0		

[illegible]

[illegible]

[illegible]

(CU FT/GRID SQUARE) , 14400.00 SECONDS AFTER DUMP

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	19.53	0.0000E+00	2011.	0.0000E+00	13.50	0.200000E-02
2	768.3	514.9	0.6870	0.0000E+00	2050.	0.0000E+00	13.50	0.200000E-02
3	768.7	514.9	0.6581	0.0000E+00	2094.	0.0000E+00	13.50	0.200000E-02
4	769.0	514.9	0.5403	0.0000E+00	2134.	0.0000E+00	13.50	0.200000E-02
5	769.2	515.0	0.4107	0.0000E+00	2168.	0.0000E+00	13.50	0.200000E-02
6	769.5	515.0	0.3134	0.0000E+00	2195.	0.0000E+00	13.50	0.200000E-02
7	769.6	515.0	0.2459	0.0000E+00	2217.	0.0000E+00	13.50	0.200000E-02
8	769.8	515.1	0.2001	0.0000E+00	2236.	0.0000E+00	13.50	0.200000E-02
9	770.0	515.1	0.1687	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02
10	770.1	515.2	0.1461	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02
11	850.9	536.6	47.11	0.0000E+00	2266.	0.0000E+00	13.50	0.200000E-02

0 = .LT. .000001)

0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8		.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14		.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36		.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37		.	.	.	0	0</												

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 17766.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	0	0	0	0	0													

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

59	0000	0	0	0	0	0	.	.	.	.	+	+	+	.01	.05	.23	.76	1.8	3.0	3.2	2.3	1.1	.40	.10	.01	+	+	.	0	0
----	------	---	---	---	---	---	---	---	---	---	---	---	---	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	---	---	---	---	---

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
4	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
5	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
6	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
7	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
8	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
9	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
10	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
11	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
12	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
13	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
14	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
15	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
16	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
17	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
18	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
19	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
20	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
21	+	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
22	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
23	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
24	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
25	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
26	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
27	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
28	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
29	+	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
30	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
31	.	.	.	.	.	.	.	.	.	0	.	0	0	0	0	0	0	00000
32	.	.	.	.	.	.	.	.	.	0	.	0	0	0	0	0	0	00000
33	.	.	.	.	.	.	.	.	.	0	.	0	0	0	0	0	0	00000
34	.	.	.	.	.	.	.	.	0	.	.	0	0	0	0	0	0	00000
35	.	.	.	.	.	.	.	.	0	.	.	0	0	0	0	0	0	00000
36	.	.	.	.	.	.	.	0	0	.	.	0	0	0	0	0	0	00000
37	.	.	.	.	.	.	.	0	0	.	.	0	0	0	0	0	0	00000
38	.	.	.	.	.	.	.	0	0	.	.	0	0	0	0	0	0	00000
39	.	.	.	.	.	0	.	0	0	.	.	0	0	0	0	0	0	00000
40	.	.	.	.	.	0	.	0	0	.	.	0	0	0	0	0	0	00000

[illegible]

TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM, 1200.00 SECONDS AFTER DUMP

...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000	0000
3	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
4	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
5	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
6	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
7	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
8	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
9	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
10	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
11	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
12	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
13	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
14	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
15	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
16	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
17	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
18	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
19	0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
20	0000	.	.	.	.	.	.	.	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
21	0000	.	.	.	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
22	0000	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
23	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
24	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
25	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
26	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
27	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
28	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
29	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
30	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
31	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
32	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
33	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
34	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
35	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
36	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
37	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
38	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
39	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
40	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
41	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
42	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
43	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
44	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
45	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
46	0000	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0
47	0000	0	.	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
48	0000	0	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
49	0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
50	0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
51	0000	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
52	0000	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
53	0000	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
54	0000	0	0	0	0	0	0	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
55	0000	0	0	0	0	0	0	0	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
56	0000	0	0	0	0	0	0	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
57	0000	0	0	0	0	0	0	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
58	0000	0	0	0	0	0	0	0	0	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	0	0	0	0
59	0000	0	0	0	0	0	0	0	0	0	+	+	+	+	+	+	+	+	+.01	.01	.01	+	+	+	+	.	0	0	0	0

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.127E+02	3975.	1350.
2.00	0.0	0.247E+00	2925.	1050.
3.00	0.0	0.694E-02	1875.	825.
4.00	0.0	0.238E-03	750.	525.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.206E+03	4050.	1350.
2.00	0.0	0.353E+02	2925.	1125.
3.00	0.0	0.851E+01	1875.	825.
4.00	0.0	0.249E+01	825.	525.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)  L(FT)    W(FT)    AREA(SQ FT)  L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1650. FT (ZBARGE) OR ABOUT GRID POINT #23 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

BOTTOM SHEAR STRESS, LBS/SQ FT:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 3 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.8085	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1090E-01	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.4500E-02	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.1761

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 67.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.22000000E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 272.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050. 1650.	1) = 1 109.2	7.474	0.6757	4059.	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050. 1650.	1) = 2 130.9	8.150	1.159	174.8	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050. 1650.	1) = 3 152.5	9.308	0.7587	133.0	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050. 1650.	1) = 4 171.5	10.07	0.4927	96.42	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051. 1650.	1) = 5 187.3	10.56	0.3331	70.53	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051. 1650.	1) = 6 200.5	10.89	0.2393	53.71	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051. 1650.	1) = 7 211.8	11.13	0.1828	42.90	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051. 1650.	1) = 8 221.7	11.31	0.1469	35.75	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051. 1650.	1) = 9 230.7	11.46	0.1227	30.81	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051. 1650.	1) = 10 238.9	11.58	0.1054	27.20	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051. 1650.	1) = 11 239.2	9.685	3.815	0.3893E+05	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050. 1650.	2) = 1 109.2	7.474	0.6757	54.72	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050. 1650.	2) = 2 130.9	8.150	1.159	2.357	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050. 1650.	2) = 3 152.5	9.308	0.7587	1.793	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050. 1650.	2) = 4 171.5	10.07	0.4927	1.300	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051. 1650.	2) = 5 187.3	10.56	0.3331	0.9510	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051. 1650.	2) = 6 200.5	10.89	0.2393	0.7240	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051. 1650.	2) = 7 211.8	11.13	0.1828	0.5784	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051. 1650.	2) = 8 221.7	11.31	0.1469	0.4821	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051. 1650.	2) = 9 230.7	11.46	0.1227	0.4154	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051. 1650.	2) = 10 238.9	11.58	0.1054	0.3666	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051. 1650.	2) = 11 239.2	9.685	3.815	524.9	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.59	5050. 1650.	3) = 109.2	7.474	0.6757	22.59	0.0000E+00	28	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.19	5050. 1650.	3) = 130.9	8.150	1.159	0.9732	0.0000E+00	55	28
NEW CLOUD CREATED, NTCLD(K) (K = 31.78	5050. 1650.	3) = 152.5	9.308	0.7587	0.7404	0.0000E+00	82	55
NEW CLOUD CREATED, NTCLD(K) (K = 32.38	5050. 1650.	3) = 171.5	10.07	0.4927	0.5367	0.0000E+00	109	82
NEW CLOUD CREATED, NTCLD(K) (K = 32.97	5051. 1650.	3) = 187.3	10.56	0.3331	0.3926	0.0000E+00	136	109
NEW CLOUD CREATED, NTCLD(K) (K = 33.56	5051. 1650.	3) = 200.5	10.89	0.2393	0.2989	0.0000E+00	163	136
NEW CLOUD CREATED, NTCLD(K) (K = 34.16	5051. 1650.	3) = 211.8	11.13	0.1828	0.2388	0.0000E+00	190	163
NEW CLOUD CREATED, NTCLD(K) (K = 34.75	5051. 1650.	3) = 221.7	11.31	0.1469	0.1990	0.0000E+00	217	190
NEW CLOUD CREATED, NTCLD(K) (K = 35.35	5051. 1650.	3) = 230.7	11.46	0.1227	0.1715	0.0000E+00	244	217
NEW CLOUD CREATED, NTCLD(K) (K = 35.94	5051. 1650.	3) = 238.9	11.58	0.1054	0.1515	0.0000E+00	271	244
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051. 1650.	3) = 239.2	9.685	3.815	216.7	0.0000E+00	272	271

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.96	5051.	1650.	4) = 1 239.2	9.685	3.815	0.0000E+00	0.0000E+00	272	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 43659.

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 100.53

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 488.07

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 40.998

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 547.60

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 16.721

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 571.88

0.00 FT BELOW THE WATER SURFACE

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	1.598	0.0000E+00	411.8	0.0000E+00	0.100000E-01
2	3987.	1368.	0.1670	0.0000E+00	447.2	0.0000E+00	0.100000E-01
3	3987.	1368.	0.1244	0.0000E+00	481.0	0.0000E+00	0.100000E-01
4	3987.	1368.	0.8472E-01	0.0000E+00	509.8	0.0000E+00	0.100000E-01
5	3988.	1368.	0.6078E-01	0.0000E+00	533.4	0.0000E+00	0.100000E-01
6	3988.	1368.	0.4554E-01	0.0000E+00	552.7	0.0000E+00	0.100000E-01
7	3988.	1368.	0.3588E-01	0.0000E+00	569.0	0.0000E+00	0.100000E-01
8	3988.	1368.	0.2958E-01	0.0000E+00	583.3	0.0000E+00	0.100000E-01
9	3988.	1368.	0.2517E-01	0.0000E+00	596.0	0.0000E+00	0.100000E-01
10	3988.	1368.	0.2181E-01	0.0000E+00	607.5	0.0000E+00	0.100000E-01
11	3988.	1368.	14.53	0.0000E+00	607.9	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 6.8193
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 581.78

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 2.7812
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 585.82

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.1343
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 587.46
MAX CONC IS 0.00000006 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	0.1084	0.0000E+00	844.6	0.0000E+00	0.100000E-01
2	2914.	1084.	0.1133E-01	0.0000E+00	890.2	0.0000E+00	0.100000E-01
3	2914.	1084.	0.8437E-02	0.0000E+00	933.3	0.0000E+00	0.100000E-01
4	2915.	1084.	0.5747E-02	0.0000E+00	969.7	0.0000E+00	0.100000E-01
5	2915.	1084.	0.4123E-02	0.0000E+00	999.2	0.0000E+00	0.100000E-01
6	2915.	1084.	0.3089E-02	0.0000E+00	1023.	0.0000E+00	0.100000E-01
7	2915.	1084.	0.2434E-02	0.0000E+00	1044.	0.0000E+00	0.100000E-01
8	2915.	1084.	0.2006E-02	0.0000E+00	1061.	0.0000E+00	0.100000E-01
9	2915.	1084.	0.1707E-02	0.0000E+00	1077.	0.0000E+00	0.100000E-01
10	2916.	1084.	0.1479E-02	0.0000E+00	1091.	0.0000E+00	0.100000E-01
11	2916.	1084.	0.9855	0.0000E+00	1092.	0.0000E+00	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.46260
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.13

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.18866
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.40

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.76945E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.51
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	.	.	.	0	0</												

[illegible]

SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	799.2	0.7355E-02	0.0000E+00	1378.	0.0000E+00	13.50	0.100000E-01
2	1841.	799.3	0.7685E-03	0.0000E+00	1432.	0.0000E+00	13.50	0.100000E-01
3	1841.	799.3	0.5723E-03	0.0000E+00	1482.	0.0000E+00	13.50	0.100000E-01
4	1842.	799.3	0.3899E-03	0.0000E+00	1525.	0.0000E+00	13.50	0.100000E-01
5	1842.	799.4	0.2797E-03	0.0000E+00	1560.	0.0000E+00	13.50	0.100000E-01
6	1842.	799.4	0.2096E-03	0.0000E+00	1588.	0.0000E+00	13.50	0.100000E-01
7	1842.	799.5	0.1651E-03	0.0000E+00	1612.	0.0000E+00	13.50	0.100000E-01
8	1842.	799.5	0.1361E-03	0.0000E+00	1632.	0.0000E+00	13.50	0.100000E-01
9	1843.	799.6	0.1158E-03	0.0000E+00	1650.	0.0000E+00	13.50	0.100000E-01
10	1843.	799.6	0.1003E-03	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01
11	1843.	799.6	0.6685E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.31381E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.56

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.12798E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.57

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.52197E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 588.58
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	0.4989E-03	0.0000E+00	1996.	0.0000E+00	13.50	0.100000E-01
2	768.3	514.9	0.5213E-04	0.0000E+00	2057.	0.0000E+00	13.50	0.100000E-01
3	768.7	514.9	0.3883E-04	0.0000E+00	2114.	0.0000E+00	13.50	0.100000E-01
4	768.9	514.9	0.2645E-04	0.0000E+00	2163.	0.0000E+00	13.50	0.100000E-01
5	769.1	515.0	0.1897E-04	0.0000E+00	2202.	0.0000E+00	13.50	0.100000E-01
6	769.3	515.0	0.1422E-04	0.0000E+00	2233.	0.0000E+00	13.50	0.100000E-01
7	769.5	515.1	0.1120E-04	0.0000E+00	2260.	0.0000E+00	13.50	0.100000E-01
8	769.7	515.1	0.9233E-05	0.0000E+00	2283.	0.0000E+00	13.50	0.100000E-01
9	769.8	515.2	0.7856E-05	0.0000E+00	2304.	0.0000E+00	13.50	0.100000E-01
10	770.0	515.2	0.6807E-05	0.0000E+00	2322.	0.0000E+00	13.50	0.100000E-01
11	770.0	515.2	0.4535E-02	0.0000E+00	2323.	0.0000E+00	13.50	0.100000E-01

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M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

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BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 195.81

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 47.185

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 163.87

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 79.133

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 137.13

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 105.87

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[illegible]

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SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	3986.	1368.	13.39	0.0000E+00	411.8	0.0000E+00	0.200000E-02
2	3987.	1368.	0.5799	0.0000E+00	447.2	0.0000E+00	0.200000E-02
3	3987.	1368.	0.4376	0.0000E+00	481.0	0.0000E+00	0.200000E-02
4	3987.	1368.	0.3164	0.0000E+00	509.8	0.0000E+00	0.200000E-02
5	3988.	1368.	0.2289	0.0000E+00	533.4	0.0000E+00	0.200000E-02
6	3988.	1368.	0.1739	0.0000E+00	552.7	0.0000E+00	0.200000E-02
7	3988.	1368.	0.1386	0.0000E+00	569.0	0.0000E+00	0.200000E-02
8	3988.	1368.	0.1154	0.0000E+00	583.3	0.0000E+00	0.200000E-02
9	3988.	1368.	0.9921E-01	0.0000E+00	596.0	0.0000E+00	0.200000E-02
10	3988.	1368.	0.8741E-01	0.0000E+00	607.5	0.0000E+00	0.200000E-02
11	3988.	1368.	121.6	0.0000E+00	607.9	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 114.76
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 128.24

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 96.040
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 146.96

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 80.373
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 162.62

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
4		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
5		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
6		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
7		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
8		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
9		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
10		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
11		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
12		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
13		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
14		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
15		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
16		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
17		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
18		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
19		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
20		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
21		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
22		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
23		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
24		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
25		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
26		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
27		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
28		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
29	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
30	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
31	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
32	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
33	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
34	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0000
35	.	.	.															

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913.	1084.	7.846	0.0000E+00	844.6	0.0000E+00	0.200000E-02
2	2914.	1084.	0.3399	0.0000E+00	890.2	0.0000E+00	0.200000E-02
3	2914.	1084.	0.2565	0.0000E+00	933.3	0.0000E+00	0.200000E-02
4	2915.	1084.	0.1854	0.0000E+00	969.7	0.0000E+00	0.200000E-02
5	2915.	1084.	0.1342	0.0000E+00	999.2	0.0000E+00	0.200000E-02
6	2915.	1084.	0.1019	0.0000E+00	1023.	0.0000E+00	0.200000E-02
7	2915.	1084.	0.8126E-01	0.0000E+00	1044.	0.0000E+00	0.200000E-02
8	2915.	1084.	0.6761E-01	0.0000E+00	1061.	0.0000E+00	0.200000E-02
9	2915.	1084.	0.5815E-01	0.0000E+00	1077.	0.0000E+00	0.200000E-02
10	2916.	1084.	0.5123E-01	0.0000E+00	1091.	0.0000E+00	0.200000E-02
11	2916.	1084.	71.25	0.0000E+00	1092.	0.0000E+00	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 67.261
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 175.69

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 56.288
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 186.56

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 47.106
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 195.56

[illegible]

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[illegible]

[illegible]

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841.	799.2	4.599	0.0000E+00	1378.	0.0000E+00	13.50	0.200000E-02
2	1841.	799.3	0.1992	0.0000E+00	1432.	0.0000E+00	13.50	0.200000E-02
3	1841.	799.3	0.1503	0.0000E+00	1482.	0.0000E+00	13.50	0.200000E-02
4	1842.	799.3	0.1087	0.0000E+00	1525.	0.0000E+00	13.50	0.200000E-02
5	1842.	799.4	0.7864E-01	0.0000E+00	1560.	0.0000E+00	13.50	0.200000E-02
6	1842.	799.4	0.5974E-01	0.0000E+00	1588.	0.0000E+00	13.50	0.200000E-02
7	1842.	799.5	0.4762E-01	0.0000E+00	1612.	0.0000E+00	13.50	0.200000E-02
8	1842.	799.5	0.3962E-01	0.0000E+00	1632.	0.0000E+00	13.50	0.200000E-02
9	1843.	799.6	0.3408E-01	0.0000E+00	1650.	0.0000E+00	13.50	0.200000E-02
10	1843.	799.6	0.3002E-01	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02
11	1843.	799.6	41.76	0.0000E+00	1667.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 39.421
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 203.00

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 32.990
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 209.11

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 27.608
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 214.08

0.00 FT BELOW THE WATER SURFACE

[illegible]

[illegible]

[illegible]

[illegible]

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	2.695	0.0000E+00	1996.	0.0000E+00	13.50	0.200000E-02
2	768.3	514.9	0.1167	0.0000E+00	2057.	0.0000E+00	13.50	0.200000E-02
3	768.7	514.9	0.8809E-01	0.0000E+00	2114.	0.0000E+00	13.50	0.200000E-02
4	768.9	514.9	0.6369E-01	0.0000E+00	2163.	0.0000E+00	13.50	0.200000E-02
5	769.1	515.0	0.4609E-01	0.0000E+00	2202.	0.0000E+00	13.50	0.200000E-02
6	769.3	515.0	0.3501E-01	0.0000E+00	2233.	0.0000E+00	13.50	0.200000E-02
7	769.5	515.1	0.2791E-01	0.0000E+00	2260.	0.0000E+00	13.50	0.200000E-02
8	769.7	515.1	0.2322E-01	0.0000E+00	2283.	0.0000E+00	13.50	0.200000E-02
9	769.8	515.2	0.1997E-01	0.0000E+00	2304.	0.0000E+00	13.50	0.200000E-02
10	770.0	515.2	0.1760E-01	0.0000E+00	2322.	0.0000E+00	13.50	0.200000E-02
11	770.0	515.2	24.47	0.0000E+00	2323.	0.0000E+00	13.50	0.200000E-02

(LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

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[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

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[illegible]

[illegible]

[illegible]

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(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
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[illegible]

[illegible]

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.858E+01	3975.	1350.
2.00	0.0	0.172E+00	2925.	1050.
3.00	0.0	0.492E-02	1875.	825.
4.00	0.0	0.170E-03	750.	525.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.699E+02	3975.	1350.
2.00	0.0	0.121E+02	2925.	1050.
3.00	0.0	0.300E+01	1875.	825.
4.00	0.0	0.899E+00	750.	525.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)  L(FT)    W(FT)    AREA(SQ FT)  L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

MODEL: SHORT-TERM FATE OF DREDGED MATERIAL FROM SPLIT HULL BARGE OR HOPPER DREDGE
(PC Version 5.01 MAY, 1993)
(Extended Memory Modification: December, 1997)
This Version Supports Grid Sizes up to 96 x 96 Points

TITLE:

FILE: TmpFile .DUE

AREA: THE PROJECT AREA IS DESCRIBED BY A 49 X 73 GRID.

THERE ARE 49 GRID POINTS (NMAX) IN THE Z-DIRECTION (FROM LEFT TO RIGHT)
AND 73 GRID POINTS (MMAX) IN THE X-DIRECTION (FROM TOP TO BOTTOM).

EXECUTION PARAMETERS:

MODEL COEFFICIENTS SPECIFIED IN INPUT DATA (KEY1 = 1).

PERFORM COMPLETE ANALYSIS INCLUDING DESCENT, COLLAPSE, AND TRANSPORT-DIFFUSION (KEY2 = 0).

PERFORM TIER II INLAND DUMPING INITIAL MIXING EVALUATION
TO COMPARE WATER QUALITY WITH STANDARD (KEY3 = 5).

MIXING ZONE WILL BE COMPUTED SINCE A MIXING ZONE HAS NOT BEEN DESIGNATED.

NO ANALYSIS OF A ZONE OF INITIAL DILUTION REQUESTED.

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF CONVECTIVE DESCENT RESULTS NOT REQUESTED (IPCN = 0).

PRINTING OF DYNAMIC COLLAPSE RESULTS NOT REQUESTED (IPCL = 0).

QUARTERLY PRINTING OF LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED (IPLT = 0).

LONG-TERM TRANSPORT DIFFUSION RESULTS REQUESTED AT THE FOLLOWING 1 DEPTH(S):
0.00 FT

GRID: NUMBER OF LONG TERM GRID POINTS IN Z-DIRECTION (NMAX) = 49
 NUMBER OF LONG TERM GRID POINTS IN X-DIRECTION (MMAX) = 73
 GRID SPACING IN Z-DIRECTION (DZ) = 75.00000 FT
 GRID SPACING IN X-DIRECTION (DX) = 75.00000 FT
 CONSTANT DEPTH GRID SPECIFIED HAVING A DEPTH (DEPC) OF 13.50000 FT.

DEPTH GRID, FEET:

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

CODED GRID:

RANGE OF N IS 1 TO 49

[illegible]

[illegible]

LEGEND FOR CODED GRID: W = WATER POINT
L = LAND POINT
O = OPEN BOUNDARY
B = MIXING ZONE BOUNDARY
Z = ZID BOUNDARY
D = DUMP LOCATION
X = DUMMY POINT

NUMBER OF GRID POINTS WITHIN ESTUARY = 3105

DISPOSAL LOCATION:

THE DUMP LOCATION IS 5025. FT (XBARGE) OR ABOUT GRID POINT #68 FROM THE TOP OF THE GRID
AND 1650. FT (ZBARGE) OR ABOUT GRID POINT #23 FROM THE LEFT EDGE OF THE GRID.

THE BOTTOM SLOPE IN THE X-DIRECTION AT THE DUMP SITE (SLOPEX, POSITIVE IF DEPTH INCREASES
FROM TOP OF GRID TO BOTTOM OF GRID) IS 0.00 DEGREES.

THE BOTTOM SLOPE IN THE Z-DIRECTION AT THE DUMP SITE (SLOPEZ, POSITIVE IF DEPTH INCREASES
FROM LEFT SIDE OF GRID TO RIGHT SIDE OF GRID) IS 0.00 DEGREES.

THE DISPOSAL LOCATION IS AT A HOLE OR DEPRESSION.
THE LENGTH OF THE HOLE IN THE X-DIRECTION (XHOLE) IS 450.00 FT,
THE LENGTH OF THE HOLE IN THE Z-DIRECTION (ZHOLE) IS 450.00 FT AND
THE AVERAGE DEPTH OF THE HOLE (DHOLE) IS 45.00 FT.

AMBIENT DENSITY PROFILE:

DEPTH (FT)	DENSITY (G/CC)
0.0000E+00	1.0240
3.000	1.0240
6.000	1.0240
12.00	1.0240
13.50	1.0240

COMPUTED DEPTH:

THE DEPTH AT THE DUMP LOCATION WAS INTERPOLATED TO BE 13.50 FT.

VELOCITY DISTRIBUTION:

TWO-VELOCITY PROFILES ARE SPECIFIED IN BOTH X AND Z DIRECTIONS FOR USE AT ALL GRID POINTS PROVIDING "QUICK LOOKS".

DEPTH IN FT IS ASSUMED CONSTANT AND VELOCITIES IN FPS ARE CONSIDERED STEADY IN TIME.

VELOCITY PROFILE PARAMETERS FOLLOW...

		FROM TOP TO BOTTOM ON GRID		FROM LEFT TO RIGHT ON GRID	
UPPER:	DEPTH, DU1 = 6.00	X-VELOCITY, UU1 = -0.298	DEPTH, DW1 = 6.00	Z-VELOCITY, WW1 = -0.790E-01	
LOWER:	DEPTH, DU2 = 12.0	X-VELOCITY, UU2 = -0.298	DEPTH, DW2 = 12.0	Z-VELOCITY, WW2 = -0.790E-01	

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

TIME PARAMETERS:

DURATION OF THE DISPOSAL, TREL = 30.00 SECONDS

DURATION OF THE SIMULATION, TSTOP = 14400.00 SECONDS

LONG-TERM TIME STEP USED IN THE SIMULATION, DTL = 1200.00 SECONDS

BARGE DESCRIPTION:

LENGTH OF BARGE, BARGL = 0.20E+03 FT

WIDTH OF BARGE, BARGW = 50. FT

DRAFT OF LOADED BARGE, DREL1 = 12.0 FT

DRAFT OF UNLOADED BARGE, DREL2 = 3.00 FT

MODEL COEFFICIENTS READ FROM INPUT:

TURBULENT THERMAL ENTRAINMENT	ALPHA0 =	0.2350
SETTLING COEFFICIENT	BETA =	0.0000
APPARENT MASS COEFFICIENT	CM =	1.0000
DRAG COEFFICIENT FOR A SPHERE	CD =	0.5000
RATIO--CLOUD/AMBIENT DENSITY GRADIENTS	GAMA =	0.2500
FORM DRAG FOR COLLAPSING CLOUD	CDRAG =	1.0000
SKIN FRICTION FOR COLLAPSING CLOUD	CFRIC =	0.0100
DRAG FOR AN ELLIPSOIDAL WEDGE	CD3 =	0.1000
DRAG FOR A PLATE	CD4 =	1.0000
ENTRAINMENT IN COLLAPSE	ALPHAC =	0.1000
FRICTION BETWEEN CLOUD AND BOTTOM	FRICTN =	0.0100
4/3 LAW HORIZ. DIFF. DISSIPATION FACTOR	ALAMDA =	0.0010
UNSTRATIFIED WATER VERT. DIFF. COEF.	AKY0 =	0.0250
STRIPPING COEF. OF FINES DURING CONVERTIVE DESCENT	=	0.0030

MATERIAL DESCRIPTION: 4 SOLIDS FRACTIONS

L A Y E R 1

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)	FALL VELOCITY (FPS)	DEPOSITIONAL VOID RATIO	CHARACTER
SAND	2.700	0.1850E-01	0.10000	0.6000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.2500E-01 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Silt	2.650	0.1499	0.01000	4.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.8500E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clay	2.650	0.5900E-01	0.00200	7.500	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 0.3800E-02 LBS/SQ. FT. SEDIMENT FRACTION WILL BE STRIPPED DURING CONVECTIVE DESCENT.					
Clumps	1.600	0.2275	3.00000	0.4000	NONCOHESIVE
CRITICAL SHEAR STRESS FOR DEPOSITION = 99.00 LBS/SQ. FT. SEDIMENT FRACTION WILL NOT BE STRIPPED DURING CONVECTIVE DESCENT.					

WATER QUALITY ANALYSIS DATA:

CONCENTRATIONS OF FOLLOWING INITIAL MIXING OF THE FLUID
ARE COMPUTED FOR WATER QUALITY EVALUATIONS.

THE INITIAL CONCENTRATION OF IS 0.000000E+00 MG/L
AND ITS BACKGROUND CONCENTRATION IS 0.000000E+00 MG/L.

THE WATER QUALITY STANDARD FOR IS 0.000000E+00 MG/L.

DESCRIPTION	SPEC. GRAV. OR DENSITY (GM/CC)	VOLUMETRIC CONCENTRATION (VOL/VOL)
FLUID	1.024	0.5451

DISCHARGE PARAMETERS:

VOLUME OF LAYER 1 = 2000. CU YD

DEPTH IS TOO SHALLOW FOR CONVECTIVE DESCENT SO DESCENT IS BYPASSED.

CLOUD COLLAPSE PHASE:

IN TRIAL #1 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.10000000 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 71.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

IN TRIAL #2 THE COLLAPSE PHASE TIME STEP (DT) WAS 0.23333333E-01 SECONDS.
THE TOTAL NUMBER OF INTEGRATION TIME STEPS (ISTEP) FOR CONVECTIVE DESCENT AND COLAPSE WAS 240.
THE INTEGRATION TIME STEP NUMBER WHEN THE BED WAS ENCOUNTERED (IBED) WAS 1.
THE BOTTOM WAS ENCOUNTERED DURING CONVECTIVE DESCENT.
DIFFUSION OF THE DISCHARGE IS GREATER THAN DYNAMIC SPREADING FROM THE COLLAPSE.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56 5050. 1650.	1) = 1 123.3	9.265	0.7970E-01	139.1	0.0000E+00	25	1	
NEW CLOUD CREATED, NTCLD(K) (K = 31.12 5050. 1650.	1) = 2 137.3	9.344	0.5833	2.434	0.0000E+00	49	25	
NEW CLOUD CREATED, NTCLD(K) (K = 31.68 5050. 1650.	1) = 3 151.7	9.928	0.4689	2.182	0.0000E+00	73	49	
NEW CLOUD CREATED, NTCLD(K) (K = 32.24 5051. 1650.	1) = 4 164.4	10.40	0.3420	1.740	0.0000E+00	97	73	
NEW CLOUD CREATED, NTCLD(K) (K = 32.80 5051. 1650.	1) = 5 175.1	10.74	0.2464	1.341	0.0000E+00	121	97	
NEW CLOUD CREATED, NTCLD(K) (K = 33.36 5051. 1650.	1) = 6 183.9	10.98	0.1826	1.047	0.0000E+00	145	121	
NEW CLOUD CREATED, NTCLD(K) (K = 33.92 5051. 1650.	1) = 7 191.3	11.17	0.1410	0.8418	0.0000E+00	169	145	
NEW CLOUD CREATED, NTCLD(K) (K = 34.48 5051. 1650.	1) = 8 197.6	11.31	0.1135	0.7001	0.0000E+00	193	169	
NEW CLOUD CREATED, NTCLD(K) (K = 35.04 5051. 1650.	1) = 9 203.3	11.42	0.9478E-01	0.6011	0.0000E+00	217	193	
NEW CLOUD CREATED, NTCLD(K) (K = 35.58 5051. 1650.	1) = 10 208.2	10.18	3.317	849.0	0.0000E+00	240	217	

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050.	1650.	2) = 1 123.3	9.265	0.7970E-01	1127.	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050.	1650.	2) = 2 137.3	9.344	0.5833	19.72	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050.	1650.	2) = 3 151.7	9.928	0.4689	17.68	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051.	1650.	2) = 4 164.4	10.40	0.3420	14.10	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051.	1650.	2) = 5 175.1	10.74	0.2464	10.87	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051.	1650.	2) = 6 183.9	10.98	0.1826	8.482	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051.	1650.	2) = 7 191.3	11.17	0.1410	6.821	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051.	1650.	2) = 8 197.6	11.31	0.1135	5.672	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051.	1650.	2) = 9 203.3	11.42	0.9478E-01	4.870	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051.	1650.	2) = 10 208.2	10.18	3.317	6880.	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION Z-LOCATION (FT) (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1650.	3) = 123.3	9.265	0.7970E-01	443.5	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050. 1650.	3) = 137.3	9.344	0.5833	7.763	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050. 1650.	3) = 151.7	9.928	0.4689	6.958	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051. 1650.	3) = 164.4	10.40	0.3420	5.549	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051. 1650.	3) = 175.1	10.74	0.2464	4.278	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051. 1650.	3) = 183.9	10.98	0.1826	3.338	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051. 1650.	3) = 191.3	11.17	0.1410	2.685	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051. 1650.	3) = 197.6	11.31	0.1135	2.233	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051. 1650.	3) = 203.3	11.42	0.9478E-01	1.916	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051. 1650.	3) = 208.2	10.18	3.317	2708.	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT) Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (CU FT)	ENTRAINED MASS (CU FT)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 30.56	5050. 1650.	4) = 1 123.3	13.50	0.1000E-02	4039.	0.0000E+00	25	1
NEW CLOUD CREATED, NTCLD(K) (K = 31.12	5050. 1650.	4) = 2 137.3	13.50	0.1000E-02	3156.	0.0000E+00	49	25
NEW CLOUD CREATED, NTCLD(K) (K = 31.68	5050. 1650.	4) = 3 151.7	13.50	0.1000E-02	2115.	0.0000E+00	73	49
NEW CLOUD CREATED, NTCLD(K) (K = 32.24	5051. 1650.	4) = 4 164.4	13.50	0.1000E-02	1322.	0.0000E+00	97	73
NEW CLOUD CREATED, NTCLD(K) (K = 32.80	5051. 1650.	4) = 5 175.1	13.50	0.1000E-02	773.2	0.0000E+00	121	97
NEW CLOUD CREATED, NTCLD(K) (K = 33.36	5051. 1650.	4) = 6 183.9	13.50	0.1000E-02	427.8	0.0000E+00	145	121
NEW CLOUD CREATED, NTCLD(K) (K = 33.92	5051. 1650.	4) = 7 191.3	13.50	0.1000E-02	226.5	0.0000E+00	169	145
NEW CLOUD CREATED, NTCLD(K) (K = 34.48	5051. 1650.	4) = 8 197.6	13.50	0.1000E-02	115.7	0.0000E+00	193	169
NEW CLOUD CREATED, NTCLD(K) (K = 35.04	5051. 1650.	4) = 9 203.3	13.50	0.1000E-02	57.42	0.0000E+00	217	193
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051. 1650.	4) = 10 208.2	10.18	3.317	52.06	0.0000E+00	240	217

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

TIME FROM DISPOSAL (SEC)	CLOUD CENTROID X-LOCATION (FT)	Z-LOCATION (FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	T O T A L M A S S (M G)	ENTRAINED MASS (M G)	TIME STEP WHEN THIS CLOUD WAS CREATED	TIME STEP WHEN PREVIOUS CLOUD WAS CREATED
NEW CLOUD CREATED, NTCLD(K) (K = 35.58	5051.	1650.	5) = 1 208.2	10.18	3.317	0.0000E+00	0.0000E+00	240	1

NOTE -- When all solid material has settled from a cloud, the cloud is erased and the remaining clouds for this solids type are renumbered.

LONG TERM DIFFUSION RESULTS:

BEGIN LONG TERM SIMULATION OF FATE OF SAND

SUMMARY OF SAND DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 999.00

COMPUTATIONS FOR SAND TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Silt

SUMMARY OF Silt DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 145.95

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 7948.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 57.645

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8036.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 23.510

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8071.1

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	3986.	1368.	1.702	0.0000E+00	435.0	0.0000E+00	13.50	0.100000E-01
2	3987.	1368.	1.265	0.0000E+00	457.3	0.0000E+00	13.50	0.100000E-01
3	3987.	1368.	1.066	0.0000E+00	479.7	0.0000E+00	13.50	0.100000E-01
4	3987.	1368.	0.8389	0.0000E+00	499.2	0.0000E+00	13.50	0.100000E-01
5	3988.	1368.	0.6411	0.0000E+00	515.2	0.0000E+00	13.50	0.100000E-01
6	3988.	1368.	0.5005	0.0000E+00	528.3	0.0000E+00	13.50	0.100000E-01
7	3988.	1368.	0.4009	0.0000E+00	539.1	0.0000E+00	13.50	0.100000E-01
8	3988.	1368.	0.3391	0.0000E+00	548.4	0.0000E+00	13.50	0.100000E-01
9	3989.	1368.	0.2881	0.0000E+00	556.6	0.0000E+00	13.50	0.100000E-01
10	3989.	1368.	16.47	0.0000E+00	563.6	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 9.5882
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8085.0

SUMMARY OF Silt DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 3.9104
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8090.7

SUMMARY OF Silt DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1.5948
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.0

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2913. 1084.	0.1155	0.0000E+00	874.5	0.0000E+00	13.50	0.100000E-01
2	2914. 1084.	0.8585E-01	0.0000E+00	903.1	0.0000E+00	13.50	0.100000E-01
3	2914. 1084.	0.7230E-01	0.0000E+00	931.6	0.0000E+00	13.50	0.100000E-01
4	2915. 1084.	0.5691E-01	0.0000E+00	956.3	0.0000E+00	13.50	0.100000E-01
5	2915. 1084.	0.4349E-01	0.0000E+00	976.5	0.0000E+00	13.50	0.100000E-01
6	2915. 1084.	0.3395E-01	0.0000E+00	992.9	0.0000E+00	13.50	0.100000E-01
7	2915. 1084.	0.2719E-01	0.0000E+00	1006.	0.0000E+00	13.50	0.100000E-01
8	2916. 1084.	0.2301E-01	0.0000E+00	1018.	0.0000E+00	13.50	0.100000E-01
9	2916. 1084.	0.1954E-01	0.0000E+00	1028.	0.0000E+00	13.50	0.100000E-01
10	2916. 1084.	1.117	0.0000E+00	1037.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.65043
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8093.9

SUMMARY OF Silt DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.26527
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.3

SUMMARY OF Silt DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.10819
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1841. 799.2	0.7833E-02	0.0000E+00	1413.	0.0000E+00	13.50	0.100000E-01
2	1841. 799.3	0.5823E-02	0.0000E+00	1447.	0.0000E+00	13.50	0.100000E-01
3	1842. 799.3	0.4905E-02	0.0000E+00	1481.	0.0000E+00	13.50	0.100000E-01
4	1842. 799.3	0.3860E-02	0.0000E+00	1510.	0.0000E+00	13.50	0.100000E-01
5	1842. 799.3	0.2950E-02	0.0000E+00	1533.	0.0000E+00	13.50	0.100000E-01
6	1842. 799.4	0.2303E-02	0.0000E+00	1552.	0.0000E+00	13.50	0.100000E-01
7	1843. 799.4	0.1845E-02	0.0000E+00	1568.	0.0000E+00	13.50	0.100000E-01
8	1843. 799.5	0.1561E-02	0.0000E+00	1582.	0.0000E+00	13.50	0.100000E-01
9	1843. 799.5	0.1326E-02	0.0000E+00	1594.	0.0000E+00	13.50	0.100000E-01
10	1843. 799.5	0.7578E-01	0.0000E+00	1604.	0.0000E+00	13.50	0.100000E-01

SUMMARY OF Silt DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.44123E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.5

SUMMARY OF Silt DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.17995E-01
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6

SUMMARY OF Silt DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.73390E-02
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 8094.6
MAX CONC IS 0.00000000 OUTPUT SUPPRESSED AT 0.00 FT

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Silt

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	767.9	514.8	0.5314E-03	0.0000E+00	2036.	0.0000E+00	13.50	0.100000E-01
2	768.3	514.9	0.3950E-03	0.0000E+00	2074.	0.0000E+00	13.50	0.100000E-01
3	768.7	514.9	0.3327E-03	0.0000E+00	2112.	0.0000E+00	13.50	0.100000E-01
4	769.1	514.9	0.2619E-03	0.0000E+00	2145.	0.0000E+00	13.50	0.100000E-01
5	769.4	514.9	0.2001E-03	0.0000E+00	2172.	0.0000E+00	13.50	0.100000E-01
6	769.6	515.0	0.1562E-03	0.0000E+00	2193.	0.0000E+00	13.50	0.100000E-01
7	769.8	515.0	0.1251E-03	0.0000E+00	2211.	0.0000E+00	13.50	0.100000E-01
8	770.1	515.1	0.1059E-03	0.0000E+00	2226.	0.0000E+00	13.50	0.100000E-01
9	770.2	515.1	0.8992E-04	0.0000E+00	2240.	0.0000E+00	13.50	0.100000E-01
10	770.4	515.1	0.5141E-02	0.0000E+00	2251.	0.0000E+00	13.50	0.100000E-01

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BEGIN LONG TERM SIMULATION OF FATE OF Clay

SUMMARY OF Clay DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 1356.0

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 1830.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 2400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 571.77

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2614.2

SUMMARY OF Clay DISTRIBUTIONS AFTER 3600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 434.54

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2751.5

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SMALL CLOUDS AT 3600.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)	
1	4026.	1379.	115.5	0.0000E+00	435.0	0.0000E+00	13.50	0.200000E-02
2	3987.	1368.	4.571	0.0000E+00	457.3	0.0000E+00	13.50	0.200000E-02
3	3987.	1368.	4.091	0.0000E+00	479.7	0.0000E+00	13.50	0.200000E-02
4	3987.	1368.	3.257	0.0000E+00	499.2	0.0000E+00	13.50	0.200000E-02
5	3988.	1368.	2.484	0.0000E+00	515.2	0.0000E+00	13.50	0.200000E-02
6	3988.	1368.	1.935	0.0000E+00	528.3	0.0000E+00	13.50	0.200000E-02
7	3988.	1368.	1.535	0.0000E+00	539.1	0.0000E+00	13.50	0.200000E-02
8	3988.	1368.	1.292	0.0000E+00	548.4	0.0000E+00	13.50	0.200000E-02
9	3989.	1368.	1.107	0.0000E+00	556.6	0.0000E+00	13.50	0.200000E-02
10	4115.	1402.	298.7	0.0000E+00	563.6	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 4800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 363.65
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2822.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 6000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 304.33
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2881.7

SUMMARY OF Clay DISTRIBUTIONS AFTER 7200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 254.68
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2931.3

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SMALL CLOUDS AT 7200.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID	MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	2953. 1094.	67.71	0.0000E+00	874.5	0.0000E+00	13.50	0.200000E-02
2	2914. 1084.	2.679	0.0000E+00	903.1	0.0000E+00	13.50	0.200000E-02
3	2914. 1084.	2.398	0.0000E+00	931.6	0.0000E+00	13.50	0.200000E-02
4	2915. 1084.	1.909	0.0000E+00	956.3	0.0000E+00	13.50	0.200000E-02
5	2915. 1084.	1.456	0.0000E+00	976.5	0.0000E+00	13.50	0.200000E-02
6	2915. 1084.	1.134	0.0000E+00	992.9	0.0000E+00	13.50	0.200000E-02
7	2915. 1084.	0.8999	0.0000E+00	1006.	0.0000E+00	13.50	0.200000E-02
8	2916. 1084.	0.7573	0.0000E+00	1018.	0.0000E+00	13.50	0.200000E-02
9	2916. 1084.	0.6490	0.0000E+00	1028.	0.0000E+00	13.50	0.200000E-02
10	3042. 1117.	175.1	0.0000E+00	1037.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 8400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 213.13
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 2972.8

SUMMARY OF Clay DISTRIBUTIONS AFTER 9600.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 178.36
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3007.3

SUMMARY OF Clay DISTRIBUTIONS AFTER 10800.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 149.27
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3035.9

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SMALL CLOUDS AT 10800.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	1880.	809.7	39.68	0.0000E+00	1413.	0.0000E+00	13.50	0.200000E-02
2	1841.	799.3	1.570	0.0000E+00	1447.	0.0000E+00	13.50	0.200000E-02
3	1842.	799.3	1.405	0.0000E+00	1481.	0.0000E+00	13.50	0.200000E-02
4	1842.	799.3	1.119	0.0000E+00	1510.	0.0000E+00	13.50	0.200000E-02
5	1842.	799.3	0.8532	0.0000E+00	1533.	0.0000E+00	13.50	0.200000E-02
6	1842.	799.4	0.6647	0.0000E+00	1552.	0.0000E+00	13.50	0.200000E-02
7	1843.	799.4	0.5274	0.0000E+00	1568.	0.0000E+00	13.50	0.200000E-02
8	1843.	799.5	0.4438	0.0000E+00	1582.	0.0000E+00	13.50	0.200000E-02
9	1843.	799.5	0.3804	0.0000E+00	1594.	0.0000E+00	13.50	0.200000E-02
10	1970.	833.0	102.6	0.0000E+00	1604.	0.0000E+00	13.50	0.200000E-02

SUMMARY OF Clay DISTRIBUTIONS AFTER 12000.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 124.92
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3059.6

SUMMARY OF Clay DISTRIBUTIONS AFTER 13200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 104.54
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3079.1

SUMMARY OF Clay DISTRIBUTIONS AFTER 14400.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 87.483
TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 3095.0

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SMALL CLOUDS AT 14400.00 SECONDS ELAPSED TIME FOR Clay

CLOUD #	LOCATION OF CLOUD CENTROID DISTANCE FROM TOP OF GRID LEFT OF GRID		MASS FROM DISPOSAL (CU FT)	ENTRAINED MASS (CU FT)	CLOUD X-Z DIAMETER (FT)	DEPTH OF TOP OF CLOUD (FT)	CLOUD VERT. THICKNESS (FT)	SOLIDS FALL VELOCITY (FPS)
1	807.6	525.3	23.26	0.0000E+00	2036.	0.0000E+00	13.50	0.200000E-02
2	768.3	514.9	0.9202	0.0000E+00	2074.	0.0000E+00	13.50	0.200000E-02
3	768.7	514.9	0.8236	0.0000E+00	2112.	0.0000E+00	13.50	0.200000E-02
4	769.1	514.9	0.6558	0.0000E+00	2145.	0.0000E+00	13.50	0.200000E-02
5	769.4	514.9	0.5001	0.0000E+00	2172.	0.0000E+00	13.50	0.200000E-02
6	769.6	515.0	0.3896	0.0000E+00	2193.	0.0000E+00	13.50	0.200000E-02
7	769.8	515.0	0.3091	0.0000E+00	2211.	0.0000E+00	13.50	0.200000E-02
8	770.1	515.1	0.2601	0.0000E+00	2226.	0.0000E+00	13.50	0.200000E-02
9	770.2	515.1	0.2229	0.0000E+00	2240.	0.0000E+00	13.50	0.200000E-02
10	896.8	548.6	60.14	0.0000E+00	2251.	0.0000E+00	13.50	0.200000E-02

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THICKNESS (FT) OF Clay ACCUMULATED ON BOTTOM, 14400.00 SECONDS AFTER DUMP
...MULTIPLY DISPLAYED VALUES BY 1.000 (LEGEND... + = .LT. .01 . = .LT. .0001 0 = .LT. .000001)

M N=	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
2 0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3 0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
4 0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
5 0000	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
6 0000	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
7 0000	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
8 0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
9 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.	.
10 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
11 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
12 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.	.
13 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
14 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.	.
15 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
16 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
17 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
18 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
19 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
20 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
21 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
22 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
23 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
24 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
25 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
26 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
27 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
28 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
29 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
30 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
31 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
32 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
33 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
34 0000	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
35 0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
36 0000	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
37 0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
38 0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
39 0000	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
40 0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
41 0000	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	.
42 0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
43 0000	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
44 0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
45 0000	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
46 0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	.	0
47 0000	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	.	0	0
48 0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
49 0000	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
50 0000	0	.	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
51 0000	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
52 0000	0	0	0	.	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	.	0	0	0
53 0000	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
54 0000	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
55 0000	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
56 0000	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
57 0000	0	0	0	0	0	0	0	.	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
58 0000	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0
59 0000	0	0	0	0	0	0	0	0	0	.	.	.	.	+	+	+	+	+	.	.	.	.	.	.	.	.	0	0	0	0

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
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3	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
6	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
9	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
11	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
12	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
13	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
14	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
16	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
18	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
19	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
21	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
22	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
23	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
24	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25	.	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
26	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
27	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
28	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
29	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	.	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	.	0	0	0														

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF Clumps

SUMMARY OF Clumps DISTRIBUTIONS AFTER 1200.00 SEC.

TOTAL SUSPENDED MATERIAL (CU FT) = 0.00000E+00

TOTAL MATERIAL SETTLED TO BOTTOM (CU FT) = 12285.

COMPUTATIONS FOR Clumps TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

[illegible]

BEGIN LONG TERM SIMULATION OF FATE OF

SUMMARY OF DISTRIBUTIONS AFTER 1200.00 SEC

TOTAL TRACER OR CONTAMINANT IN SOLUTION (MG) = 0.00000E+00

COMPUTATIONS FOR TERMINATED AT 1200.00 SEC. ELAPSED TIME...MATERIAL SETTLED TO BOTTOM

FINAL DISTRIBUTIONS OF TOTAL SETTLED MATERIAL FOLLOW.....

```
(LEGEND... + = .LT. .01      . = .LT. .0001      0 = .LT. .000001)
```

[illegible]

[illegible]

M	N=	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48
2		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
3	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
4	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	0	00000
5	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
6	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
7	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
8	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
9	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	0	00000
10	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
11	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
12	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
13	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
14	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
15	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
16	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
17	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
18	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
19	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
20	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
21	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
22	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
23	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
24	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
25	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
26	+	+	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
27	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
28	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
29	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
30	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
31	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
32	+	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
33	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
34	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
35	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
36	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
37	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
38	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
39	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
40	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
41	.	.	.	.	.	.	.	.	.	.	.	.	.	0	0	0	0	00000
42																		

[illegible]

M N= 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31

[illegible]

[illegible]

SUMMARY OF CONCENTRATIONS FOR SAND

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR Silt

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.138E+02	3975.	1350.
2.00	0.0	0.267E+00	2925.	1050.
3.00	0.0	0.746E-02	1875.	825.
4.00	0.0	0.255E-03	750.	525.

SUMMARY OF CONCENTRATIONS FOR Clay

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.251E+03	4050.	1425.
2.00	0.0	0.440E+02	3000.	1125.
3.00	0.0	0.106E+02	1950.	825.
4.00	0.0	0.310E+01	825.	525.

SUMMARY OF CONCENTRATIONS FOR Clumps

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
1.00	0.0	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.	0.

SUMMARY OF CONCENTRATIONS FOR

TIME (HR)	DEPTH (FT)	MAX CONC ABOVE BACKGROUND ON ENTIRE GRID (MG/L)	MAX CONC ON GRID (MG/L)	X-LOC (FT)	Z-LOC (FT)
0.33	0.0	0.000E+00	0.000E+00	0.	0.
0.67	0.0	0.000E+00	0.000E+00	0.	0.
1.00	0.0	0.000E+00	0.000E+00	0.	0.
1.33	0.0	0.000E+00	0.000E+00	0.	0.
1.67	0.0	0.000E+00	0.000E+00	0.	0.
2.00	0.0	0.000E+00	0.000E+00	0.	0.
2.33	0.0	0.000E+00	0.000E+00	0.	0.
2.67	0.0	0.000E+00	0.000E+00	0.	0.
3.00	0.0	0.000E+00	0.000E+00	0.	0.
3.33	0.0	0.000E+00	0.000E+00	0.	0.
3.67	0.0	0.000E+00	0.000E+00	0.	0.
4.00	0.0	0.000E+00	0.000E+00	0.	0.

ESTIMATES OF AREAS CURRENTLY IN VIOLATION (SNAPSHOT) AND MIXING ZONES (ACCUMULATED AREA OF VIOLATION)

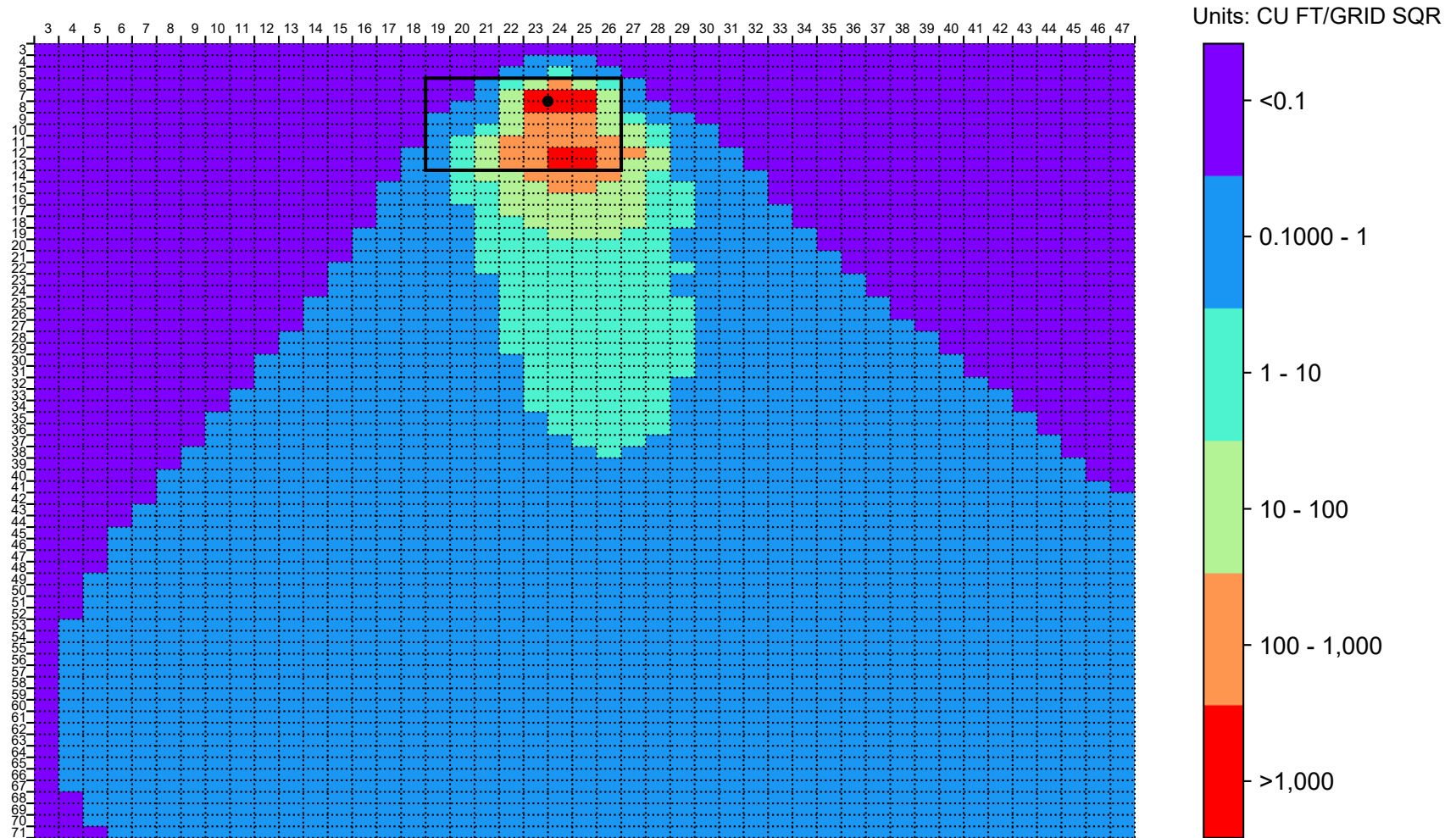
```
UAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAA
3      TIME          SNAPSHOT          ACCUMULATED          3
3      ( SEC )      AREA(SQ FT)  L(FT)    W(FT)    AREA(SQ FT)  L(FT)    W(FT)    3
3
3
3
AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAU
```

*** RUN COMPLETED ***

Attachment G-2

Results Figures Per Scenario

- disposal point
- CAD Cell Boundary



Total Accumulated Material on STFATE model grid (cu/yd) = 1082.40
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1084.00
 Total Lost (cu/yd) = 1.60
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 457.99

Total Accumulated Material WITHIN Boundary (cu/yd) = 947.84
 Total Lost (cu/yd) = 136.16
 Percent Material Outside Boundary (%) = 12.60
 f value = 0.542

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point A at [7,23]. Results are adjusted to include multiplier.
 Source: LNBCAD_AENP_1C.duo



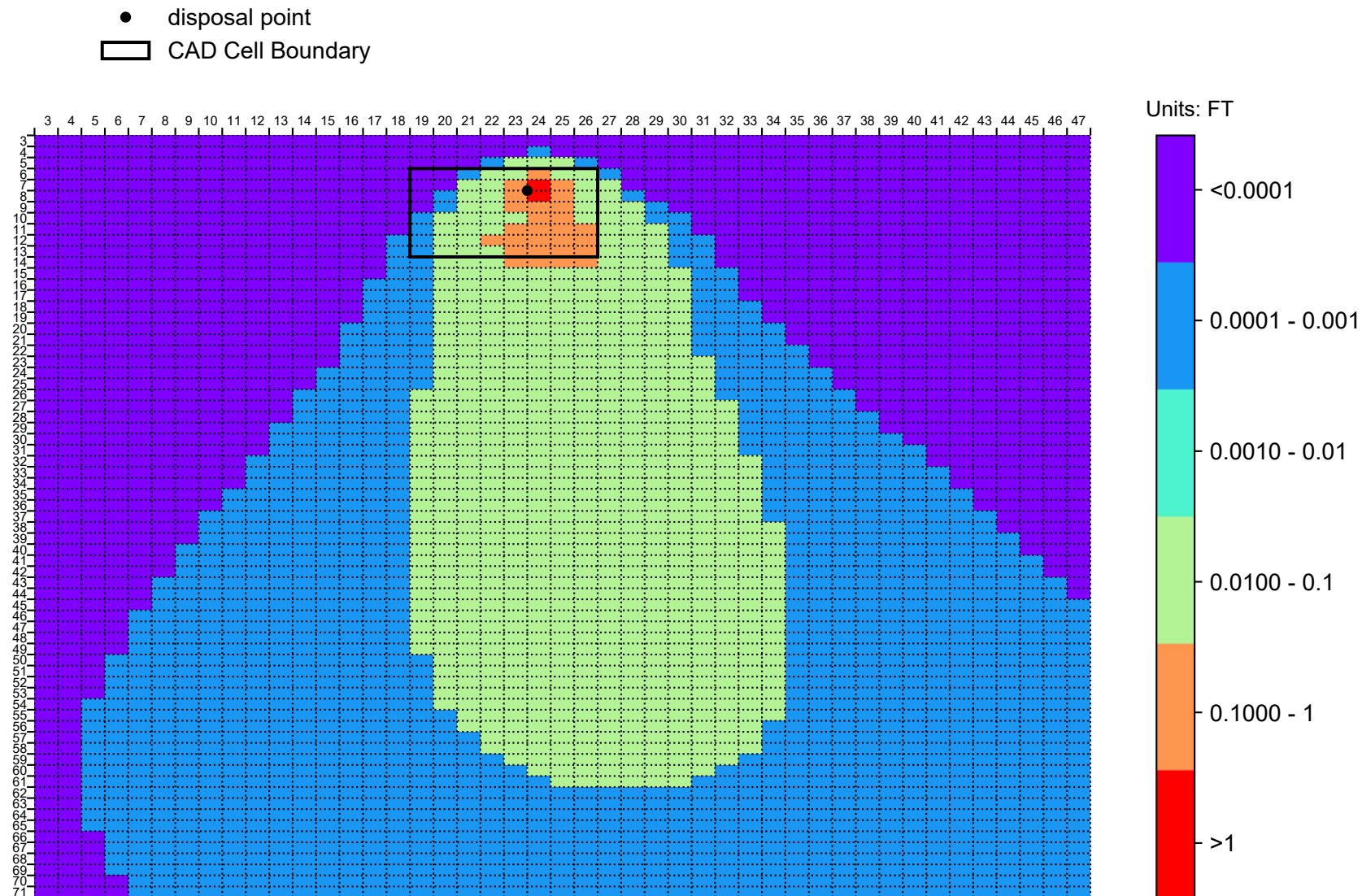


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_1C.duo

- disposal point
- CAD Cell Boundary

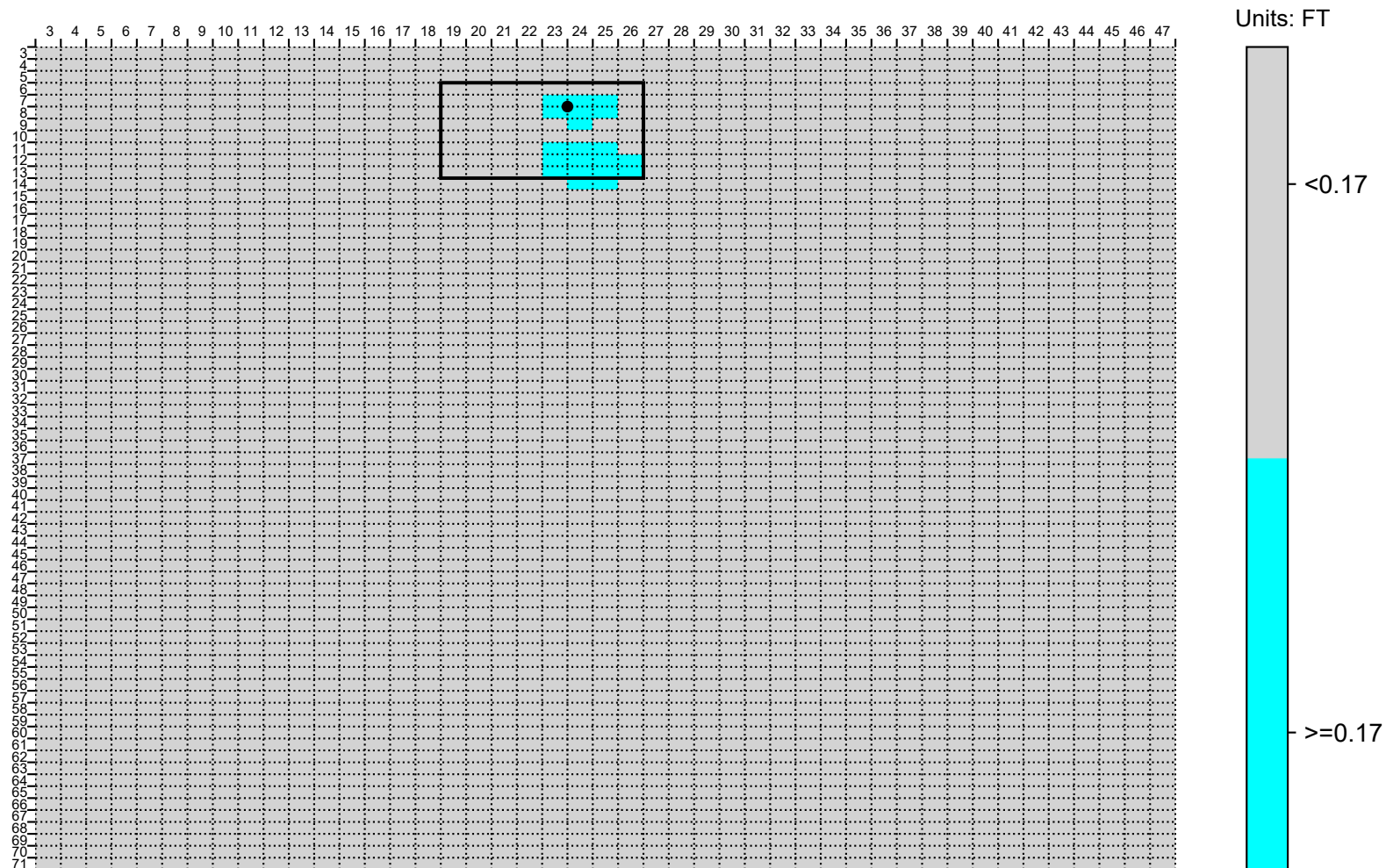
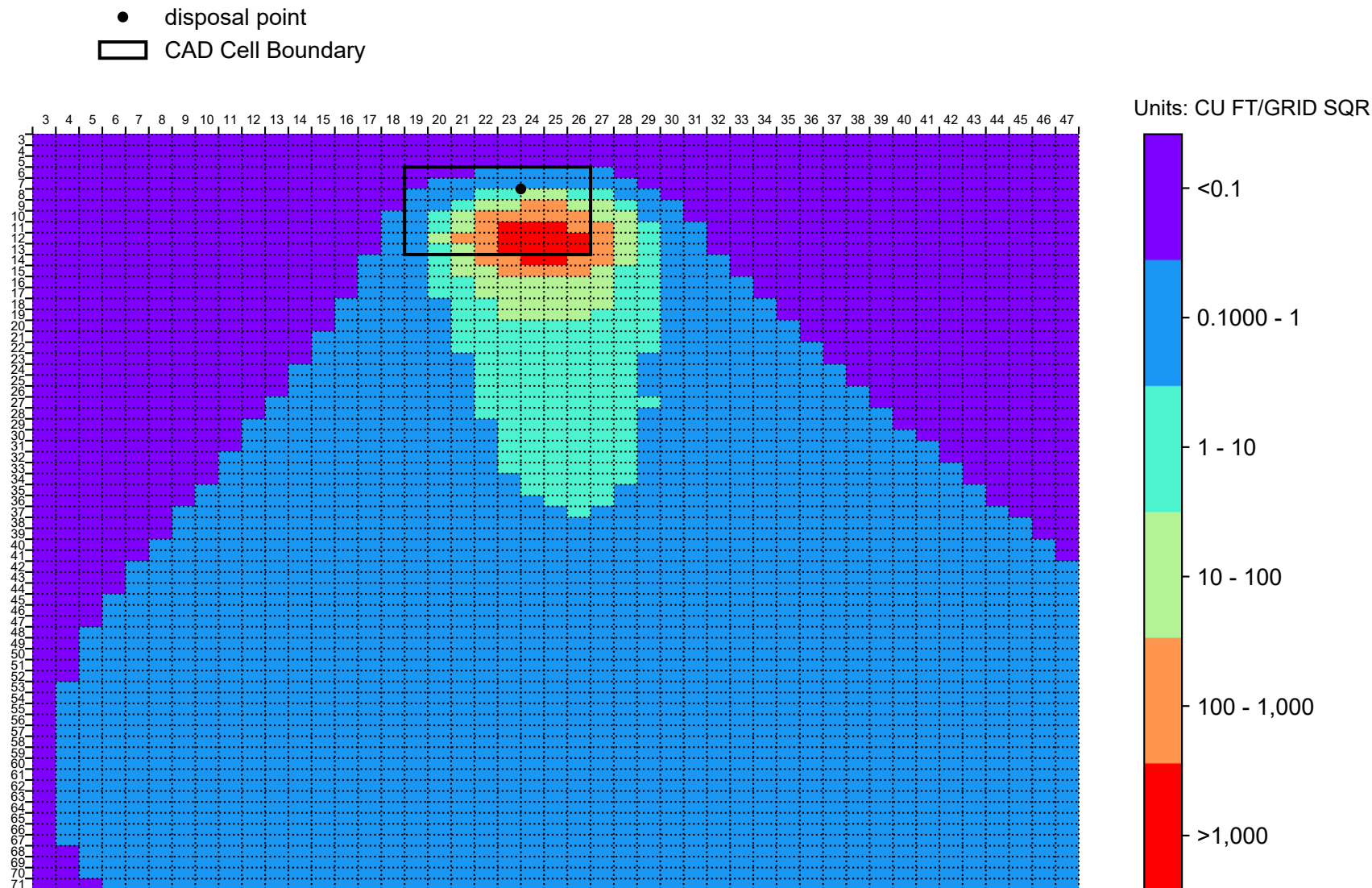


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_1C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1431.21
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1434.00
 Total Lost (cu/yd) = 2.79
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 190.36

Total Accumulated Material WITHIN Boundary (cu/yd) = 1131.79
 Total Lost (cu/yd) = 302.21
 Percent Material Outside Boundary (%) = 21.10
 f value = 0.717

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point A at [7,23]. Results are adjusted to include multiplier.
 Source: LNBCAD_AENP_2.duo



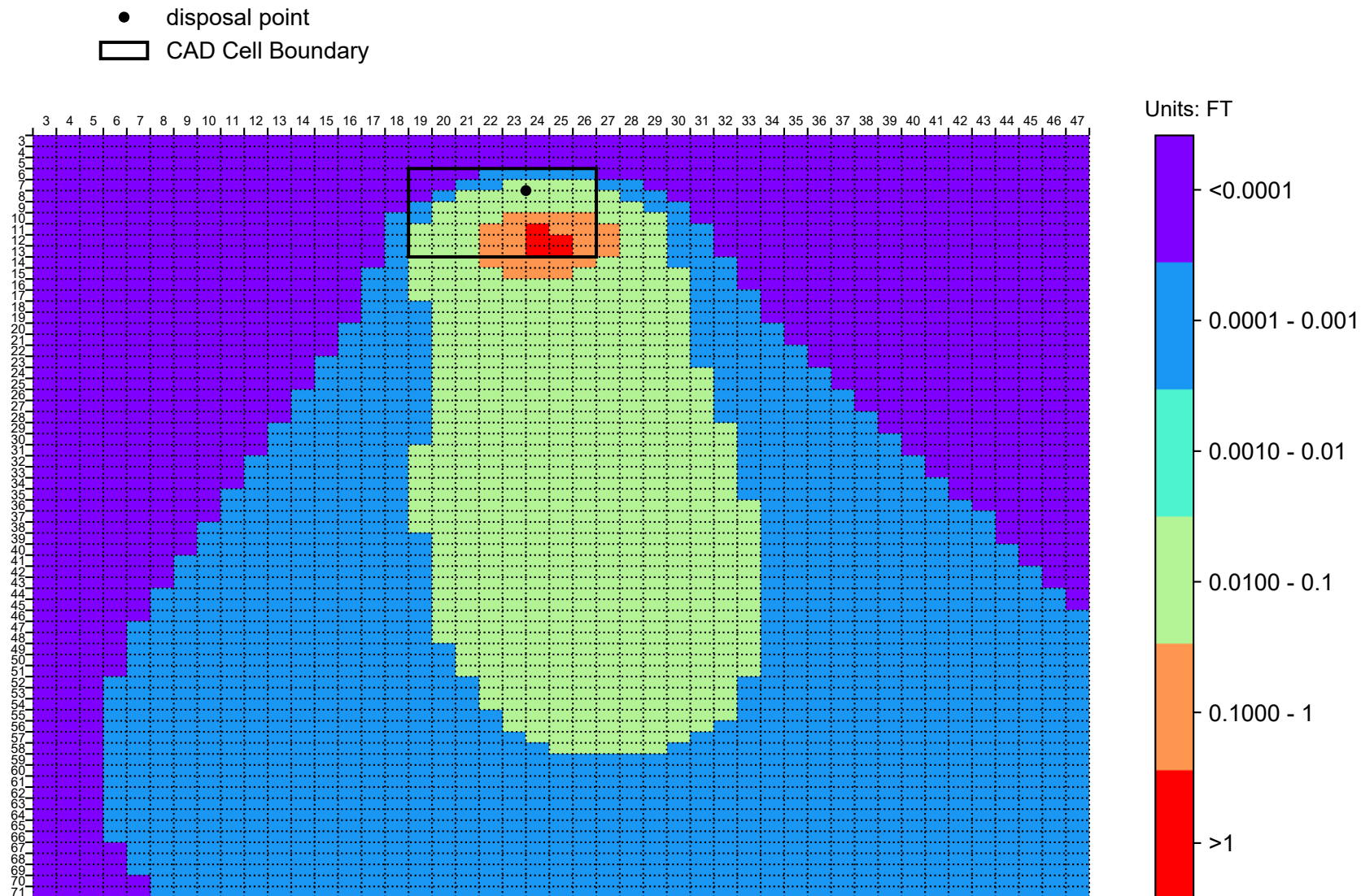


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_2.duo

- disposal point
- CAD Cell Boundary

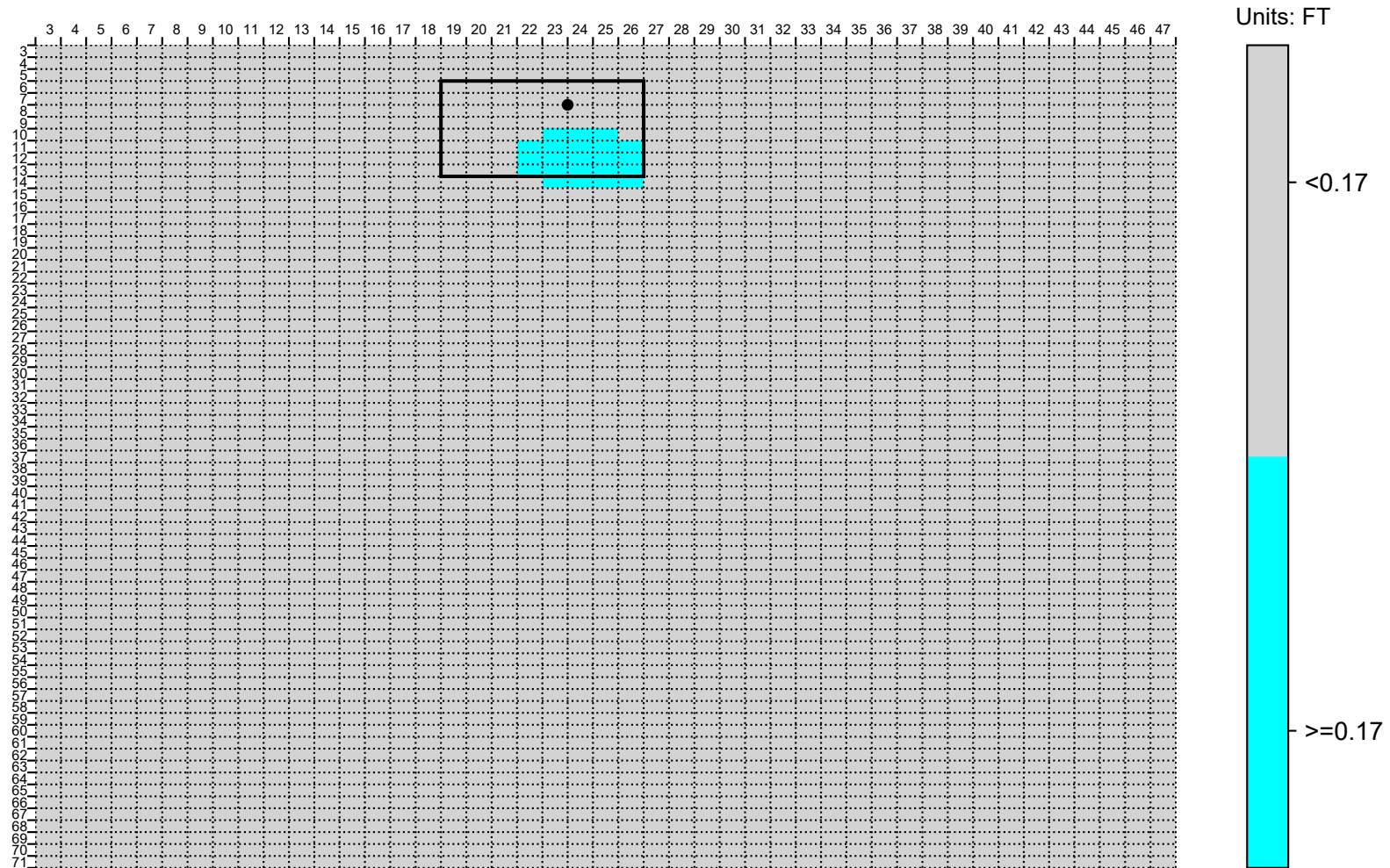
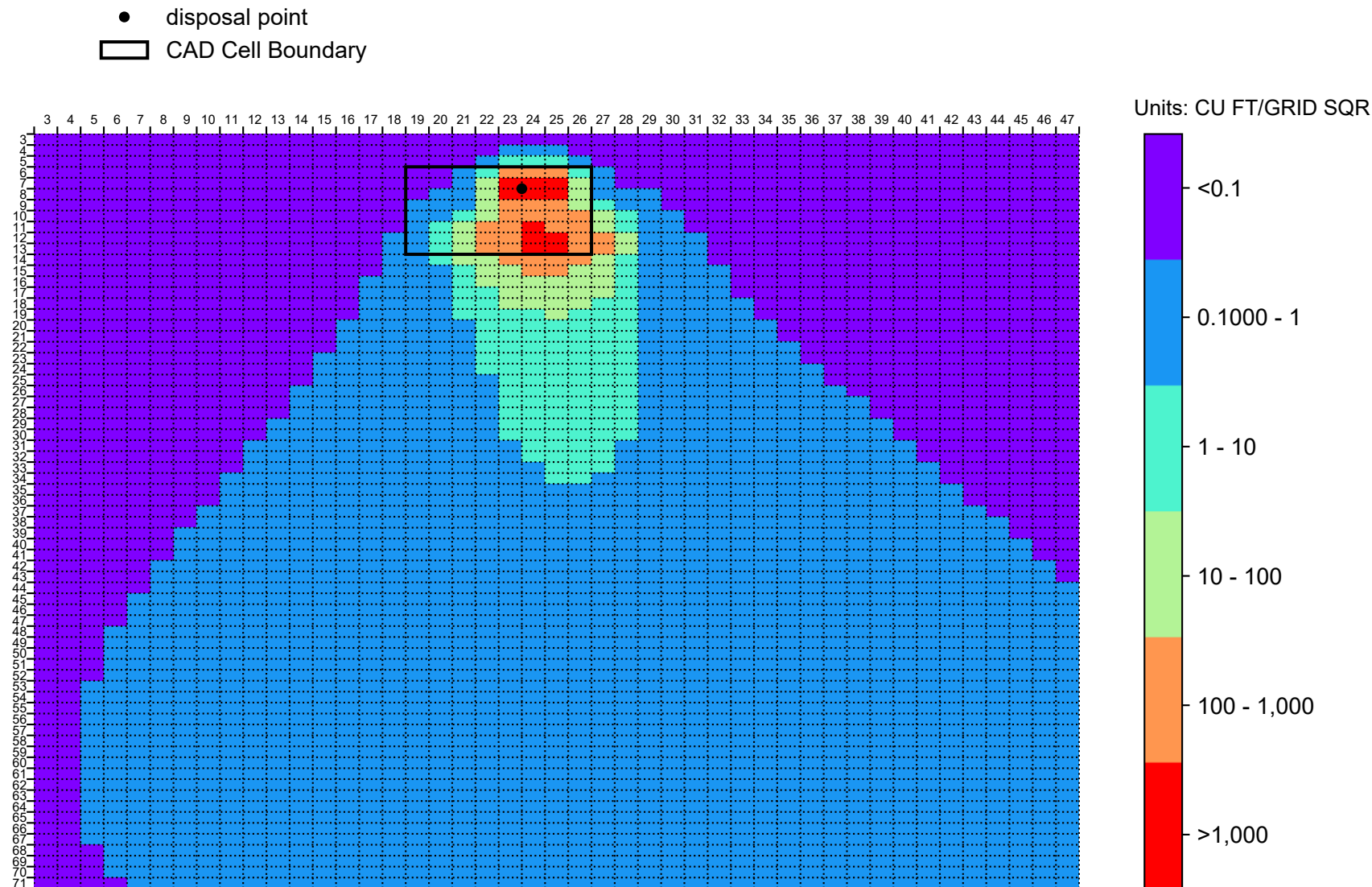


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_2.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1314.25
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1316.00
 Total Lost (cu/yd) = 1.75
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 583.09

Total Accumulated Material WITHIN Boundary (cu/yd) = 1180.16
 Total Lost (cu/yd) = 135.84
 Percent Material Outside Boundary (%) = 10.30
 f value = 0.658

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point A at [7,23]. Results are adjusted to include multiplier.
 Source: LNBCAD_AENP_3C.duo



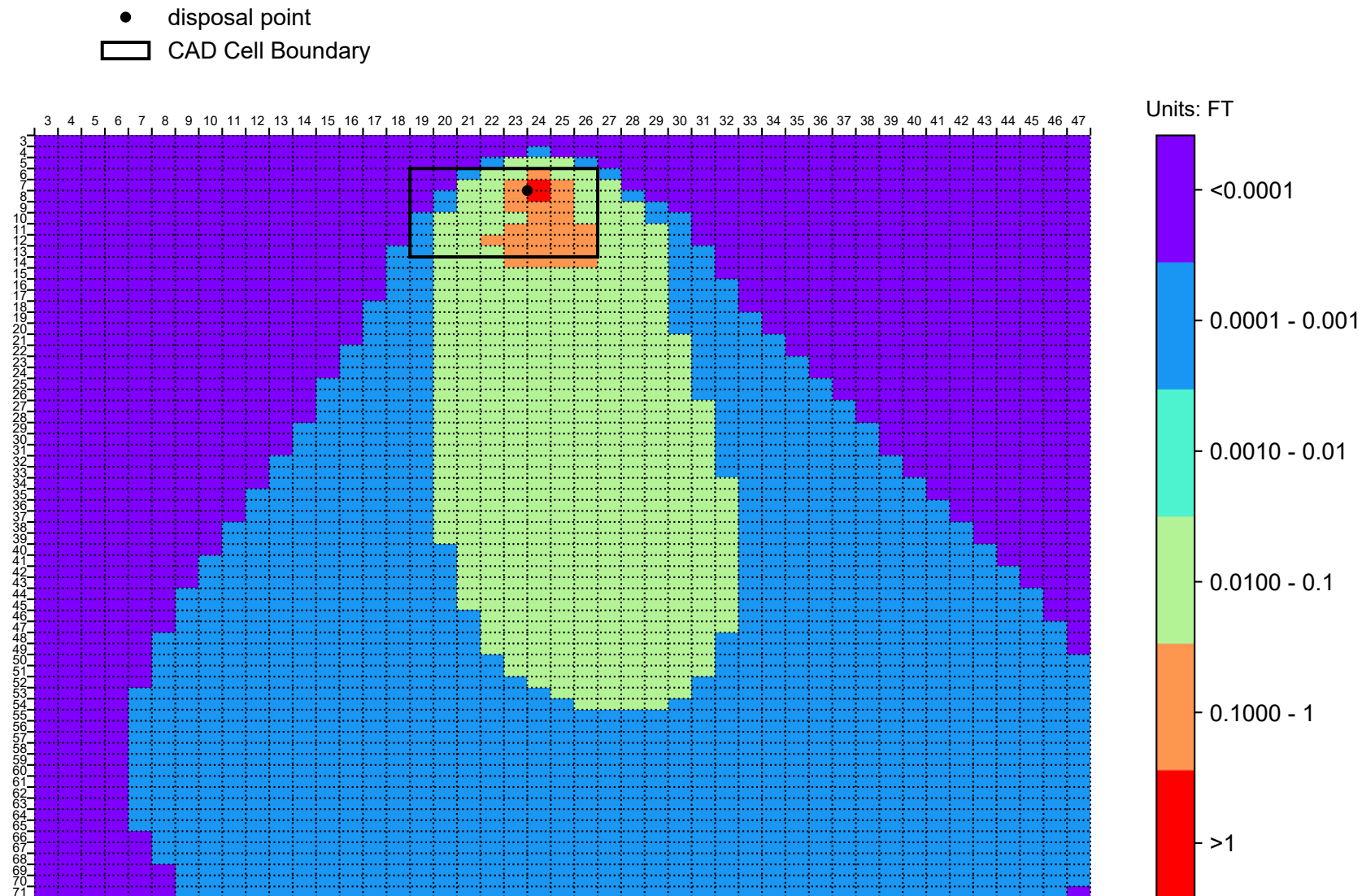


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_3C.duo

- disposal point
- CAD Cell Boundary

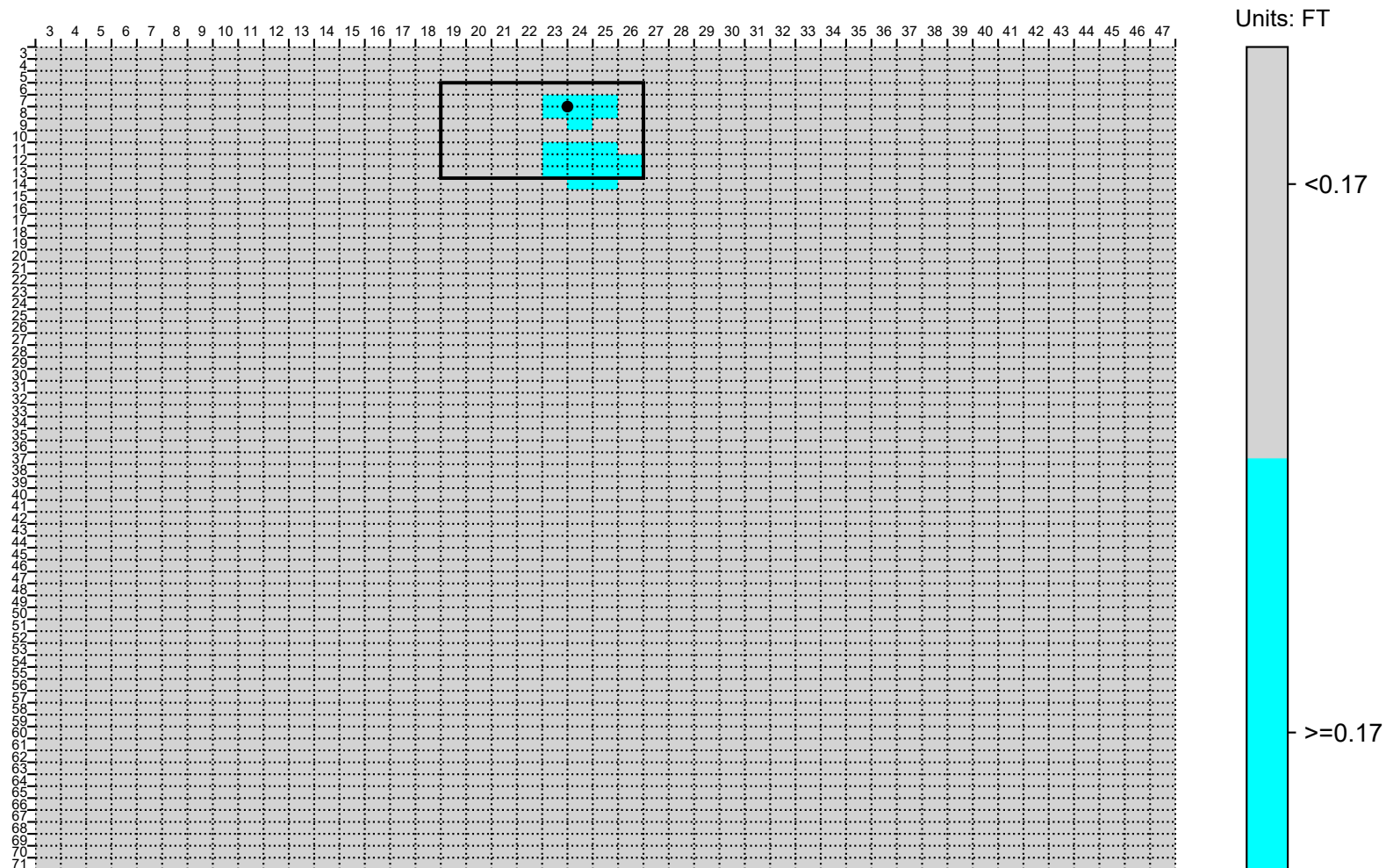
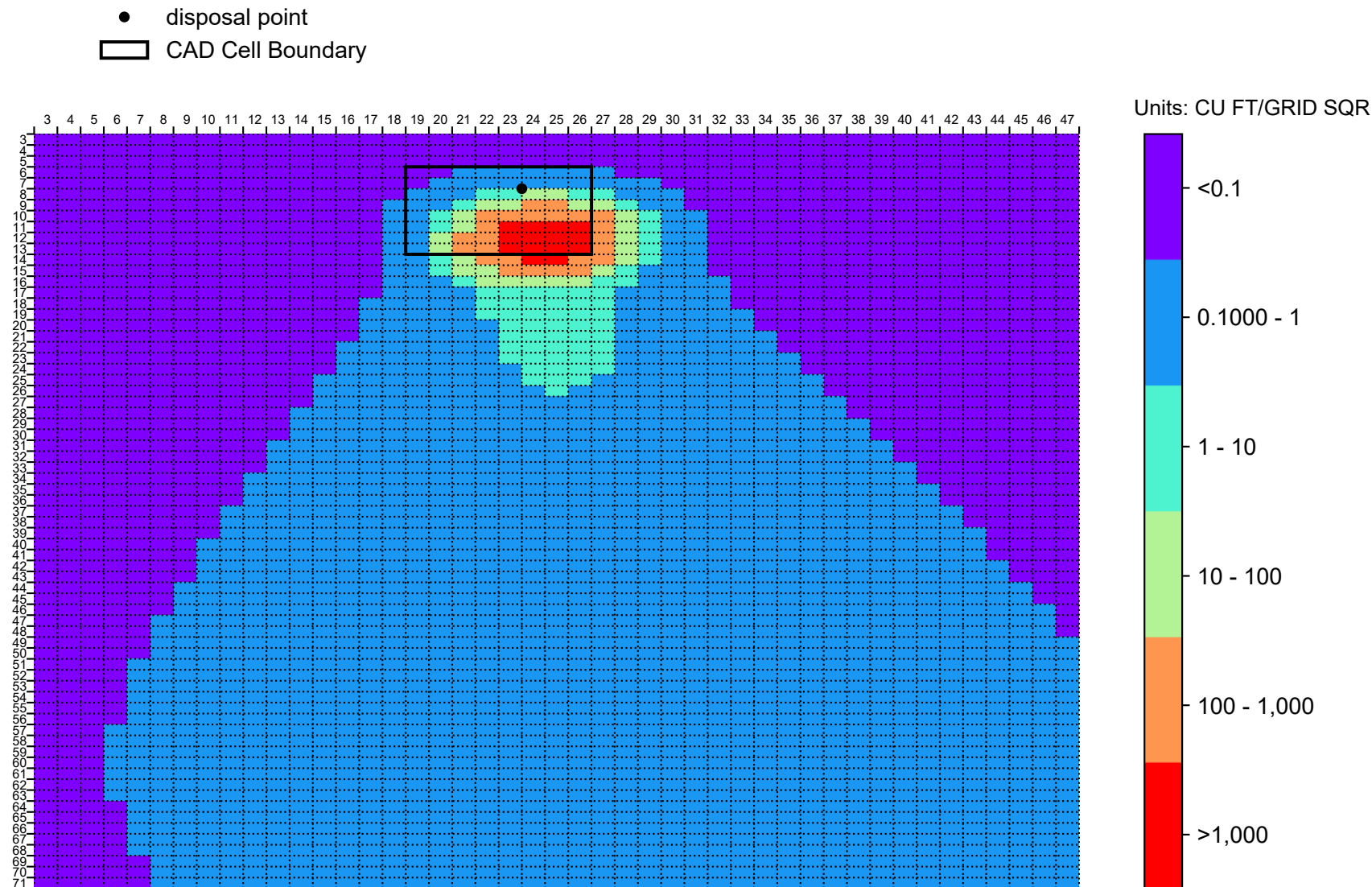


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_3C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1648.63
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1648.00
 Total Lost (cu/yd) = 0.00
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 229.48

Total Accumulated Material WITHIN Boundary (cu/yd) = 1328.30
 Total Lost (cu/yd) = 319.70
 Percent Material Outside Boundary (%) = 19.40
 f value = 0.824

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point A at [7,23]. Results are adjusted to include multiplier.
 Source: LNBCAD_AENP_4.duo



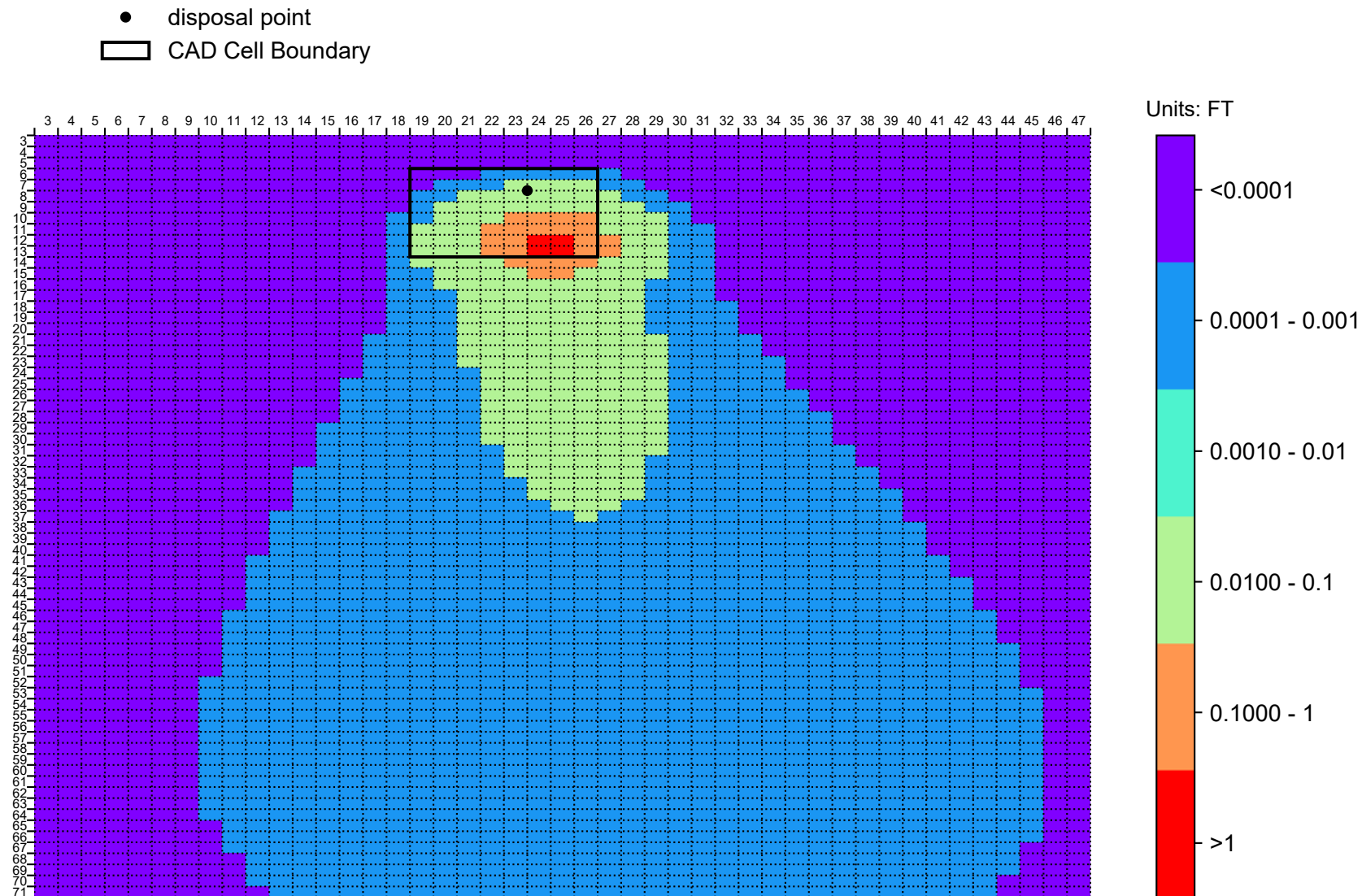


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_4.duo

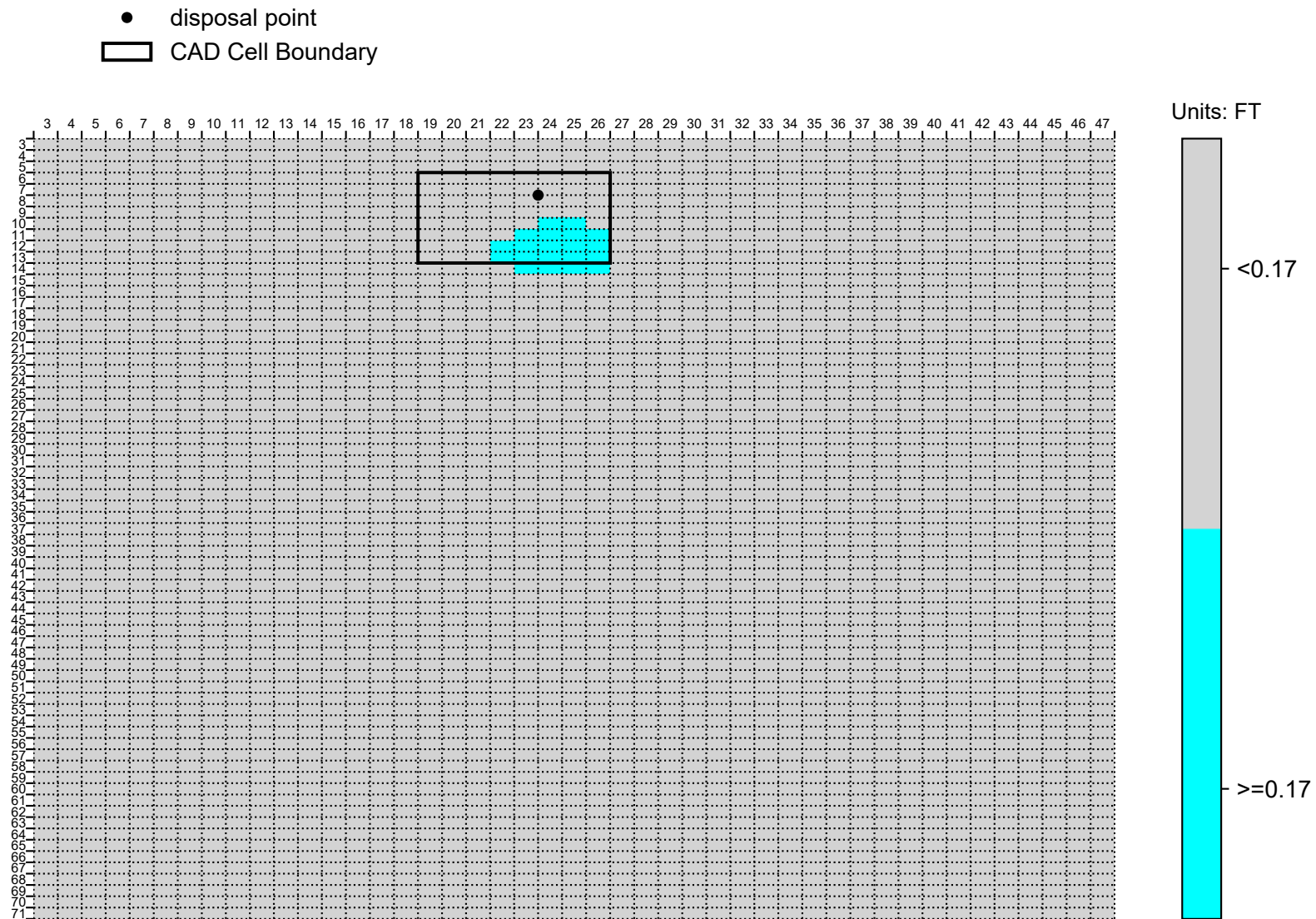
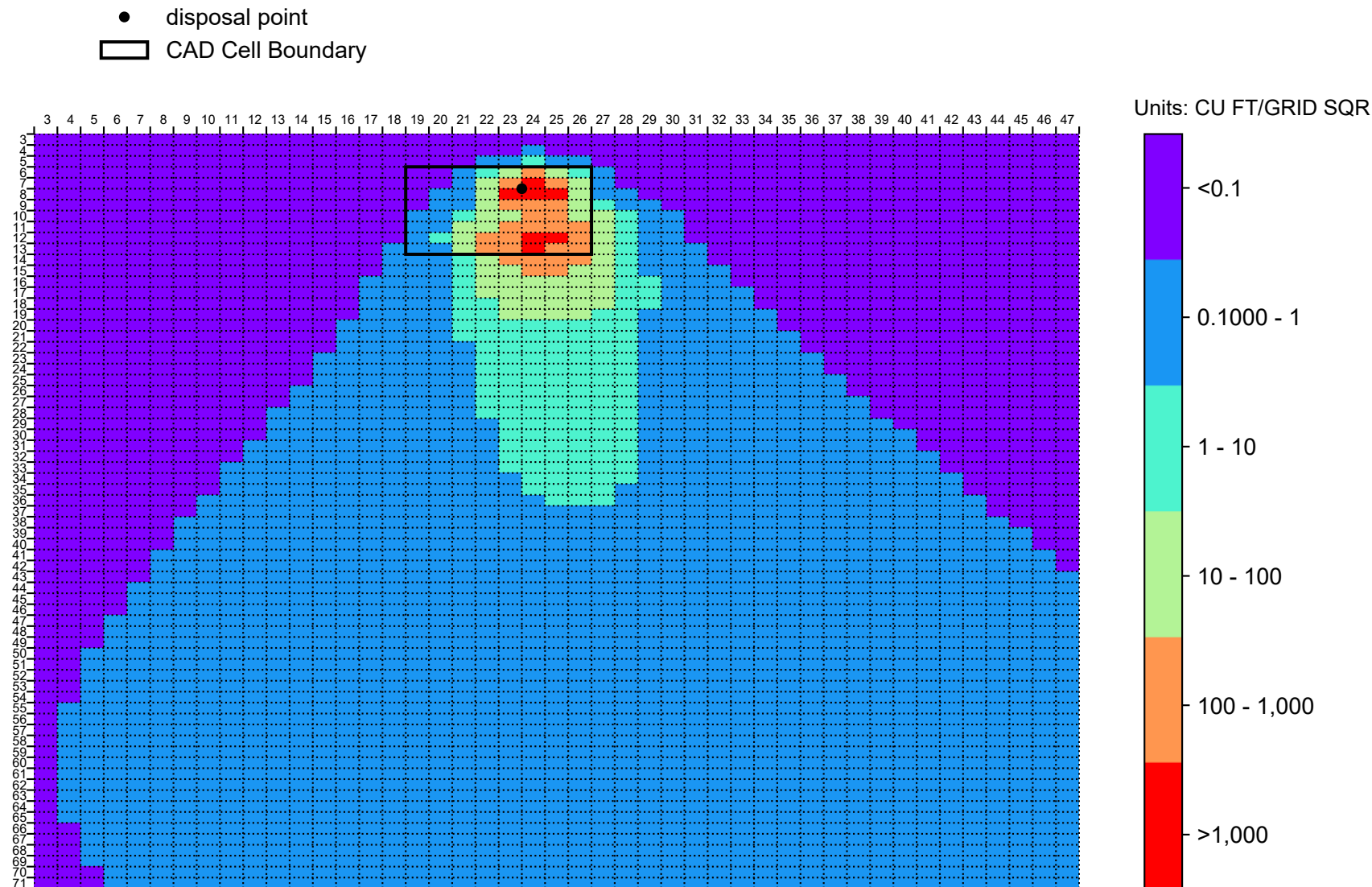


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_4.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 906.98
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 910.00
 Total Lost (cu/yd) = 3.02
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 398.78

Total Accumulated Material WITHIN Boundary (cu/yd) = 795.29
 Total Lost (cu/yd) = 114.71
 Percent Material Outside Boundary (%) = 12.60
 f value = 0.455

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point A at [7,23]. Results are adjusted to include multiplier.
 Source: LNBCAD_AENP_5C.duo



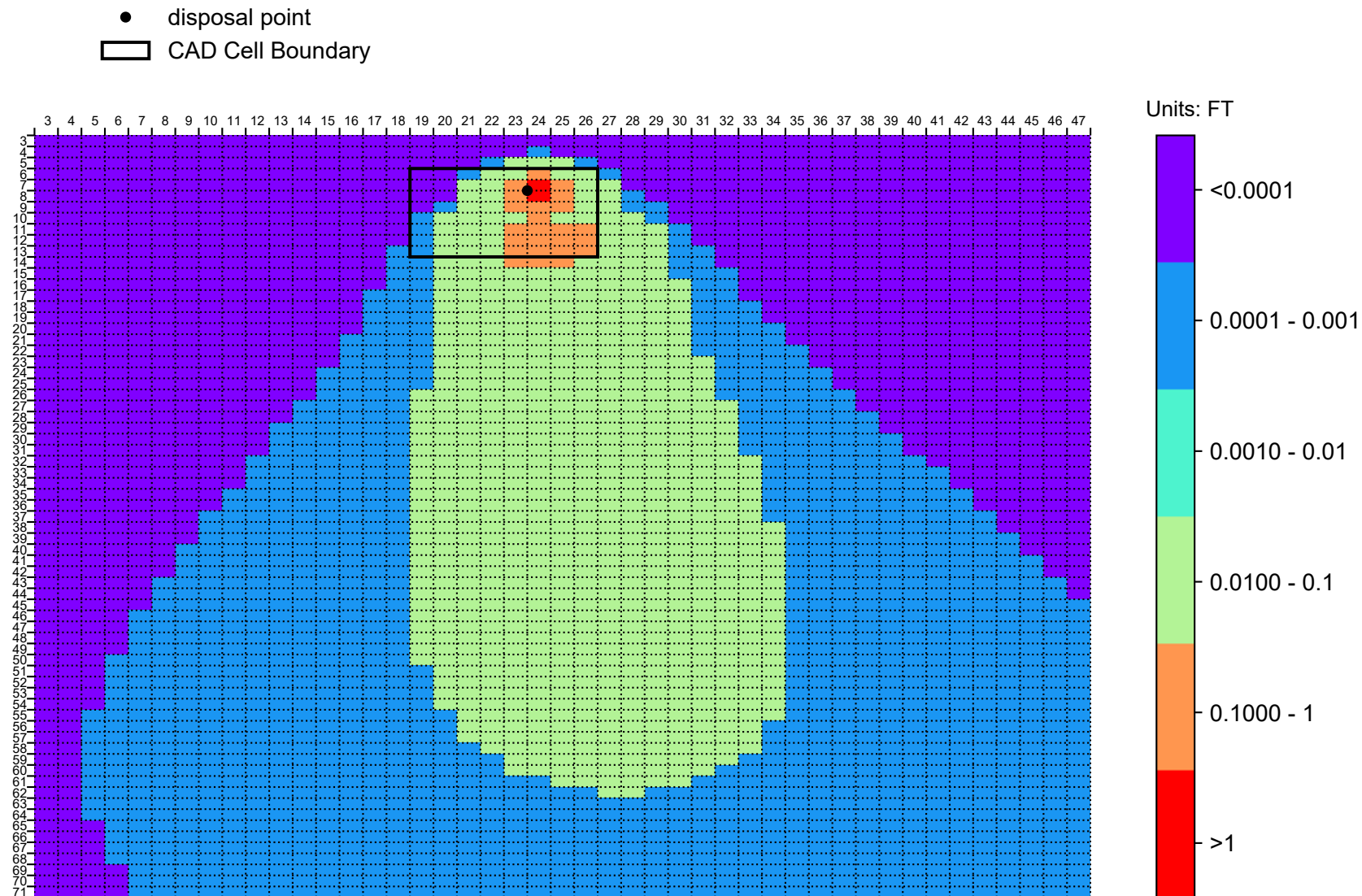


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_5C.duo

- disposal point
- CAD Cell Boundary

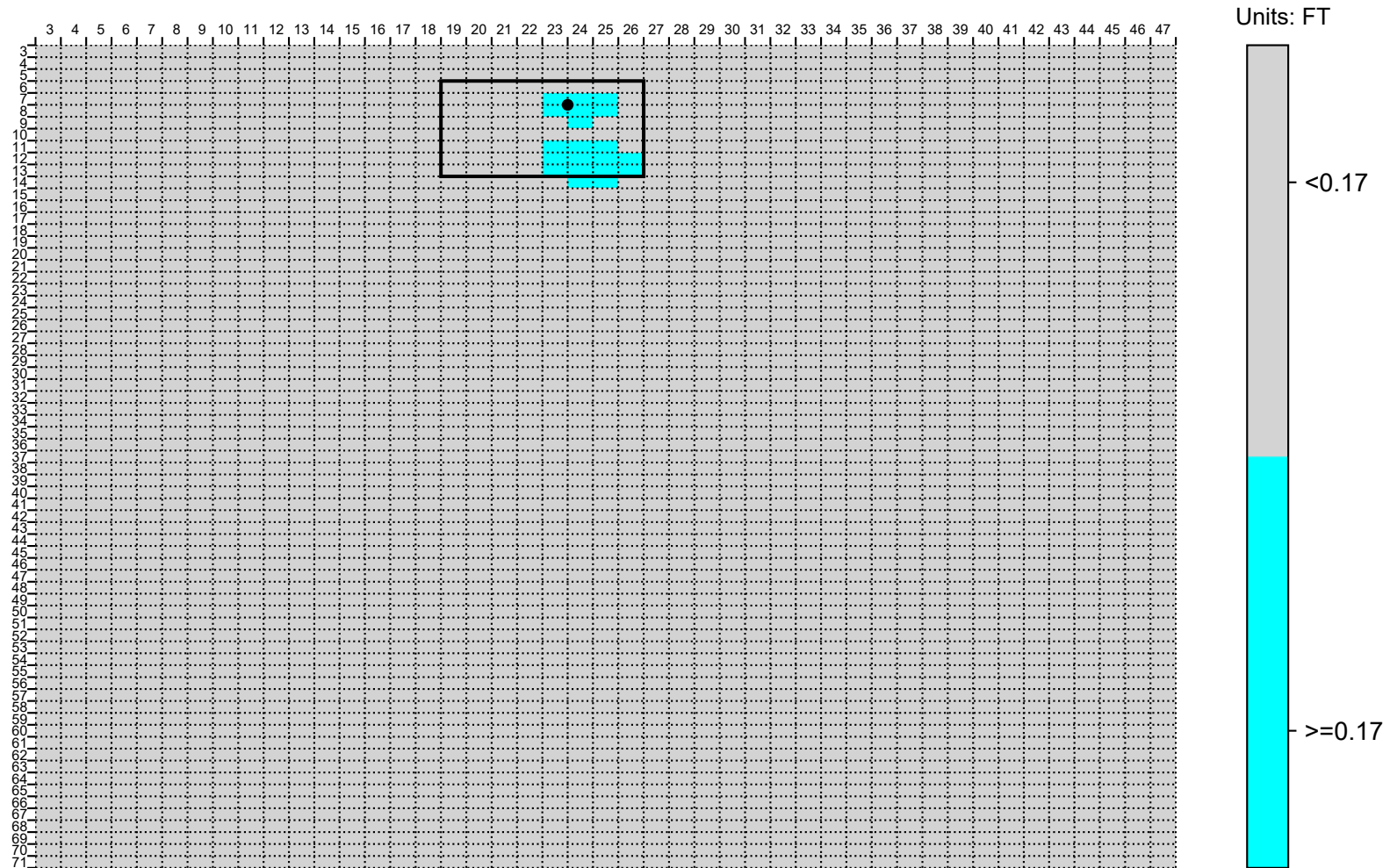
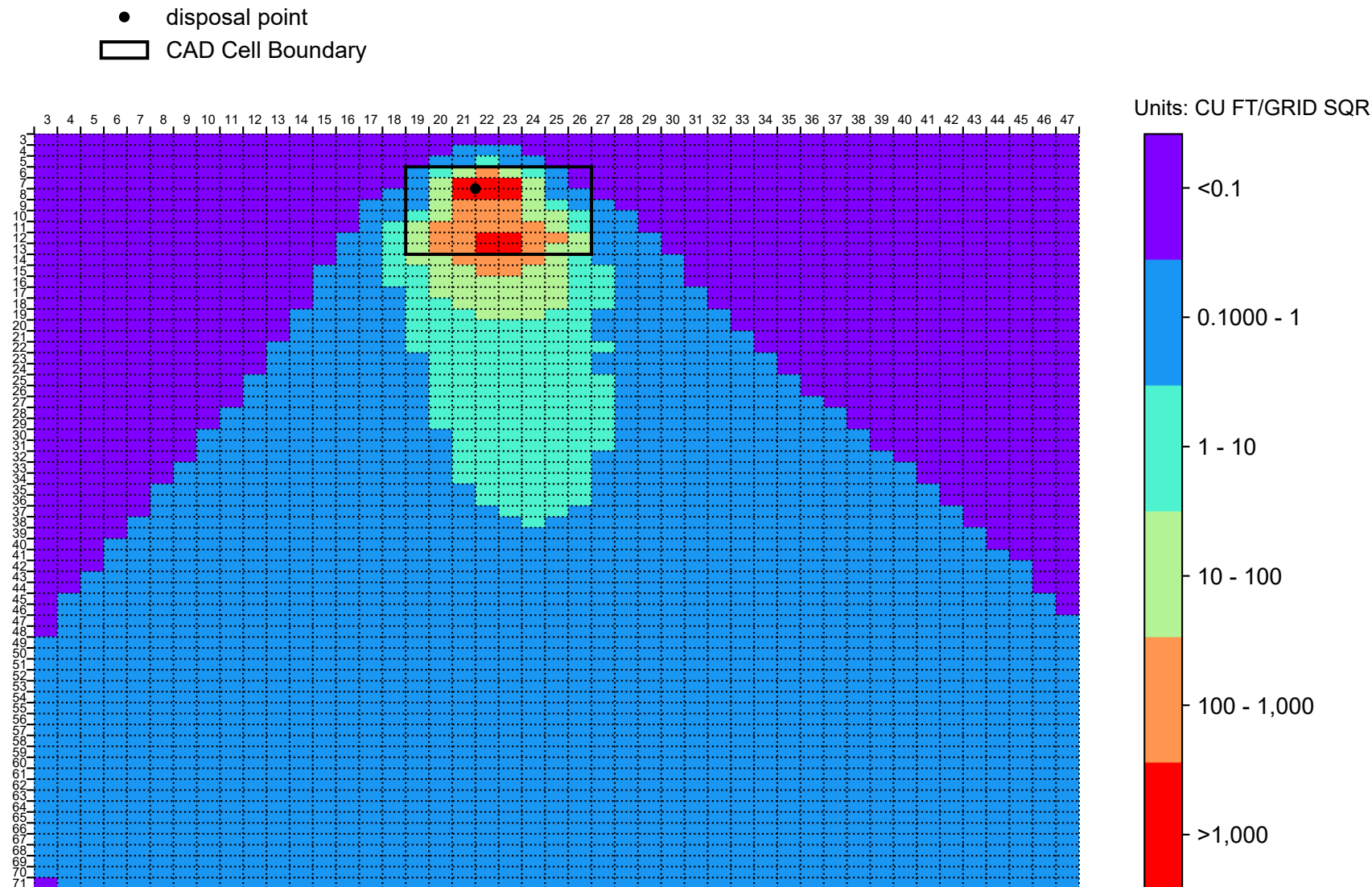


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point A at [7,23]. Results are adjusted to include multiplier.

Source: LNBCAD_AENP_5C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1082.54
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1084.00
 Total Lost (cu/yd) = 1.46
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 457.99

Total Accumulated Material WITHIN Boundary (cu/yd) = 959.13
 Total Lost (cu/yd) = 124.87
 Percent Material Outside Boundary (%) = 11.50
 f value = 0.542

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_1C.duo



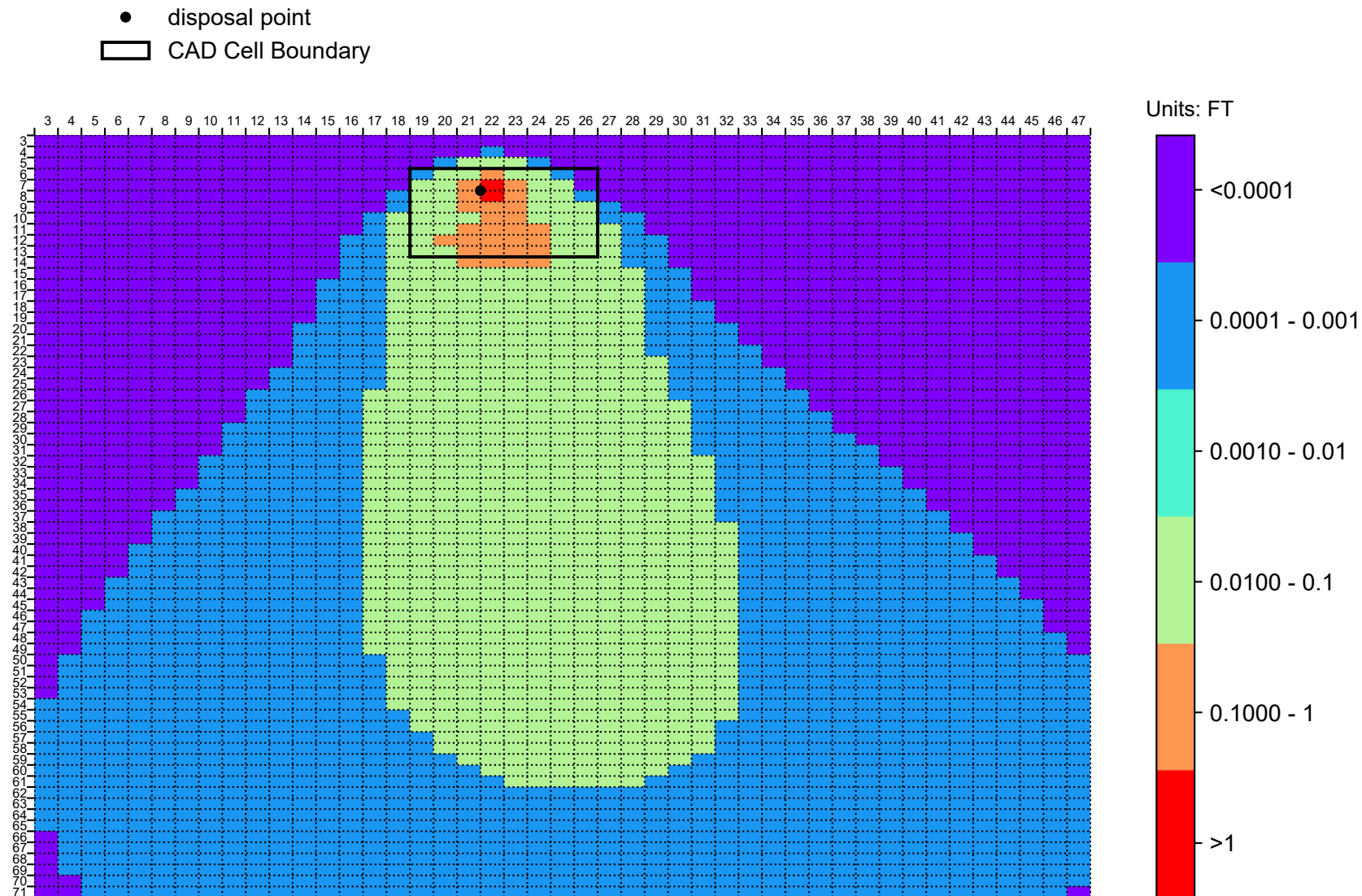


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_1C.duo

- disposal point
- CAD Cell Boundary

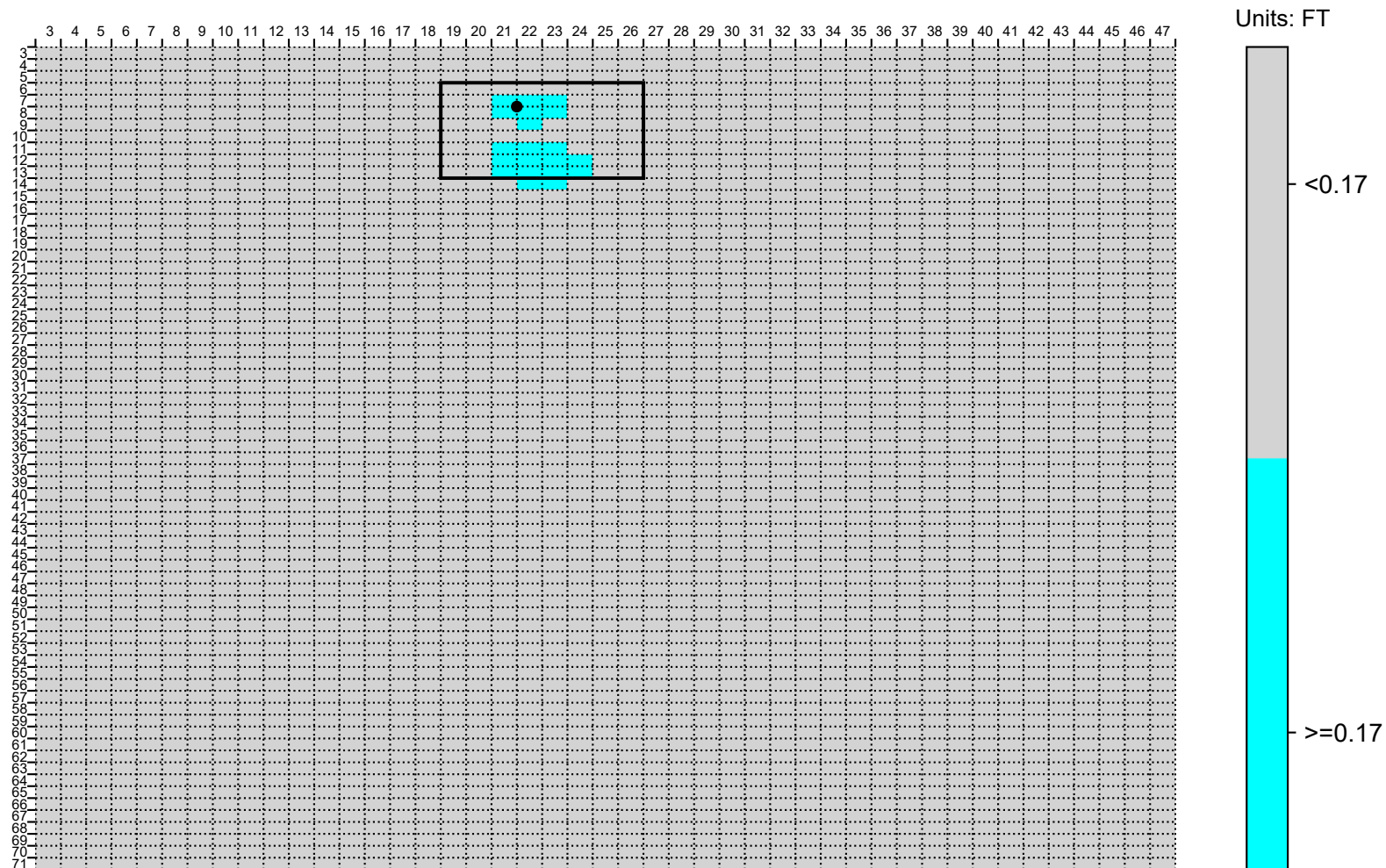
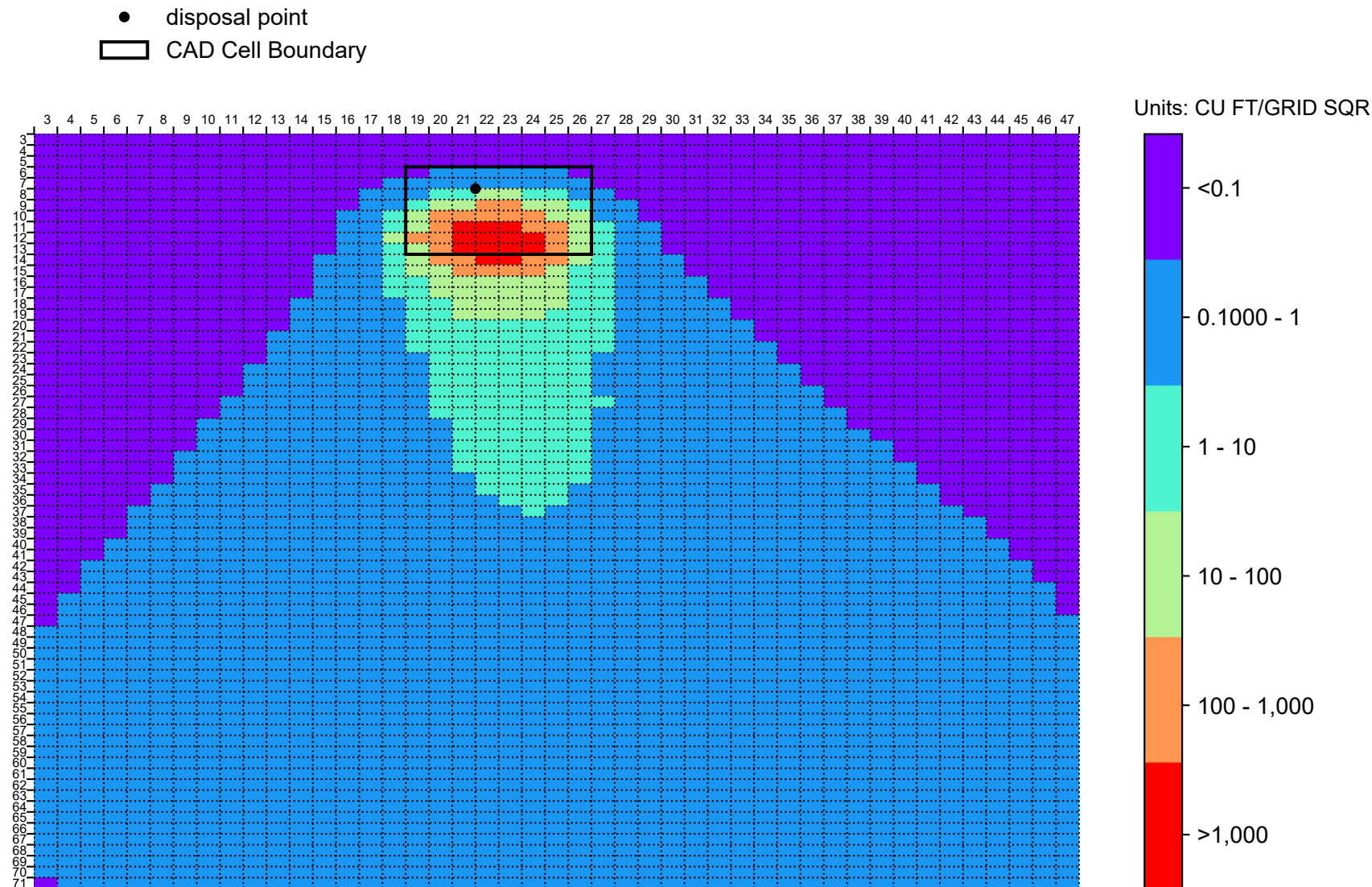


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_1C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1431.35
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1434.00
 Total Lost (cu/yd) = 2.65
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 190.36

Total Accumulated Material WITHIN Boundary (cu/yd) = 1171.90
 Total Lost (cu/yd) = 262.10
 Percent Material Outside Boundary (%) = 18.30
 f value = 0.717

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point B at [7,21]. Results are adjusted to include multiplier.
 Source: LNBCAD_BENP_2.duo



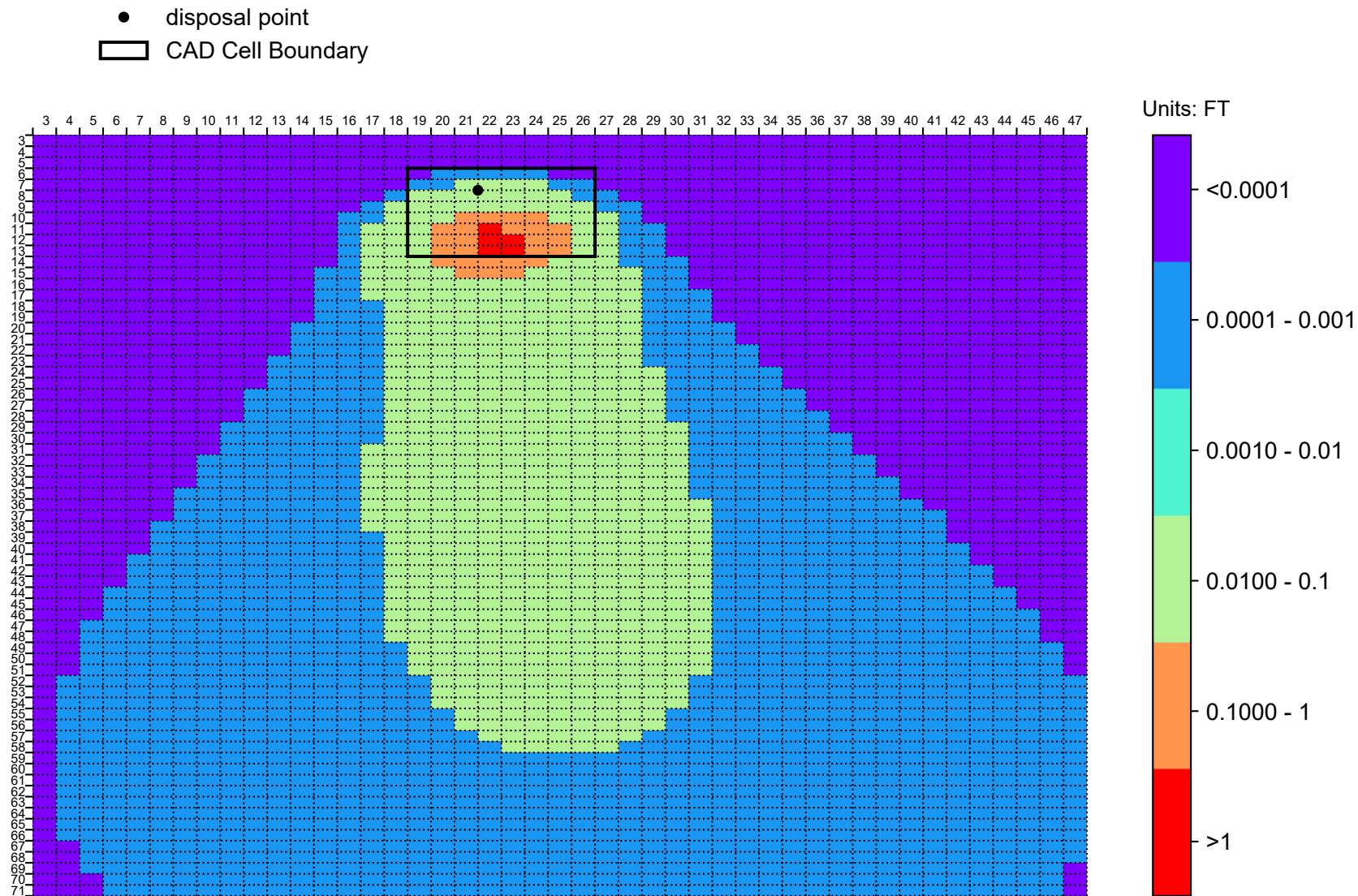


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_2.duo

- disposal point
- CAD Cell Boundary

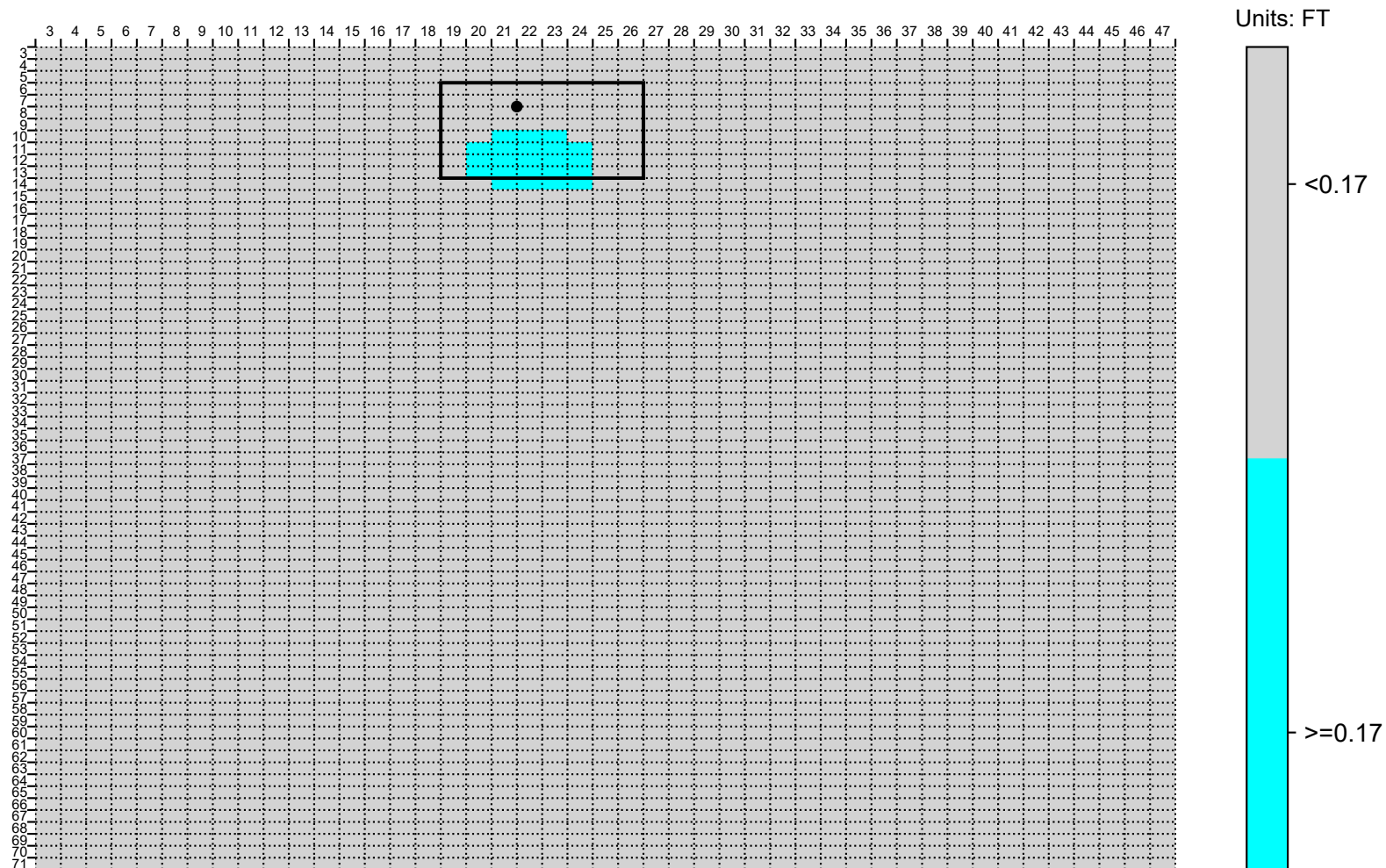
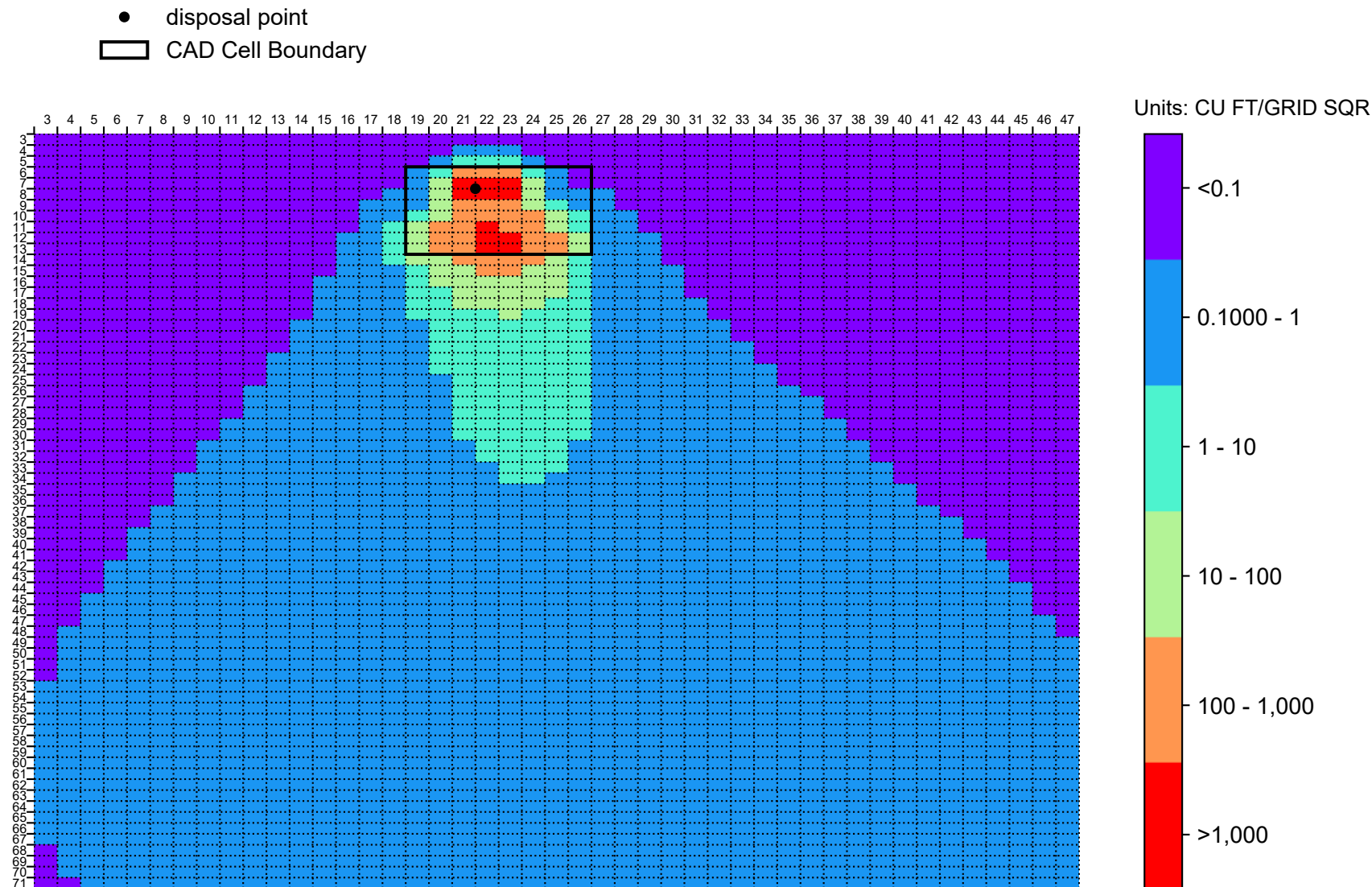


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_2.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1314.42
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1316.00
 Total Lost (cu/yd) = 1.58
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 583.09

Total Accumulated Material WITHIN Boundary (cu/yd) = 1193.83
 Total Lost (cu/yd) = 122.17
 Percent Material Outside Boundary (%) = 9.30
 f value = 0.658

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point B at [7,21]. Results are adjusted to include multiplier.
 Source: LNBCAD_BENP_3C.duo



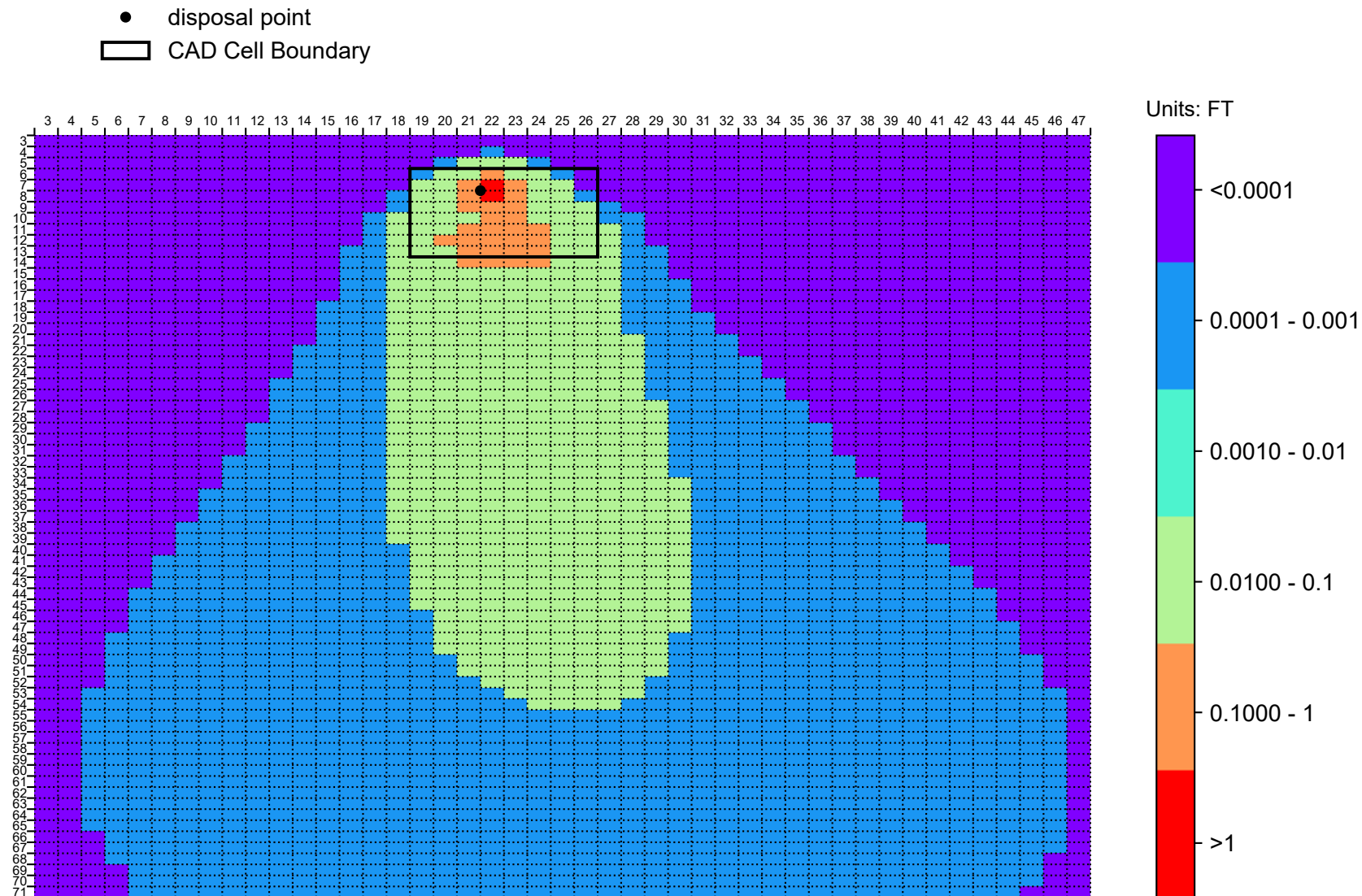


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_3C.duo

- disposal point
- CAD Cell Boundary

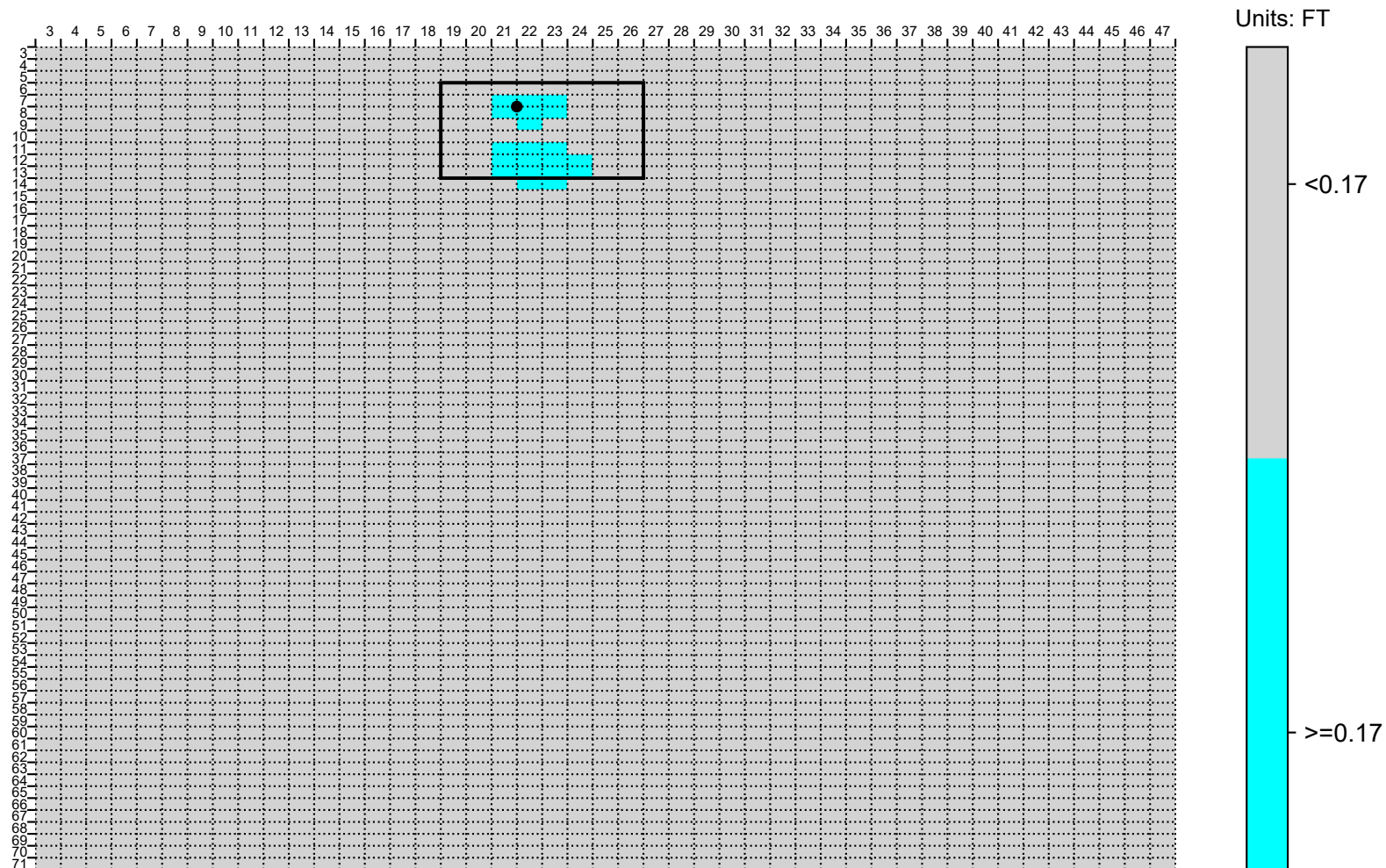
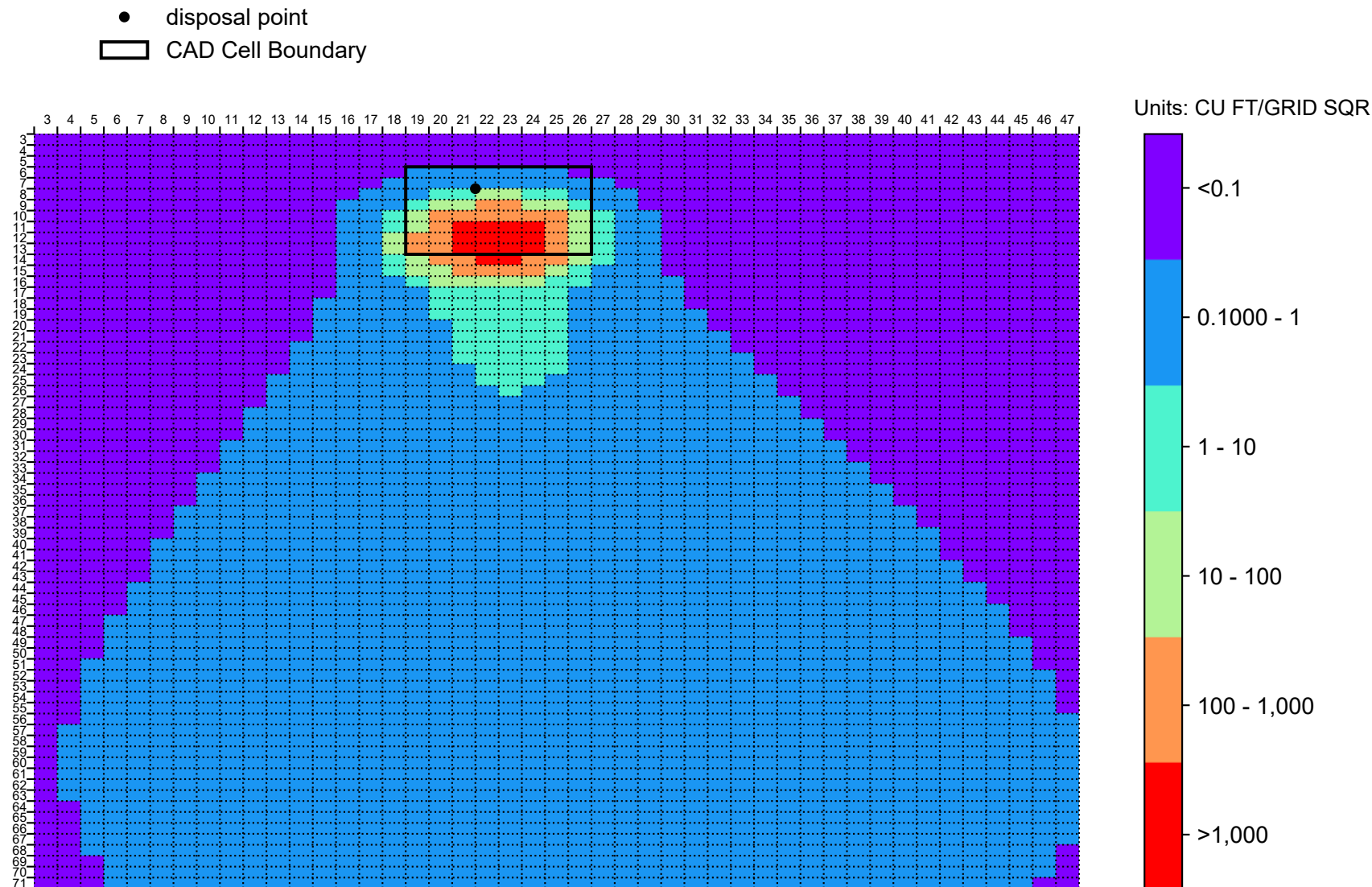


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_3C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1648.75
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1648.00
 Total Lost (cu/yd) = 0.00
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 229.48

Total Accumulated Material WITHIN Boundary (cu/yd) = 1379.19
 Total Lost (cu/yd) = 268.81
 Percent Material Outside Boundary (%) = 16.30
 f value = 0.824

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point B at [7,21]. Results are adjusted to include multiplier.
 Source: LNBCAD_BENP_4.duo



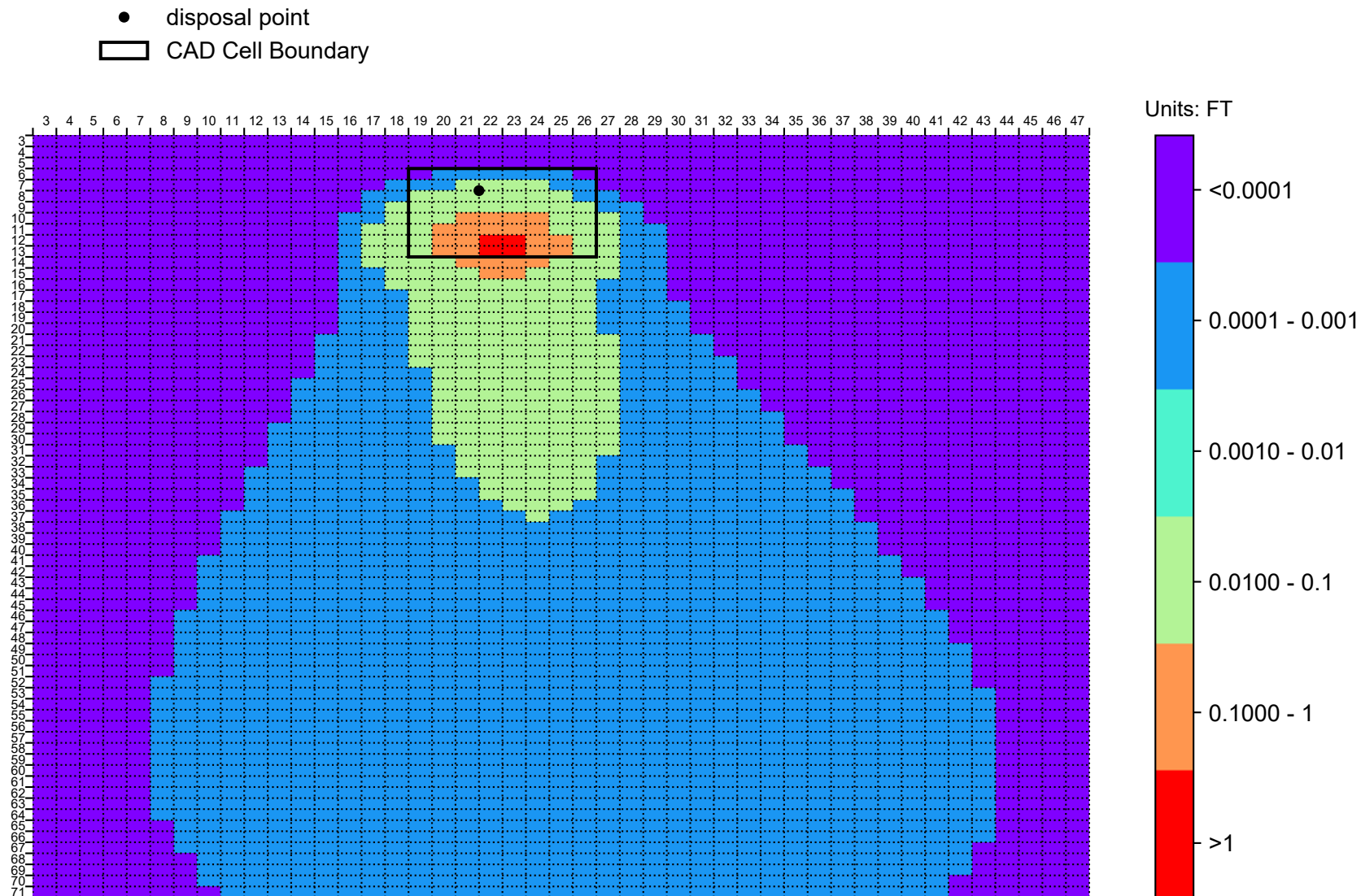


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_4.duo

- disposal point
- CAD Cell Boundary

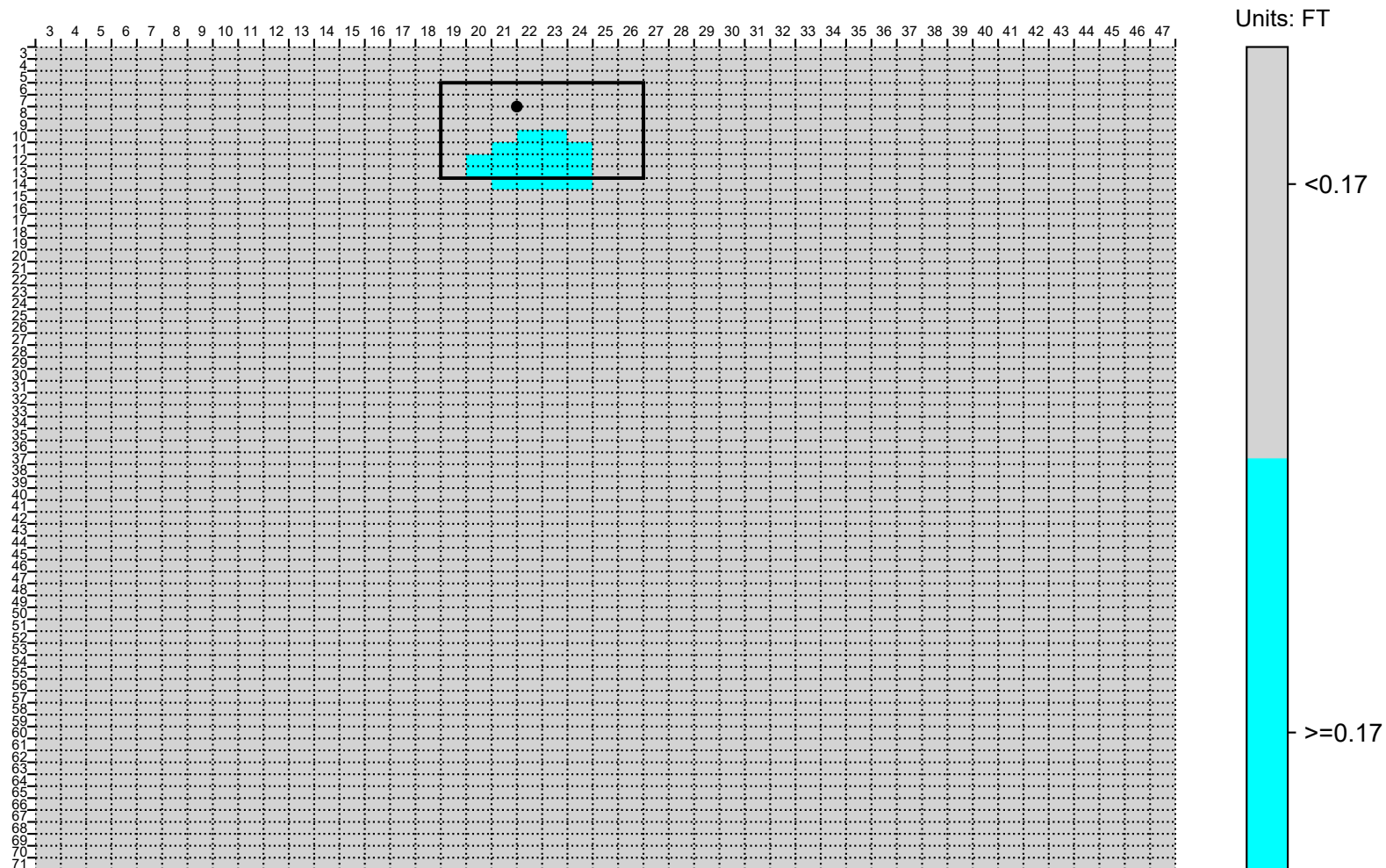
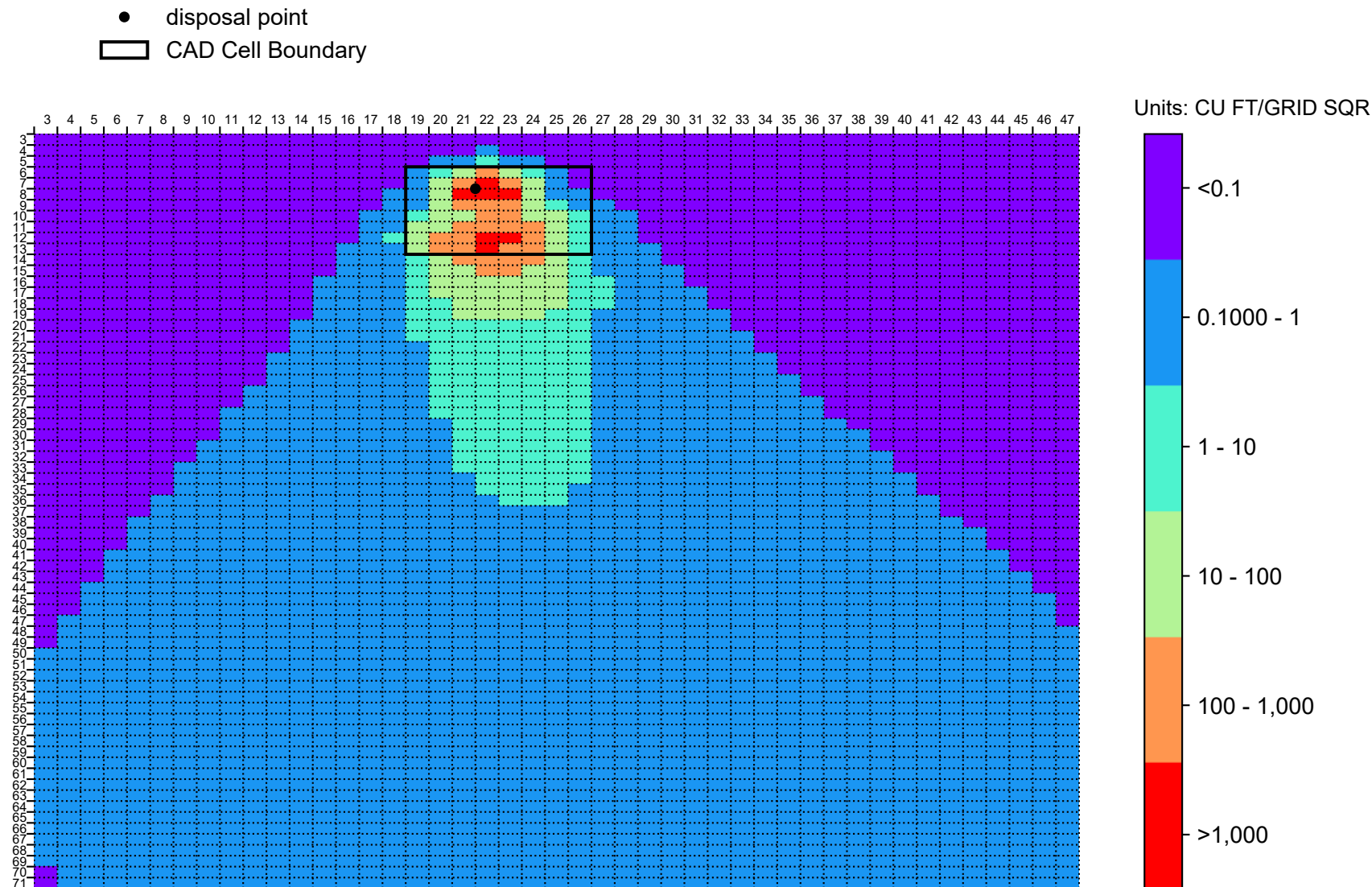


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_4.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 907.13
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 910.00
 Total Lost (cu/yd) = 2.87
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 398.78

Total Accumulated Material WITHIN Boundary (cu/yd) = 803.27
 Total Lost (cu/yd) = 106.73
 Percent Material Outside Boundary (%) = 11.70
 f value = 0.455

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point B at [7,21]. Results are adjusted to include multiplier.
 Source: LNBCAD_BENP_5C.duo



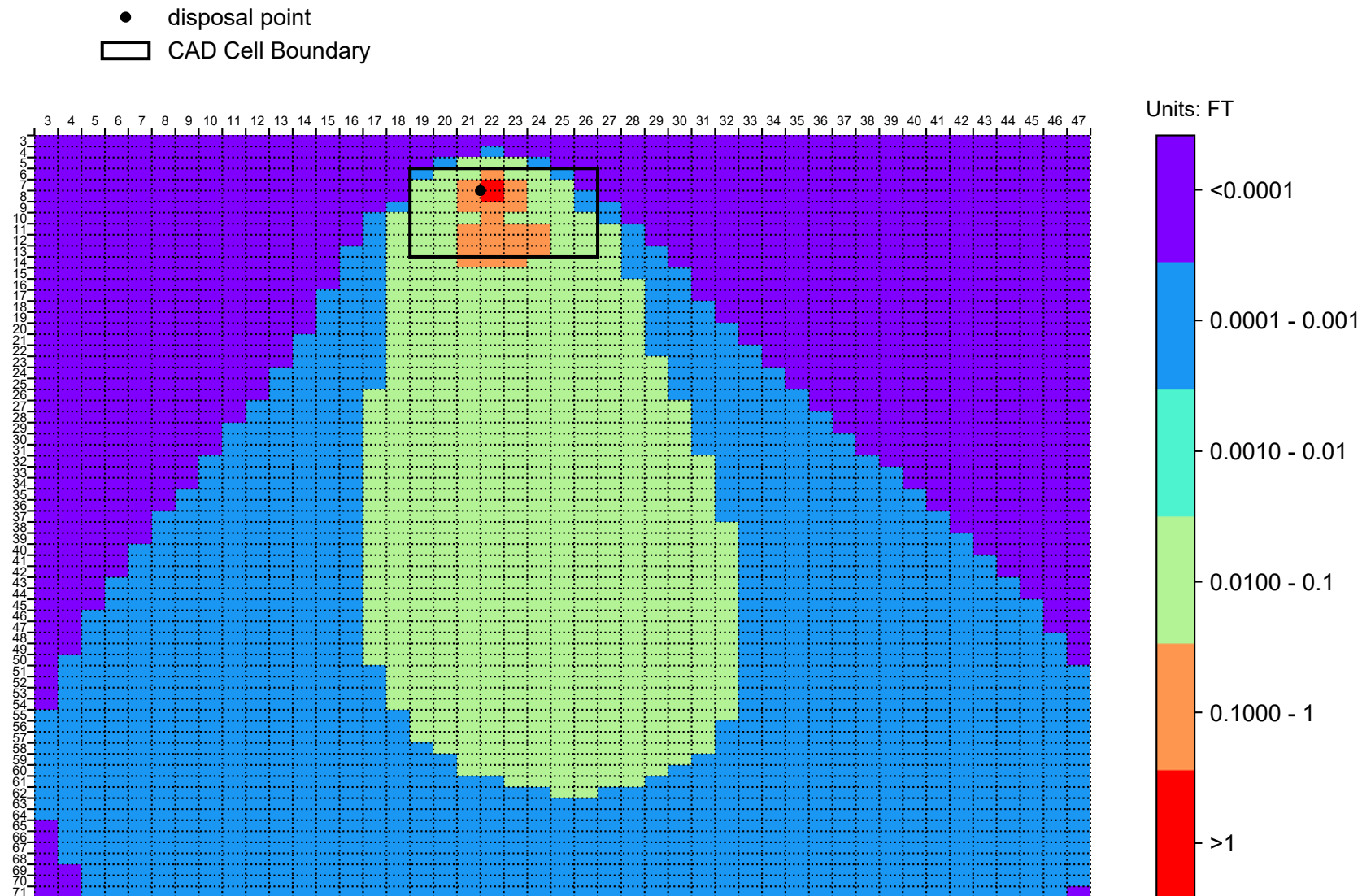


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_5C.duo

- disposal point
- CAD Cell Boundary

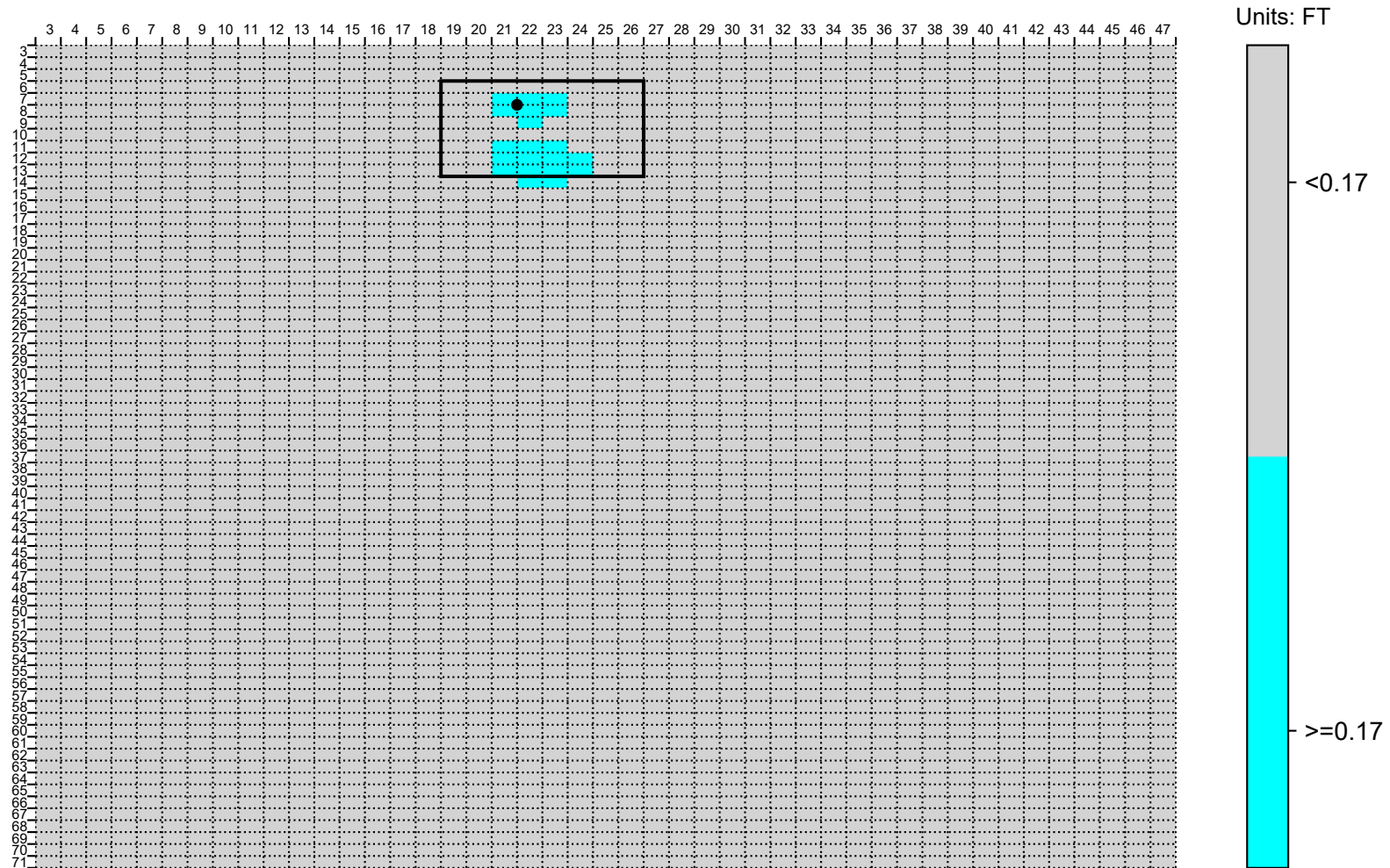
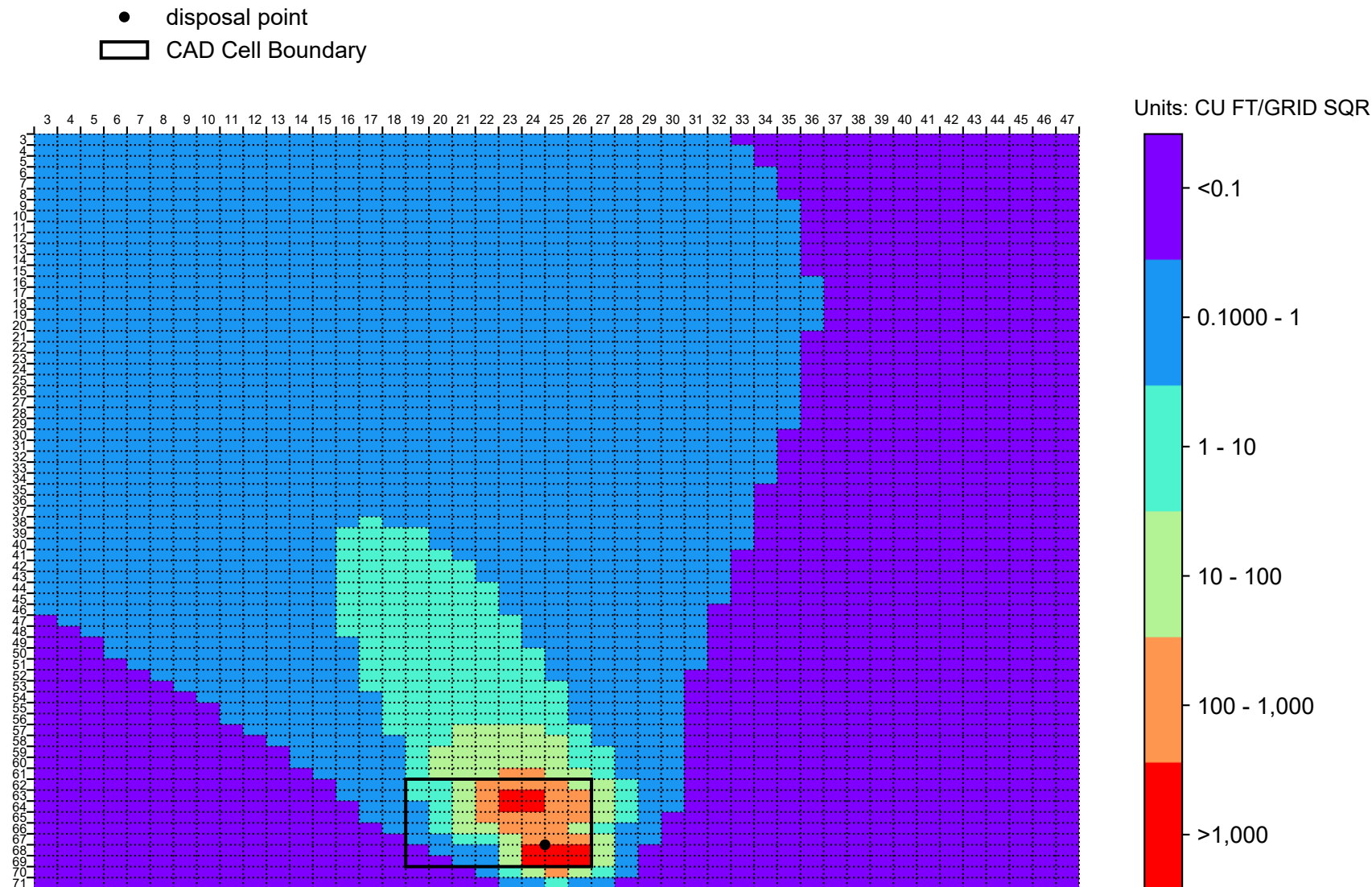


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point B at [7,21]. Results are adjusted to include multiplier.

Source: LNBCAD_BENP_5C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1079.70
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1084.00
 Total Lost (cu/yd) = 4.30
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 407.01

Total Accumulated Material WITHIN Boundary (cu/yd) = 994.48
 Total Lost (cu/yd) = 89.52
 Percent Material Outside Boundary (%) = 8.30
 f value = 0.542

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_1C.duo



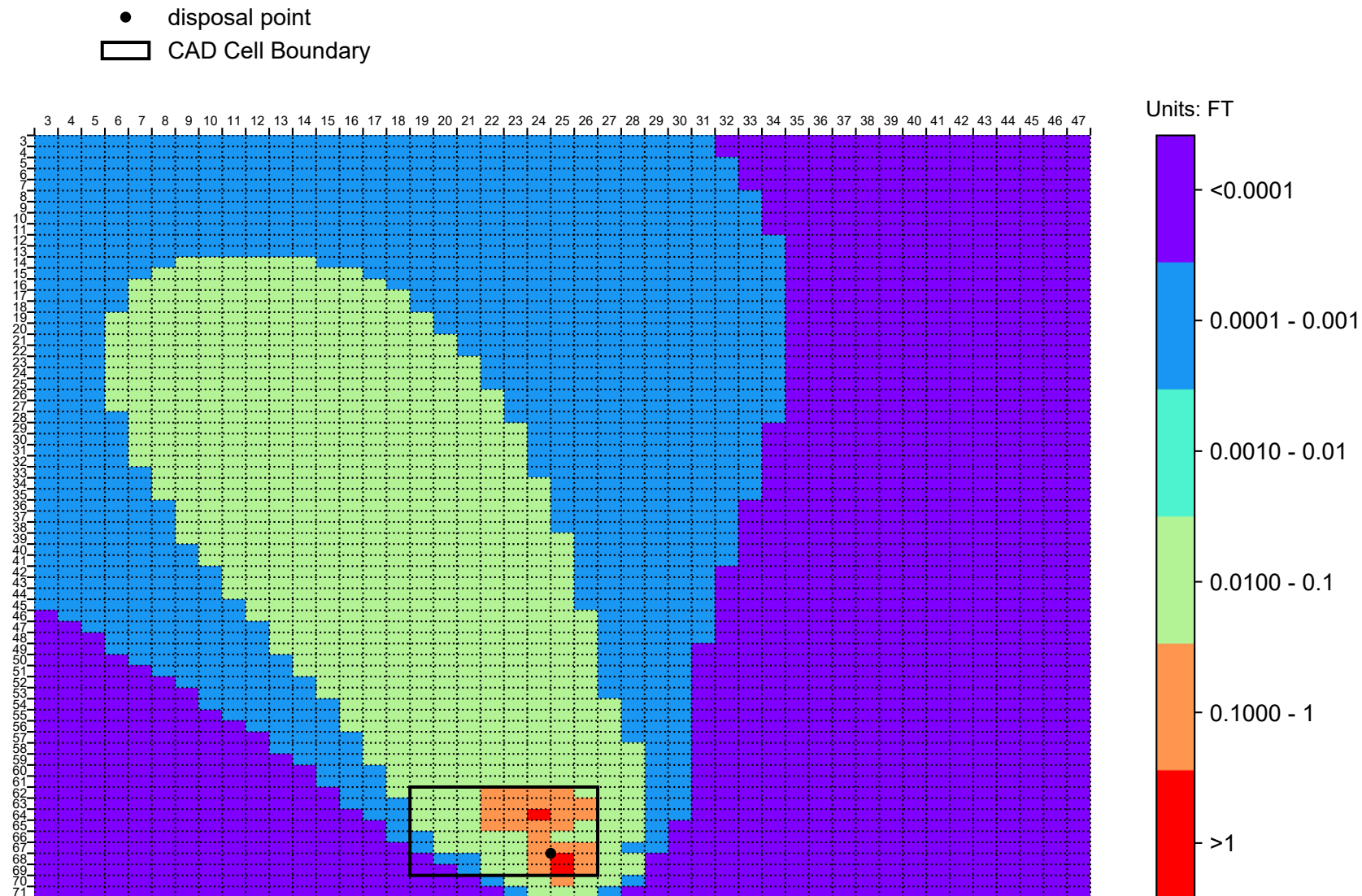


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_1C.duo

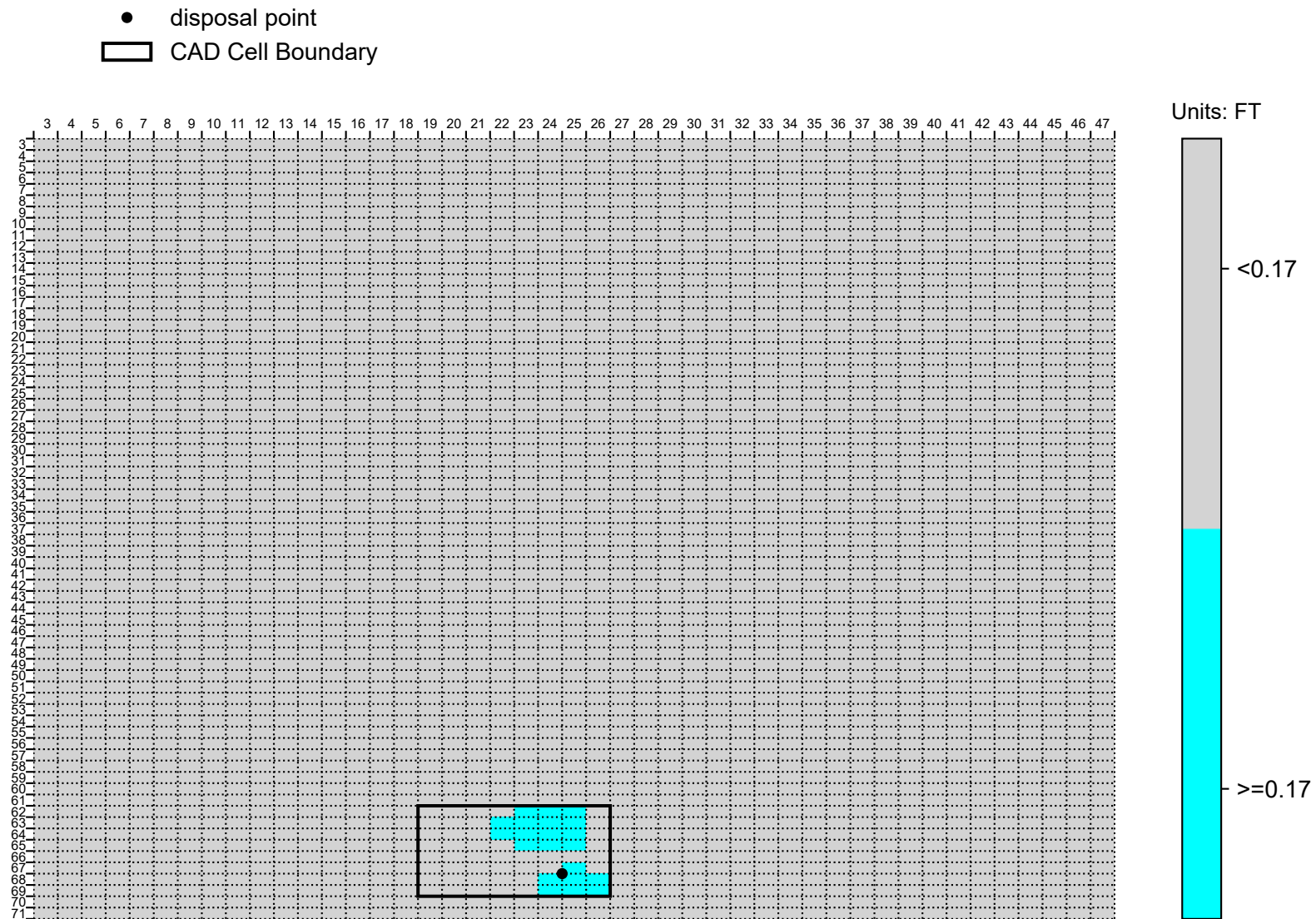
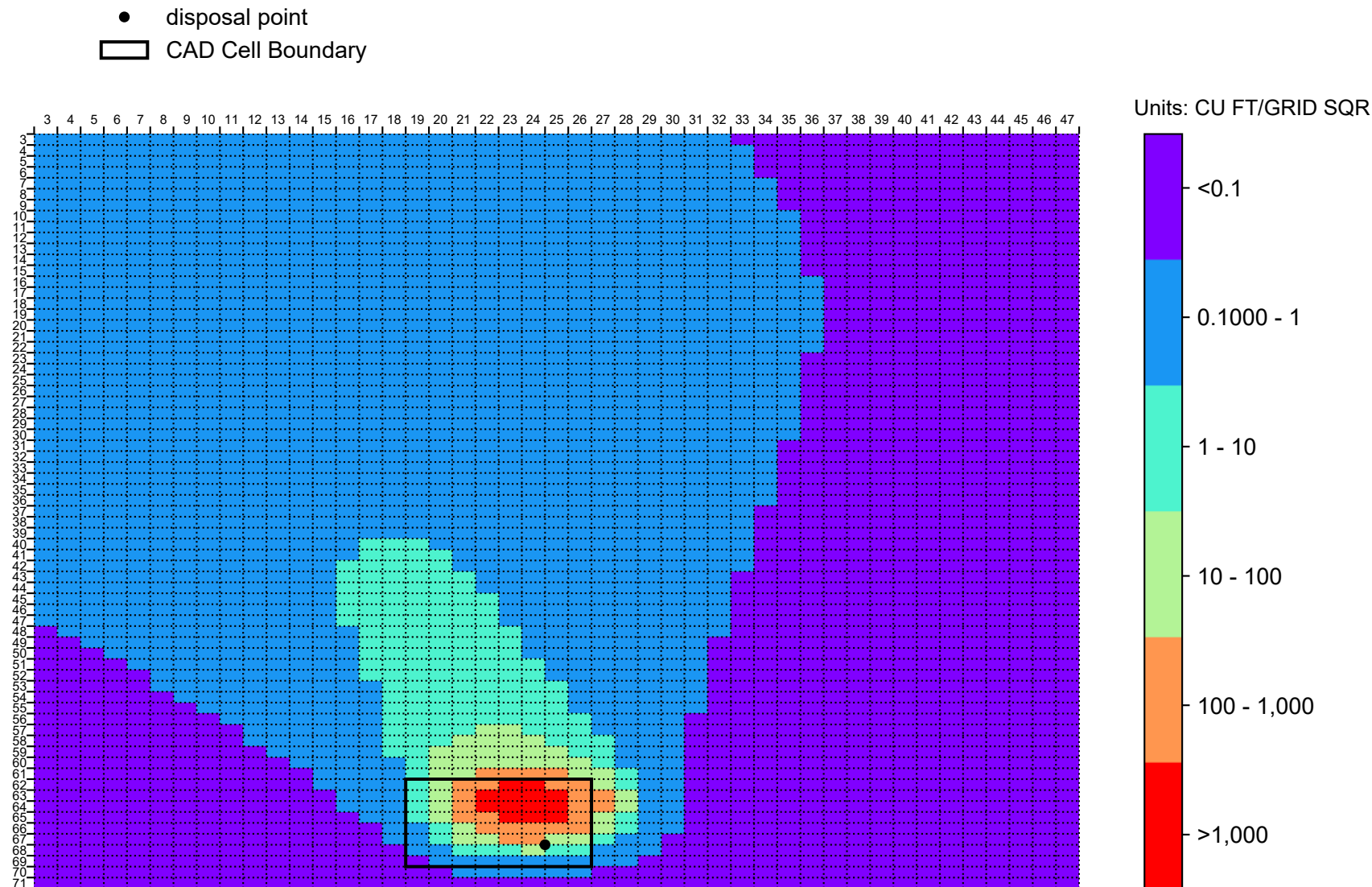


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_1C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1430.54
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1434.00
 Total Lost (cu/yd) = 3.46
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 14.23

Total Accumulated Material WITHIN Boundary (cu/yd) = 1323.96
 Total Lost (cu/yd) = 110.04
 Percent Material Outside Boundary (%) = 7.70
 f value = 0.717

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_2.duo



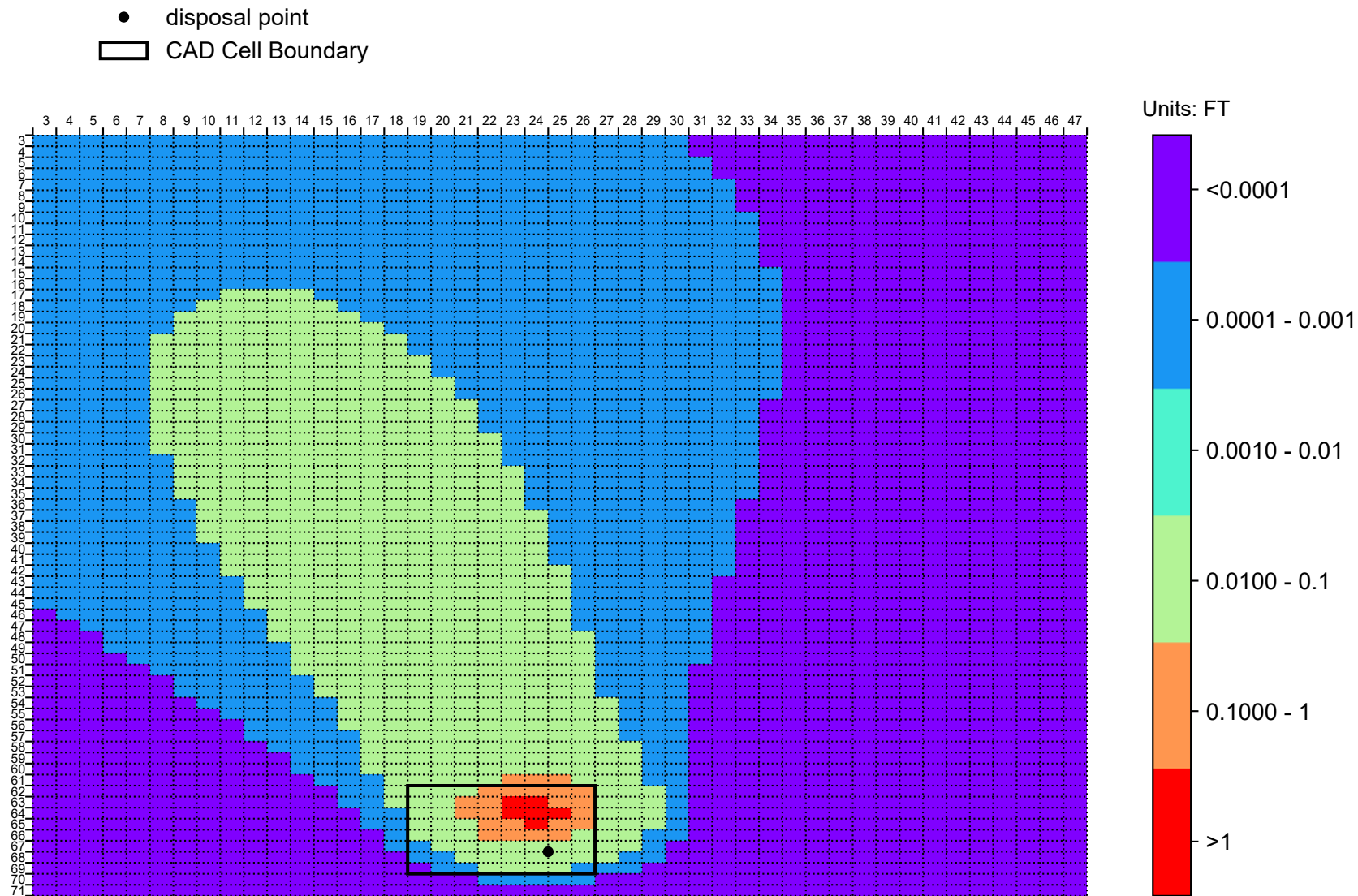


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_2.duo

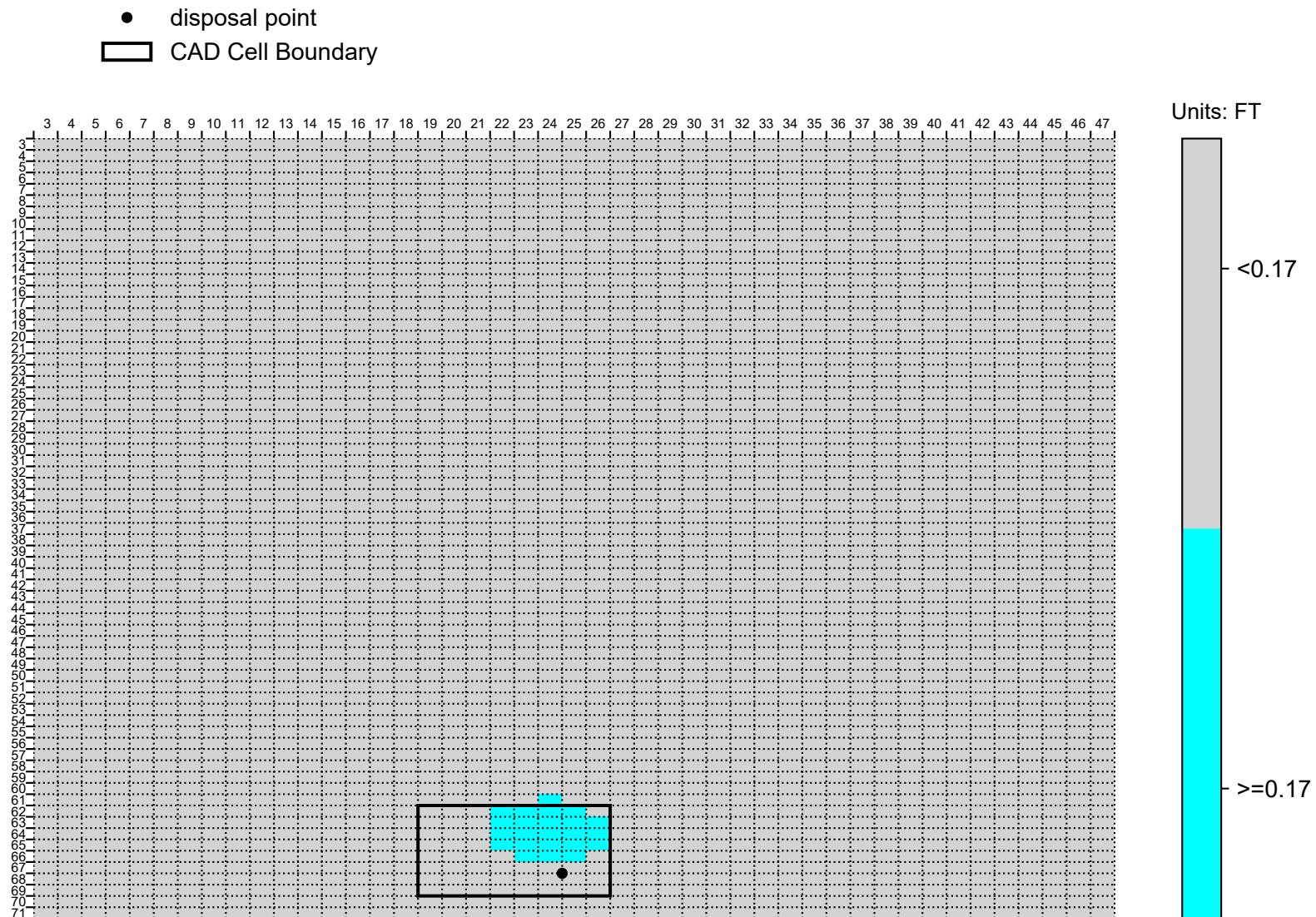
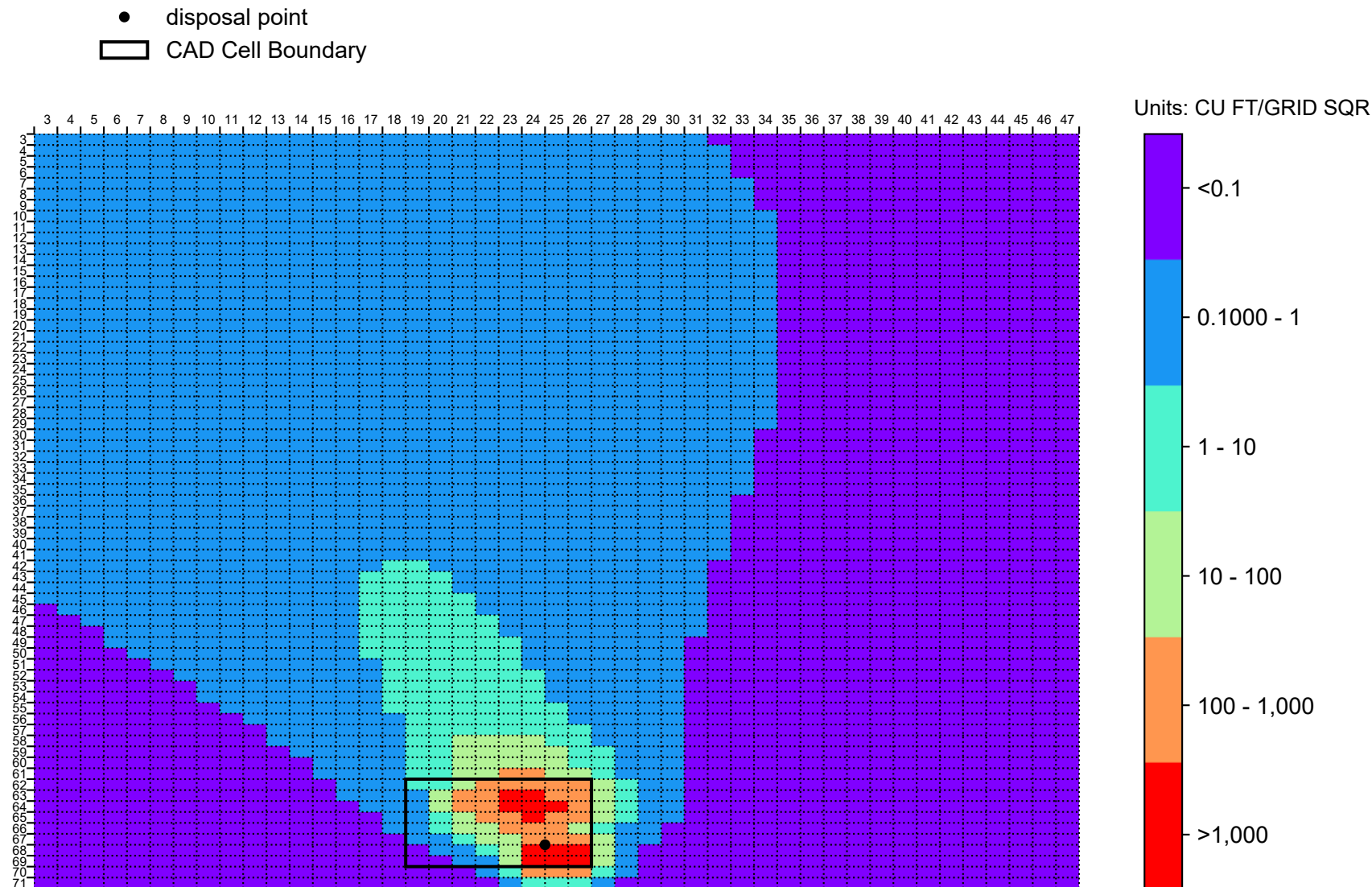


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_2.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1313.39
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1316.00
 Total Lost (cu/yd) = 2.61
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 521.49

Total Accumulated Material WITHIN Boundary (cu/yd) = 1233.06
 Total Lost (cu/yd) = 82.94
 Percent Material Outside Boundary (%) = 6.30
 f value = 0.658

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_3C.duo



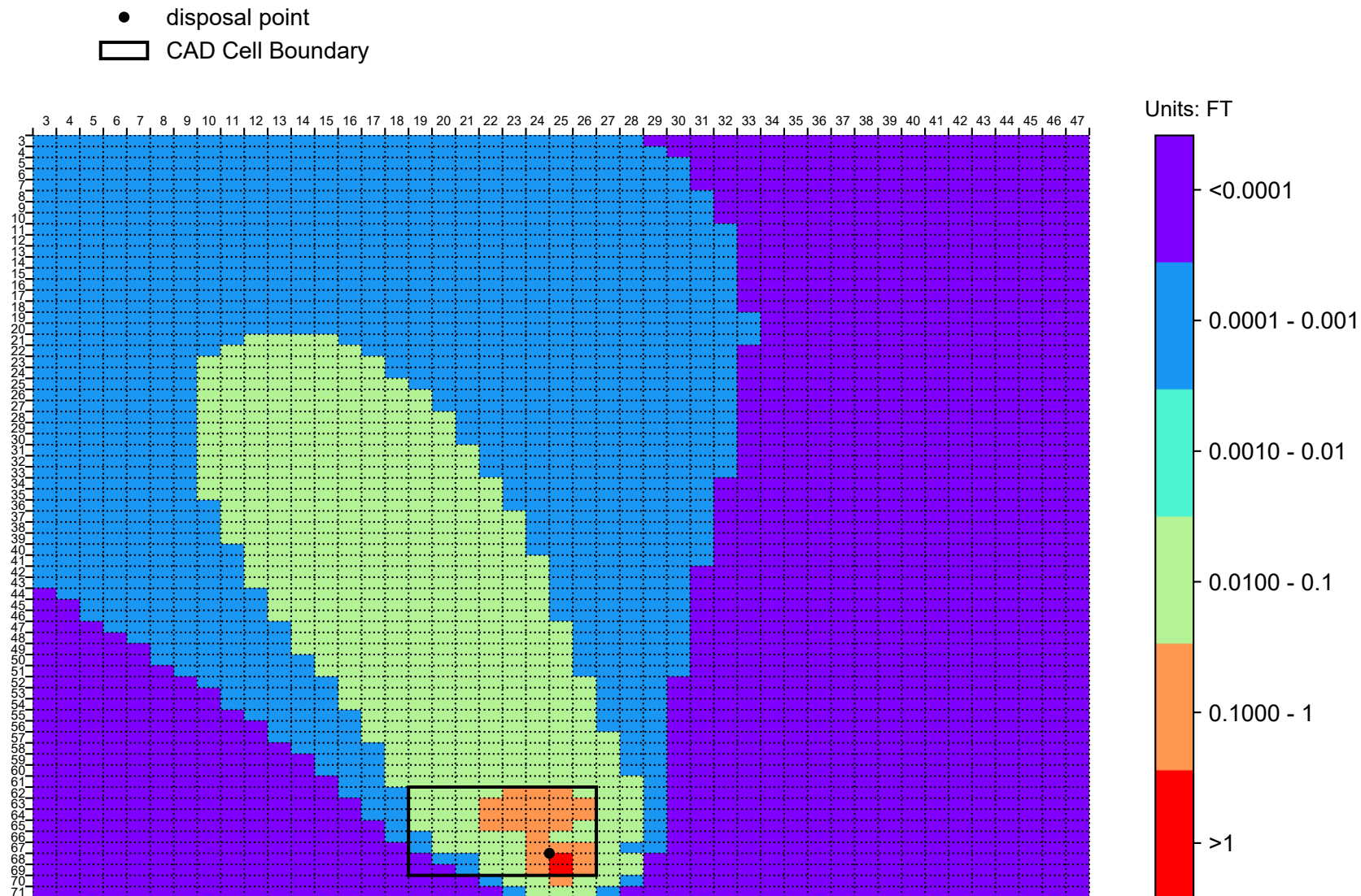


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_3C.duo

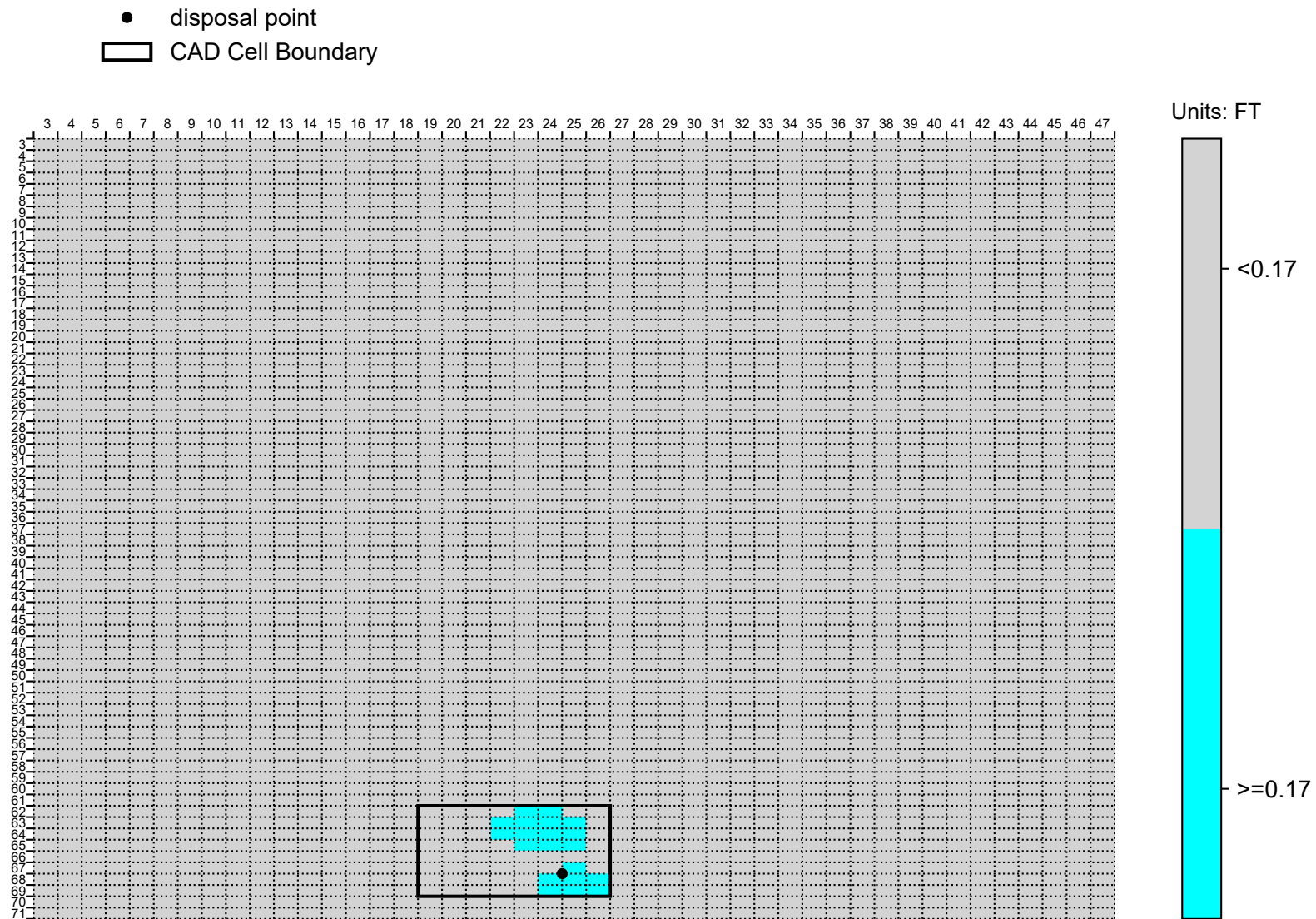
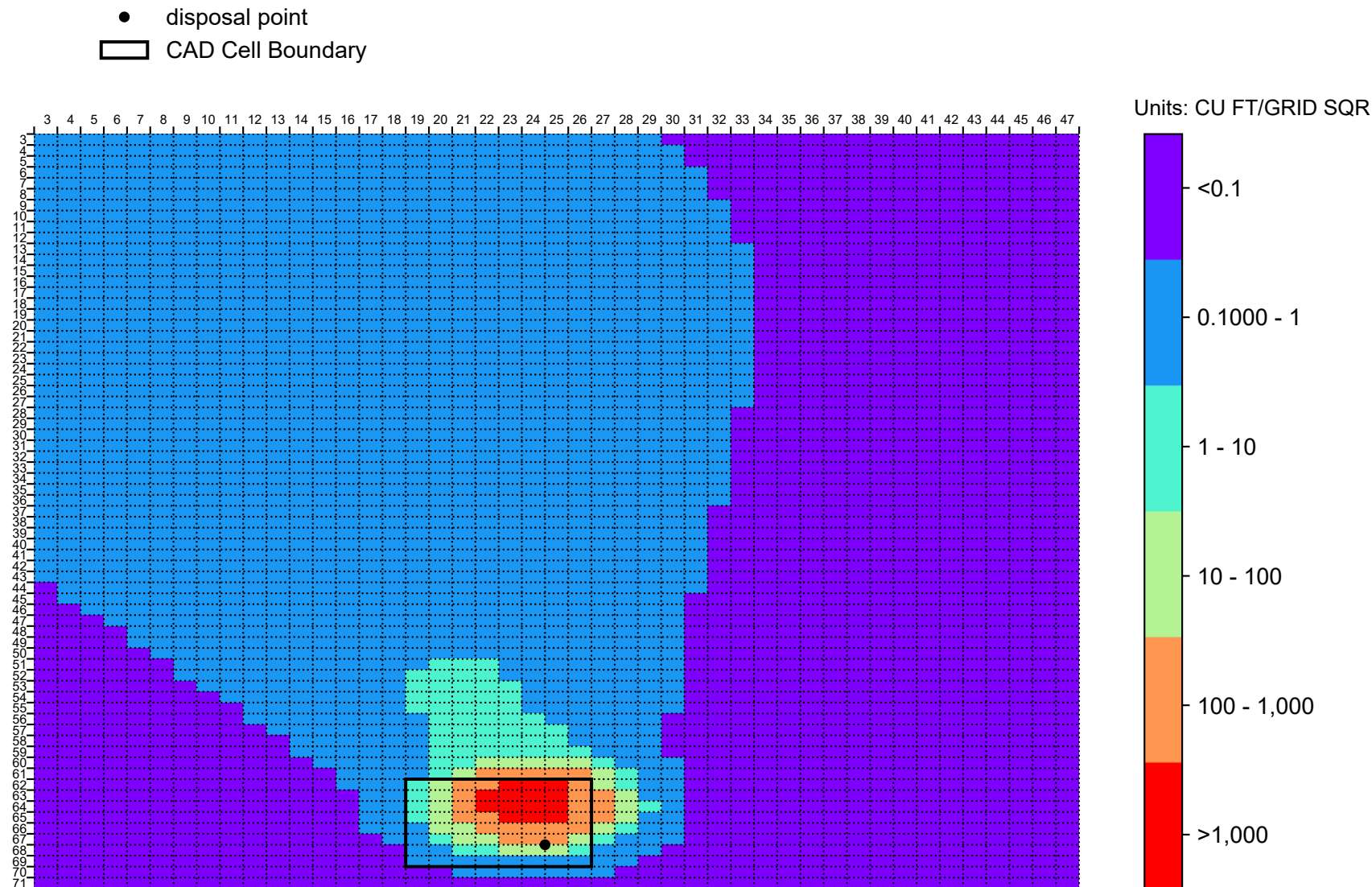


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_3C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1648.75
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1648.00
 Total Lost (cu/yd) = 0.00
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 18.71

Total Accumulated Material WITHIN Boundary (cu/yd) = 1554.78
 Total Lost (cu/yd) = 93.22
 Percent Material Outside Boundary (%) = 5.70
 f value = 0.824

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_4.duo



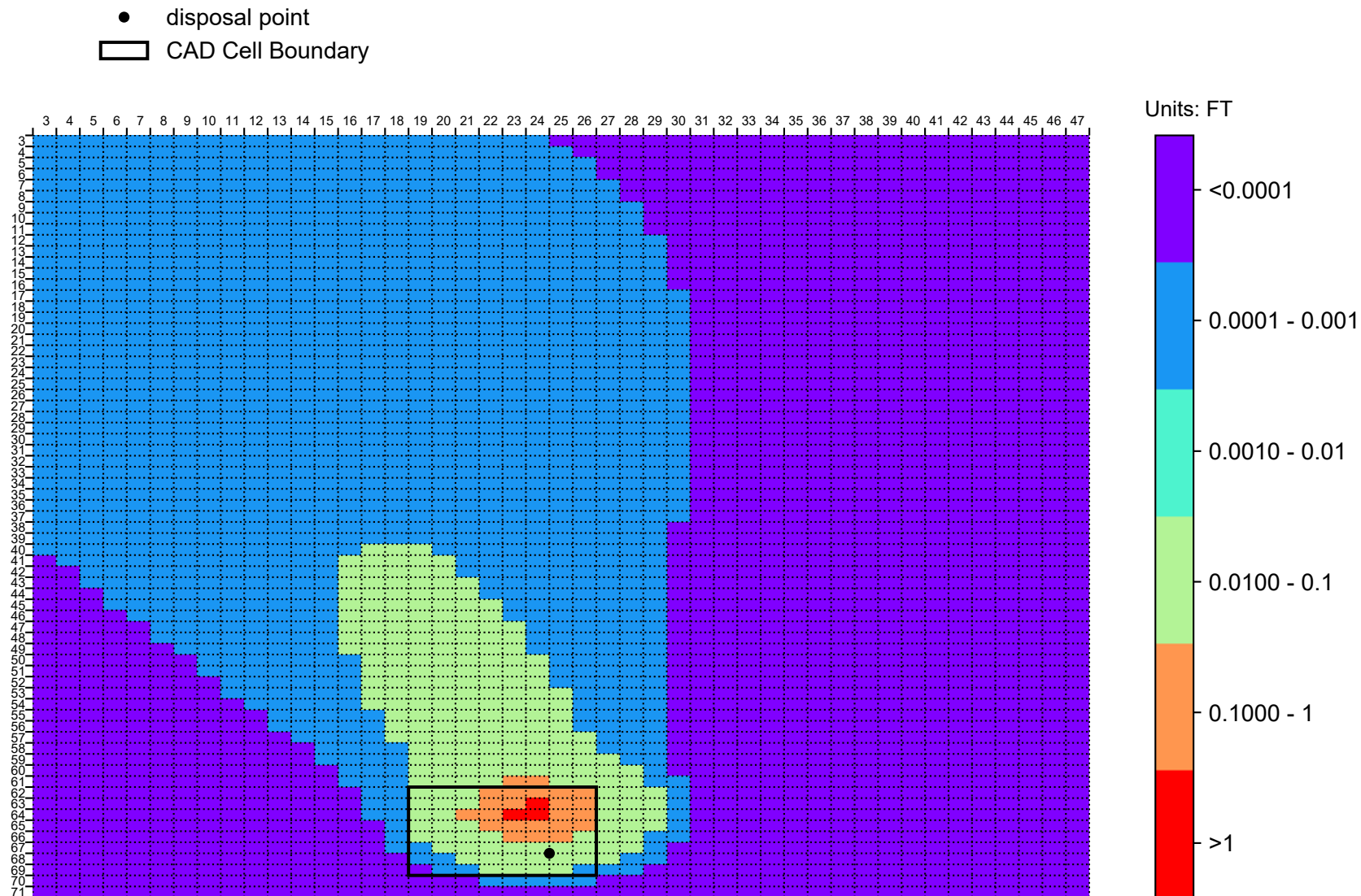


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_4.duo

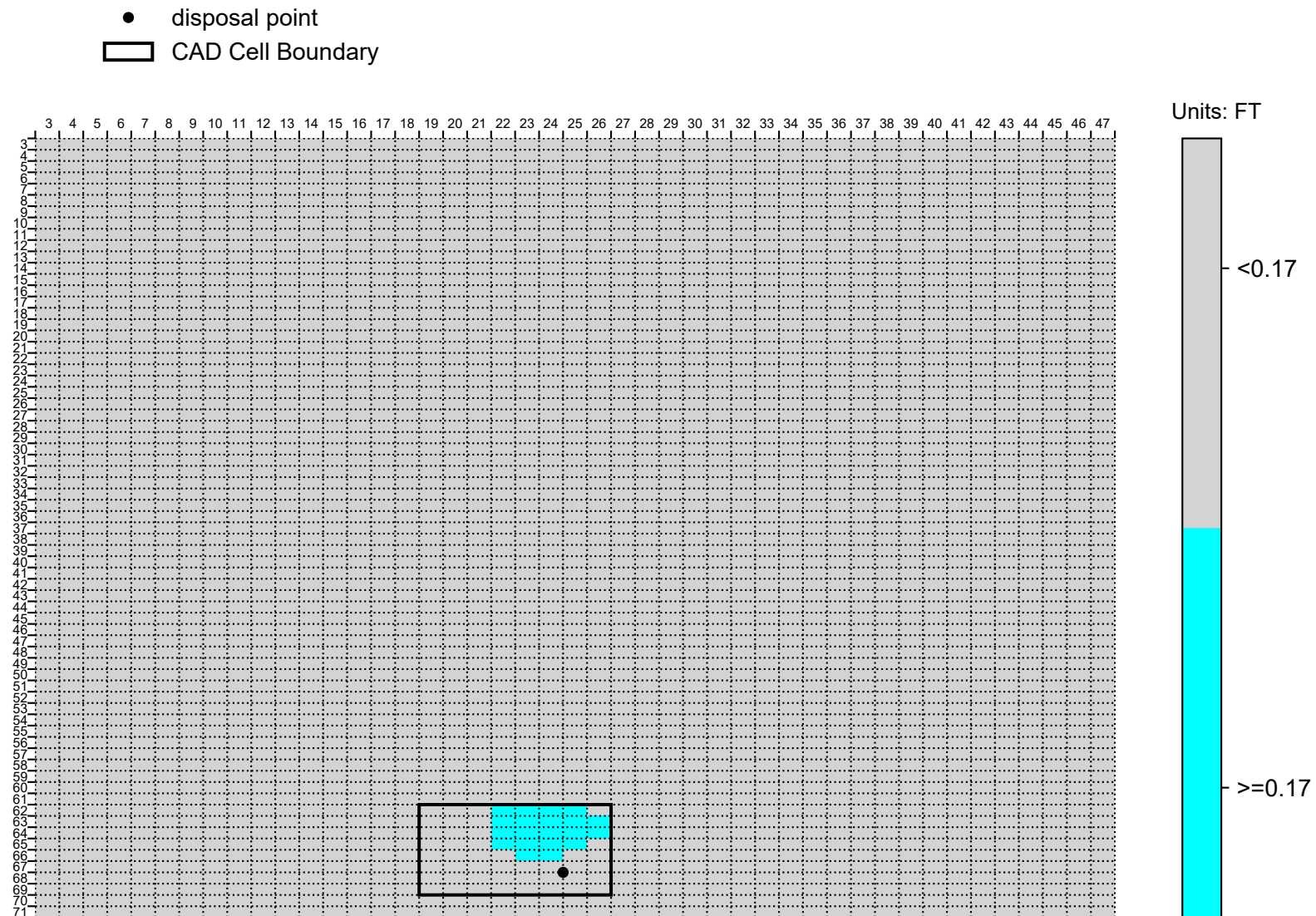
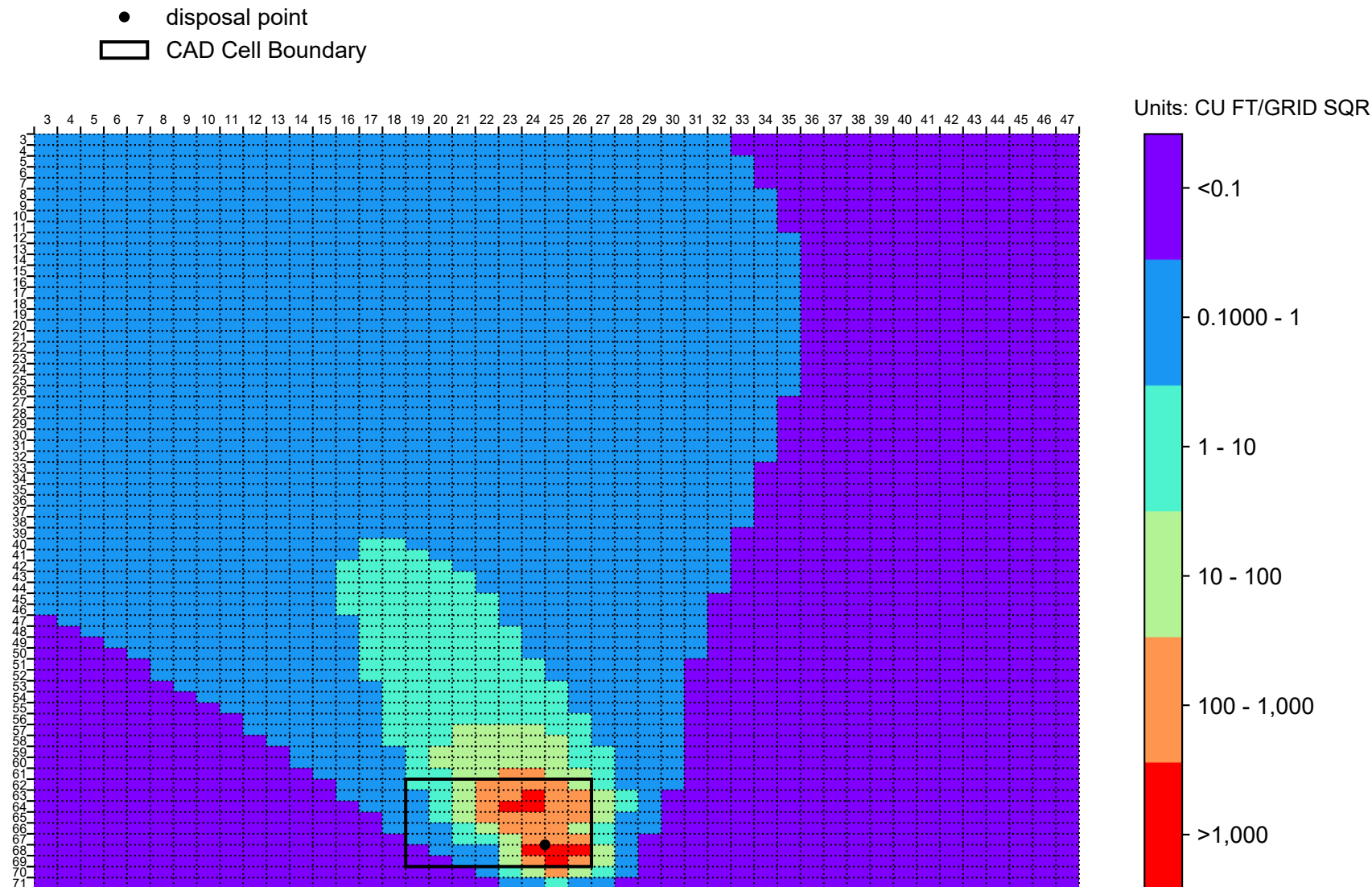


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_4.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 907.72
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 910.00
 Total Lost (cu/yd) = 2.28
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 359.48

Total Accumulated Material WITHIN Boundary (cu/yd) = 829.94
 Total Lost (cu/yd) = 80.06
 Percent Material Outside Boundary (%) = 8.80
 f value = 0.455

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_5C.duo



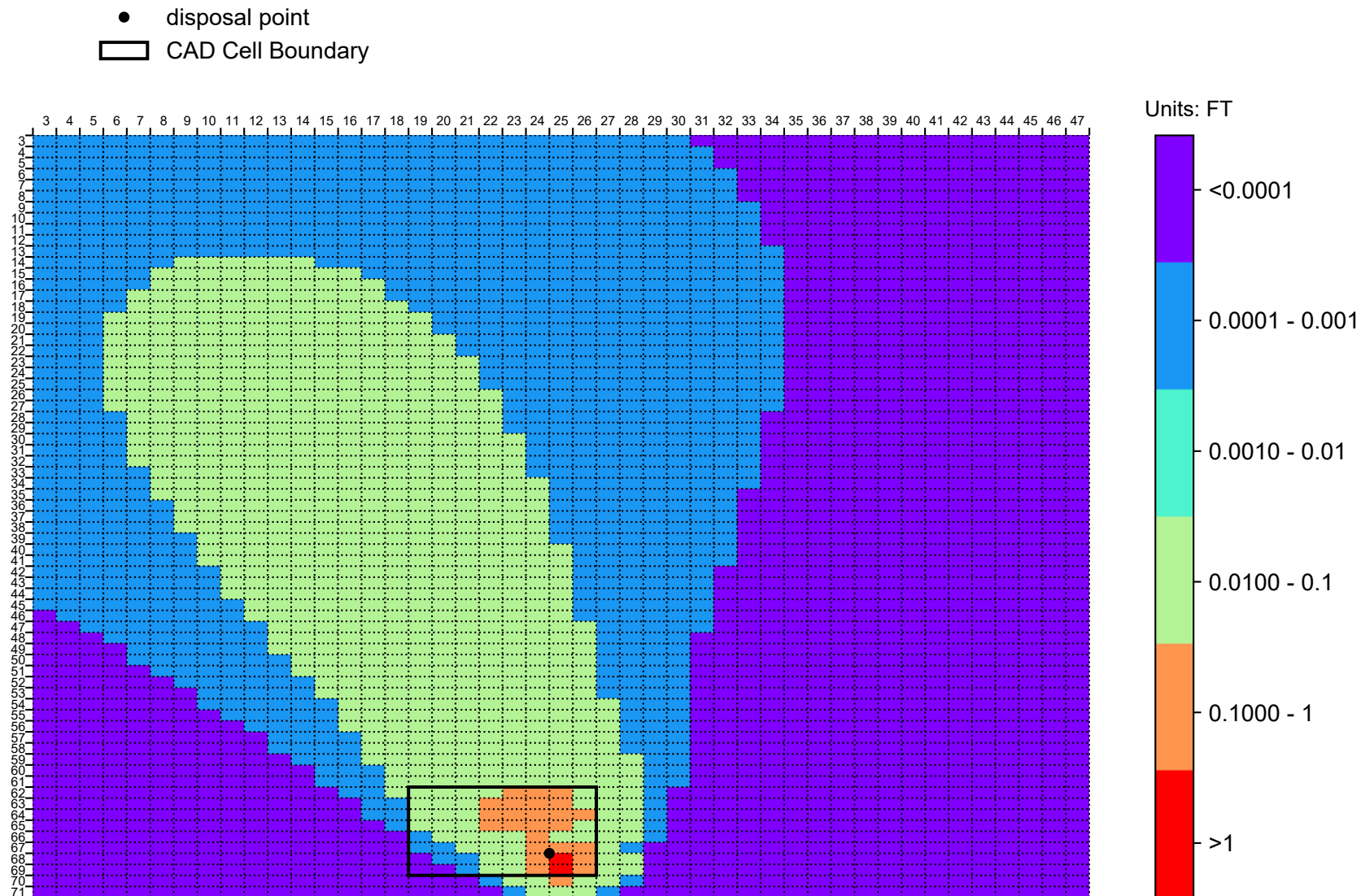


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_5C.duo

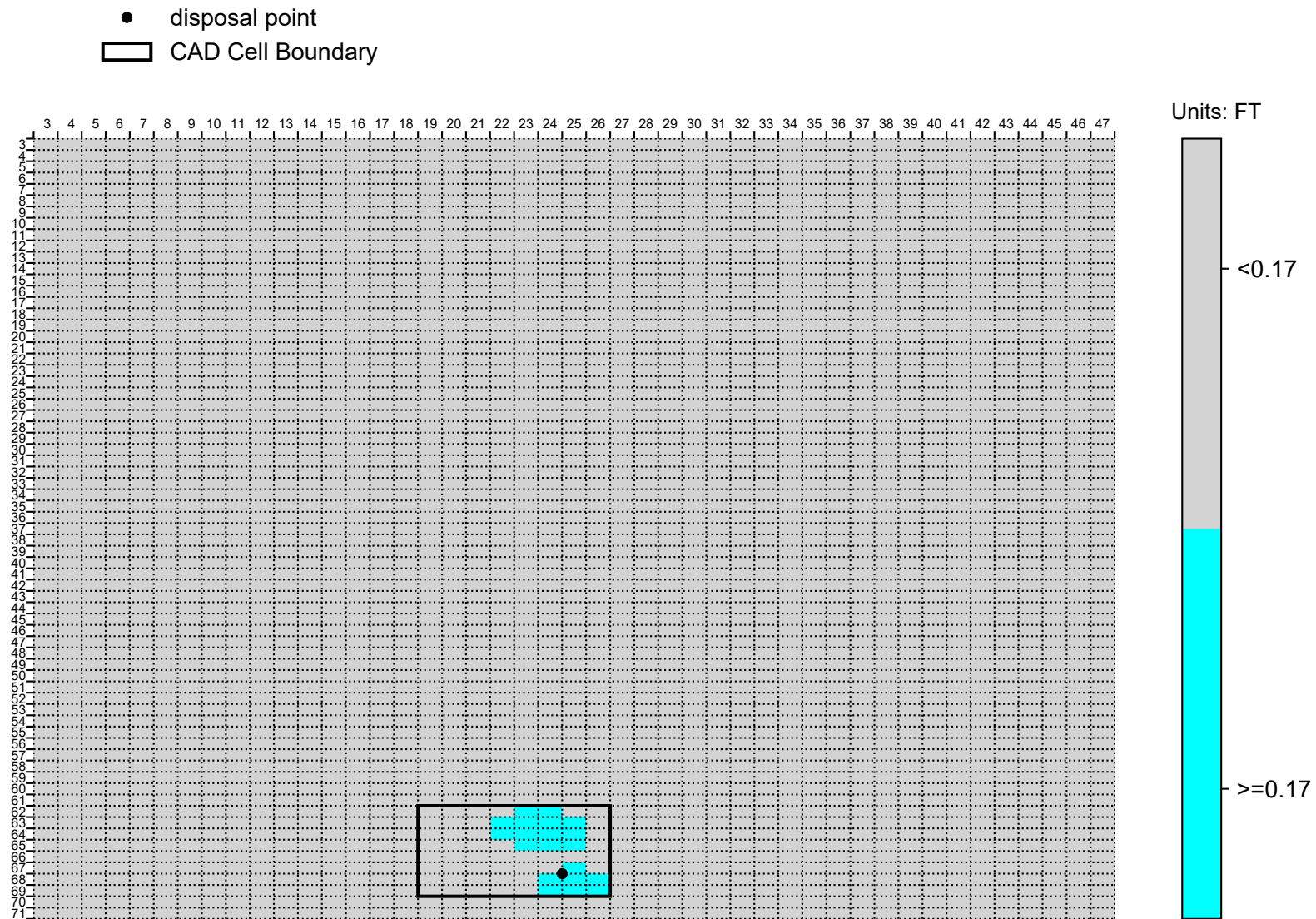
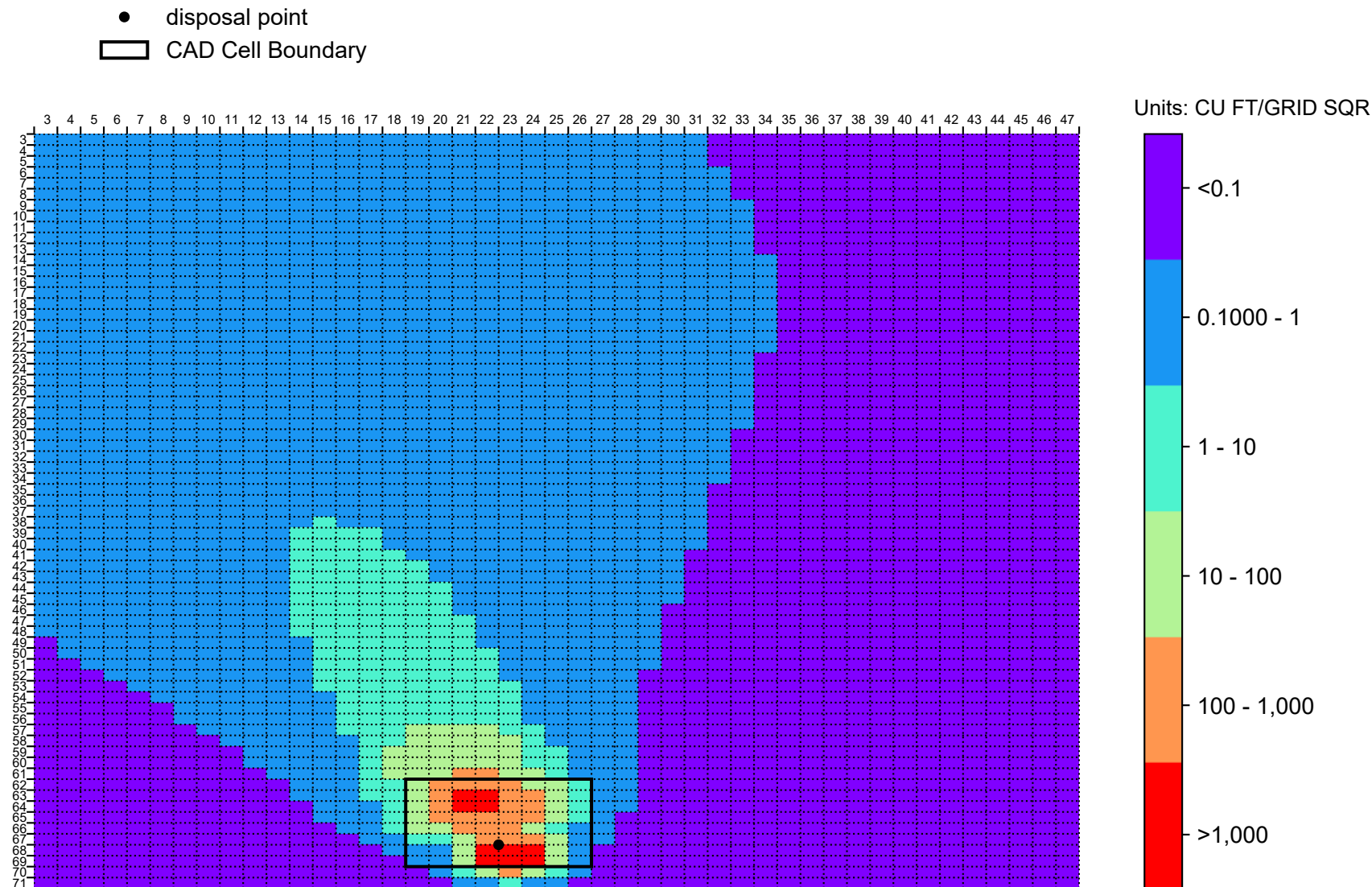


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point X at [67,24]. Results are adjusted to include multiplier.

Source: LNBCAD_XFNP_5C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1079.54
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1084.00
 Total Lost (cu/yd) = 4.46
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 407.01

Total Accumulated Material WITHIN Boundary (cu/yd) = 1001.09
 Total Lost (cu/yd) = 82.91
 Percent Material Outside Boundary (%) = 7.60
 f value = 0.542

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.
 Source: LNBCAD_YFNP_1C.duo



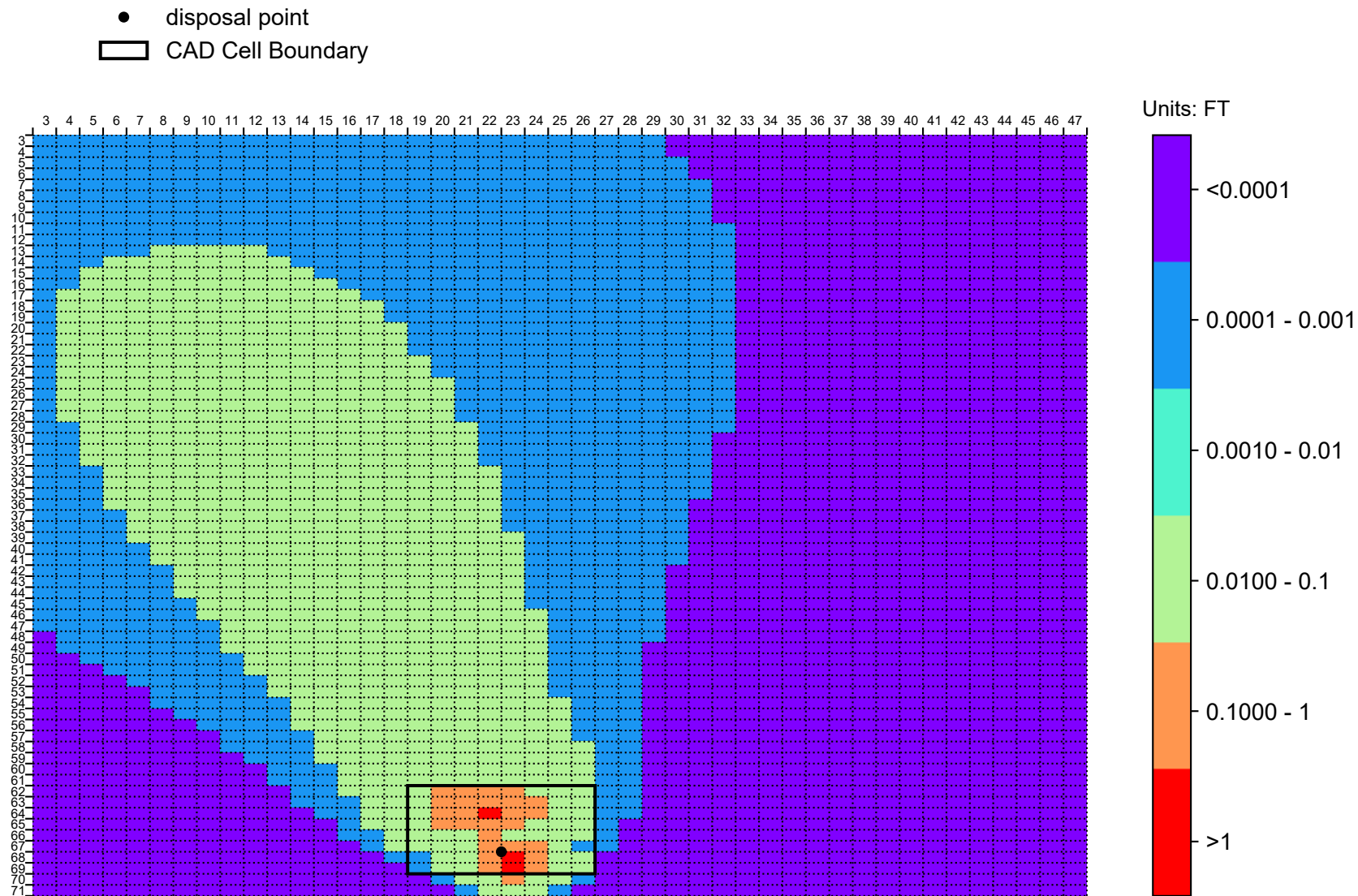


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_1C.duo

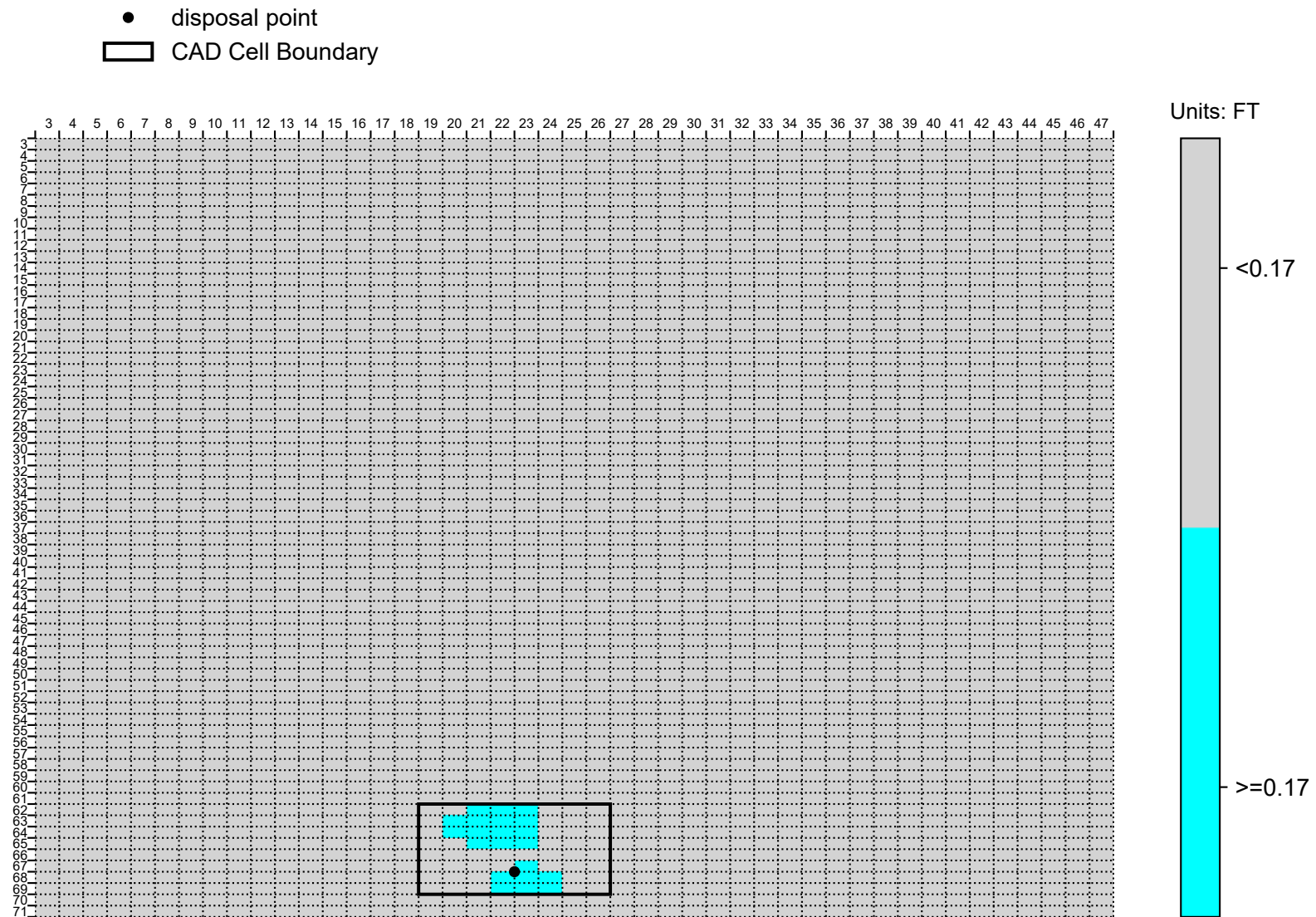
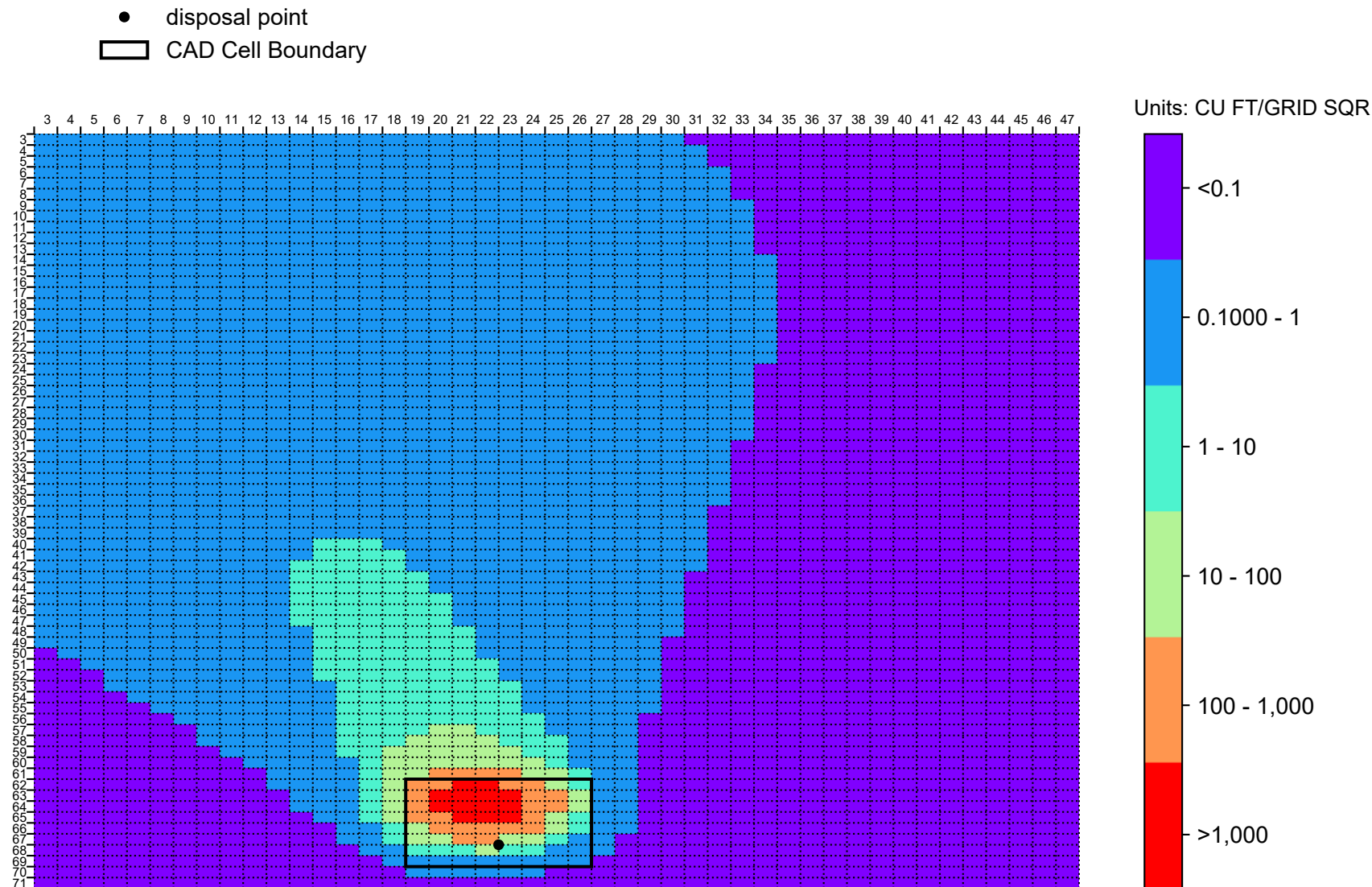


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_1C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1430.30
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1434.00
 Total Lost (cu/yd) = 3.70
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 14.23

Total Accumulated Material WITHIN Boundary (cu/yd) = 1335.09
 Total Lost (cu/yd) = 98.91
 Percent Material Outside Boundary (%) = 6.90
 f value = 0.717

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.
 Source: LNBCAD_YFNP_2.duo



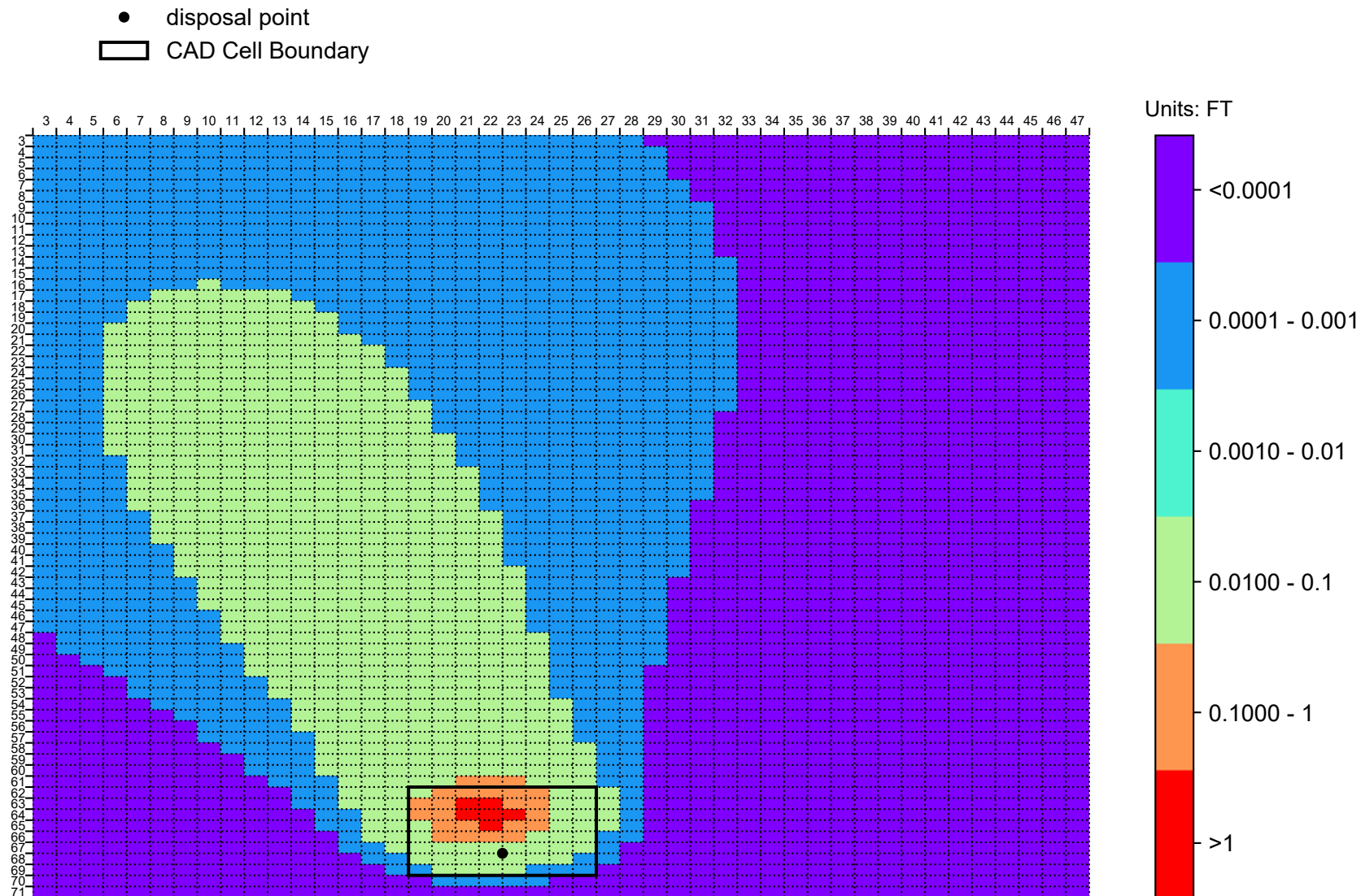


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_2.duo

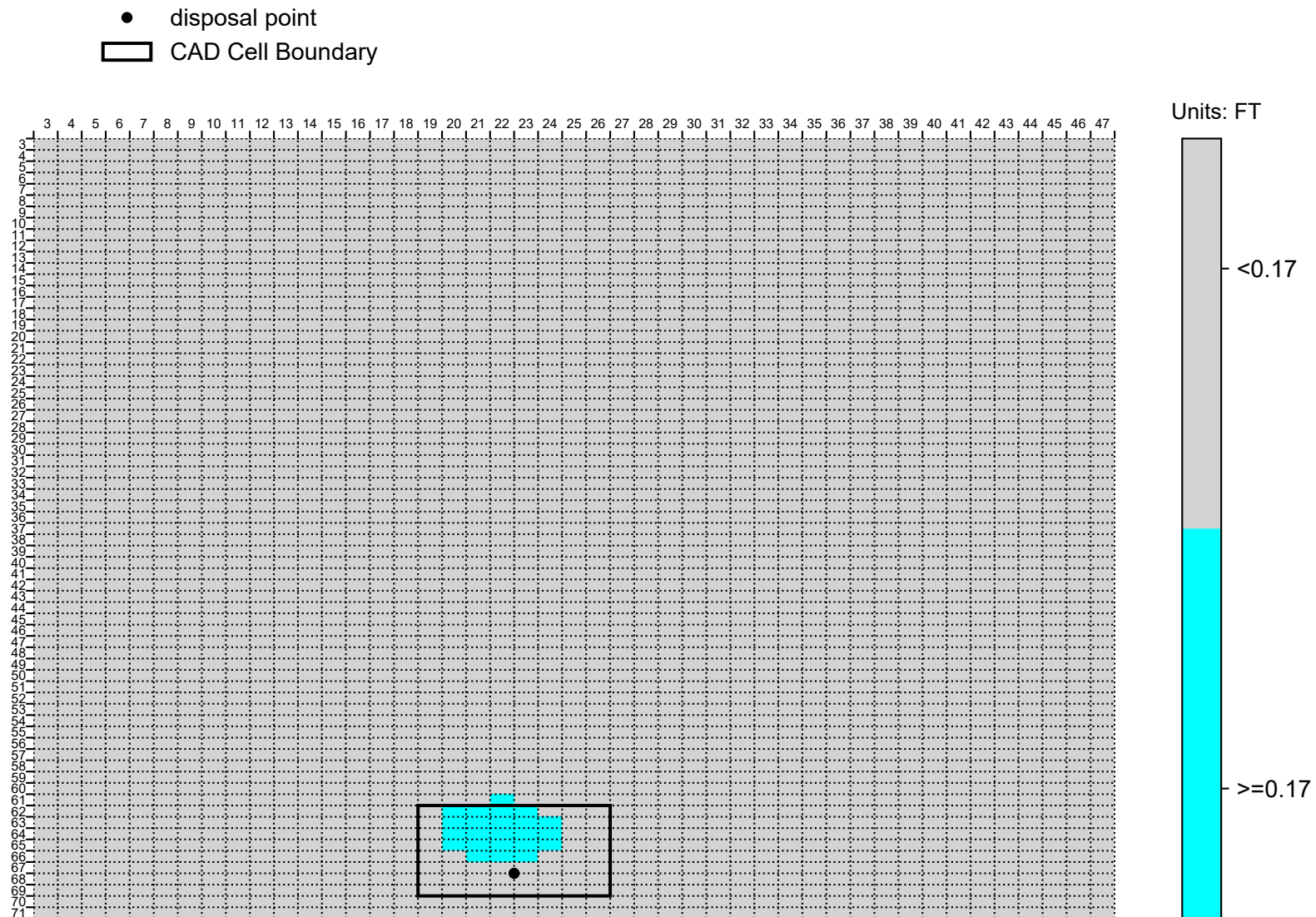
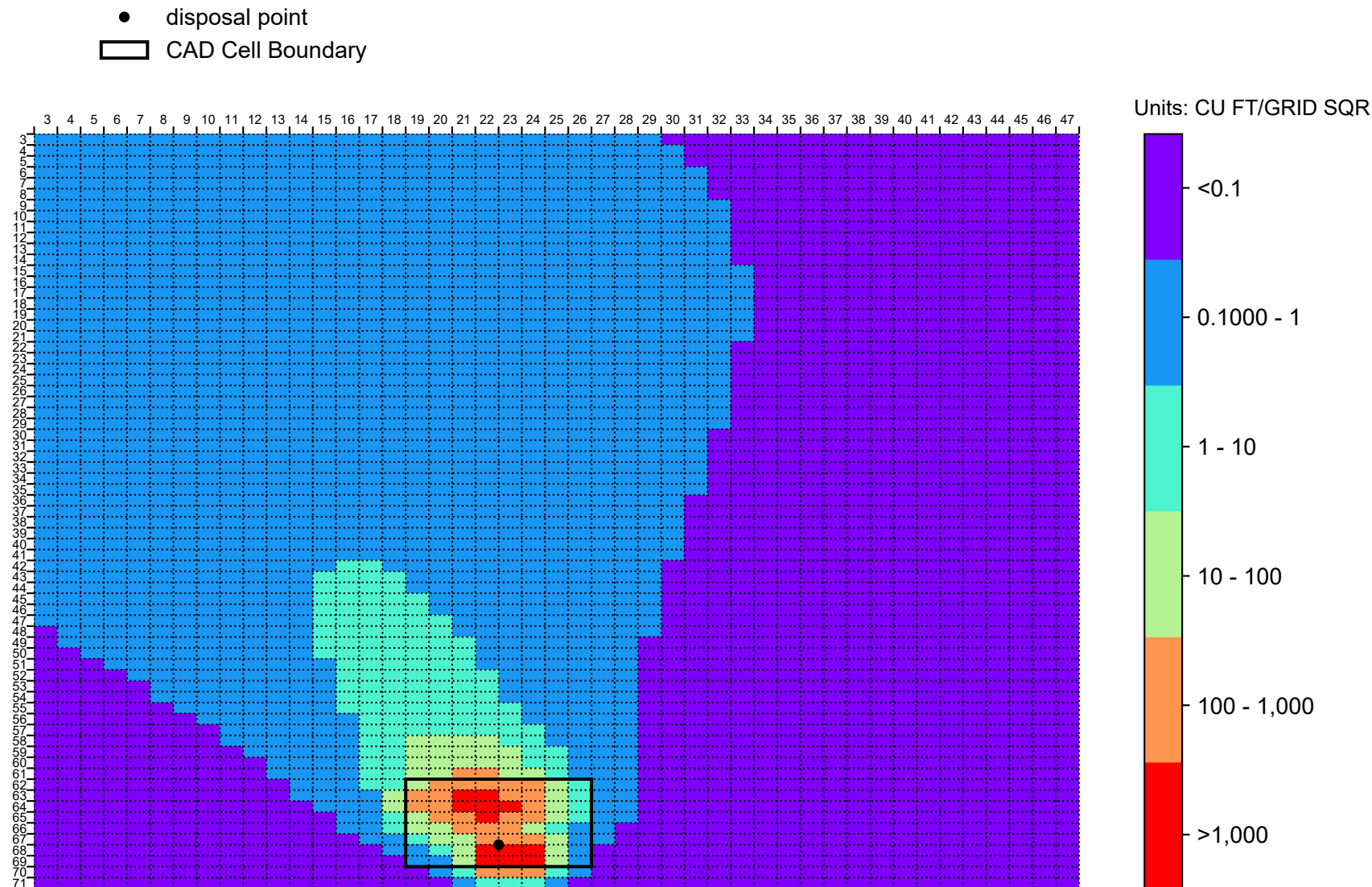


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_2.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1313.15
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1316.00
 Total Lost (cu/yd) = 2.85
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 521.49

Total Accumulated Material WITHIN Boundary (cu/yd) = 1241.72
 Total Lost (cu/yd) = 74.28
 Percent Material Outside Boundary (%) = 5.60
 f value = 0.658

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_3C.duo



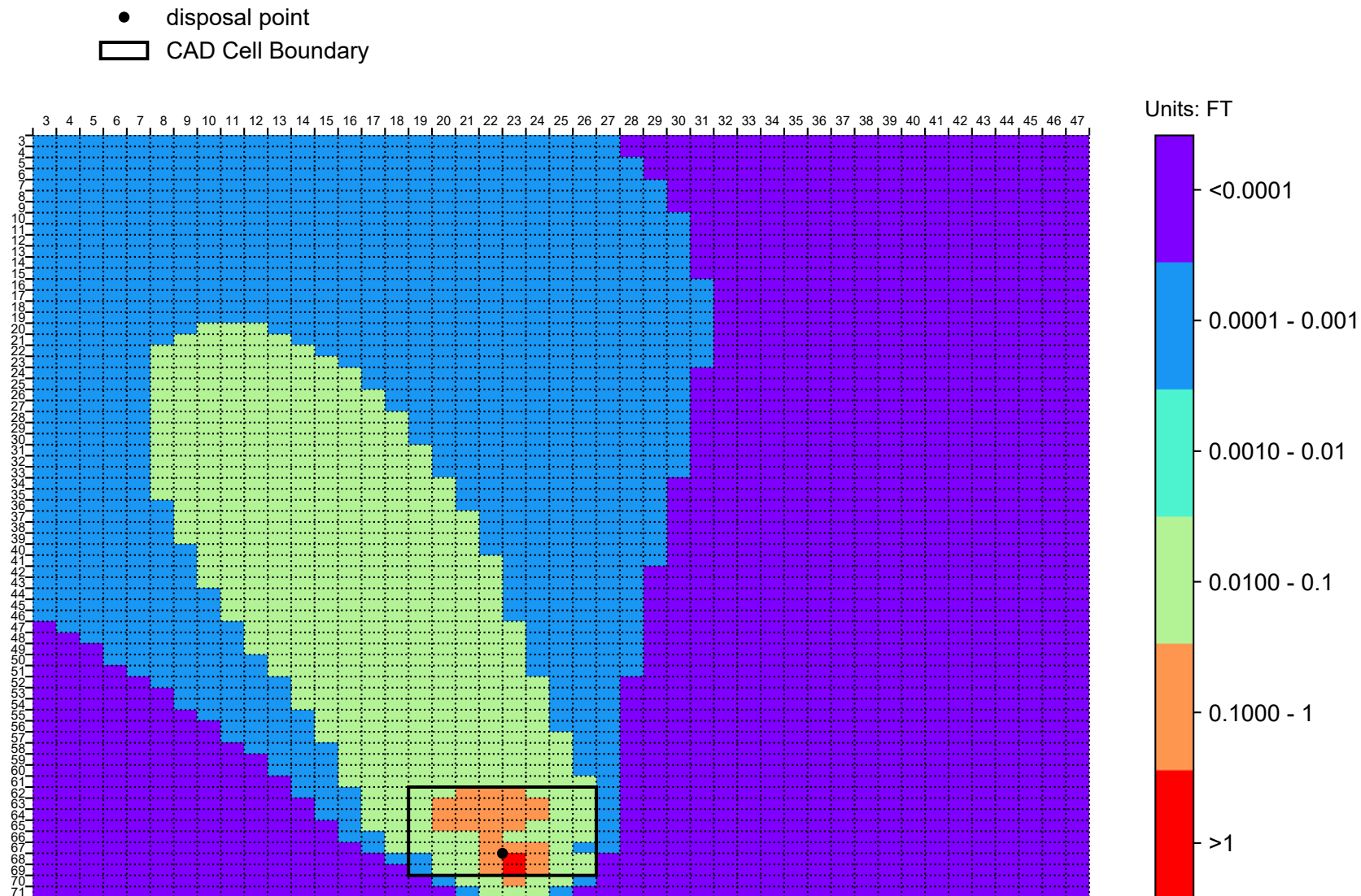


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_3C.duo

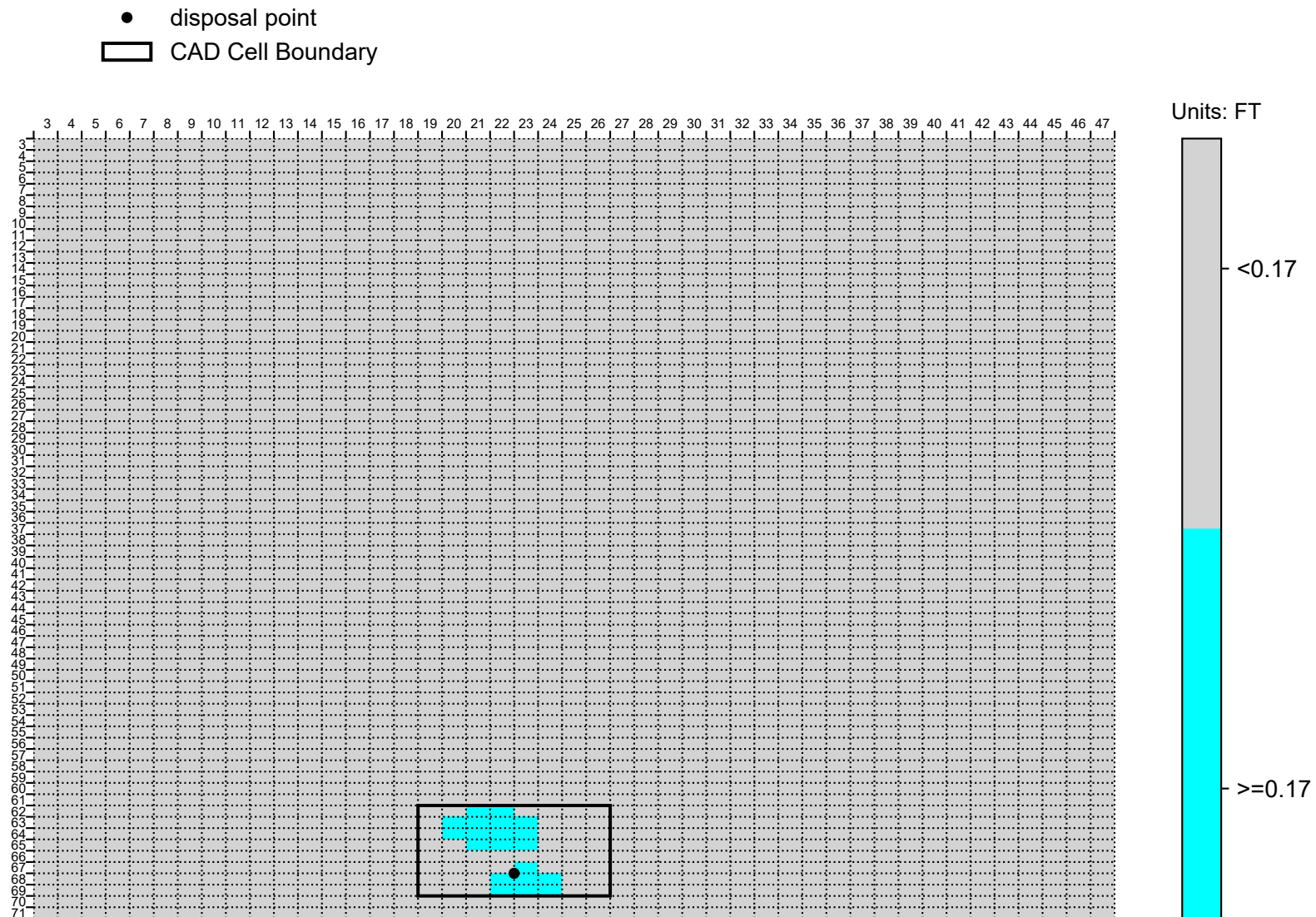
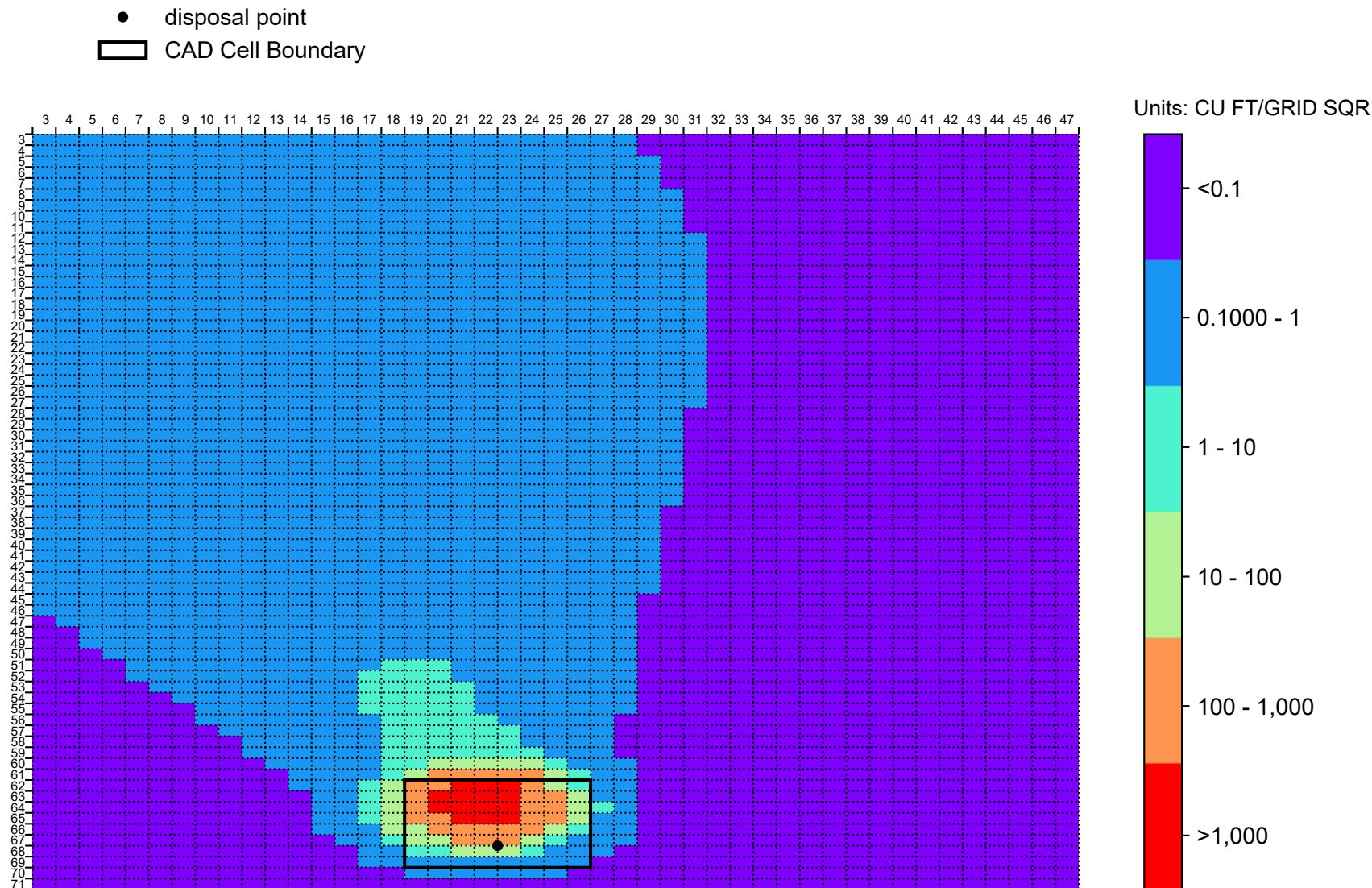


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_3C.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 1648.46
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 1648.00
 Total Lost (cu/yd) = 0.00
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 18.71

Total Accumulated Material WITHIN Boundary (cu/yd) = 1570.30
 Total Lost (cu/yd) = 77.70
 Percent Material Outside Boundary (%) = 4.70
 f value = 0.824

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.
 Source: LNBCAD_YFNP_4.duo



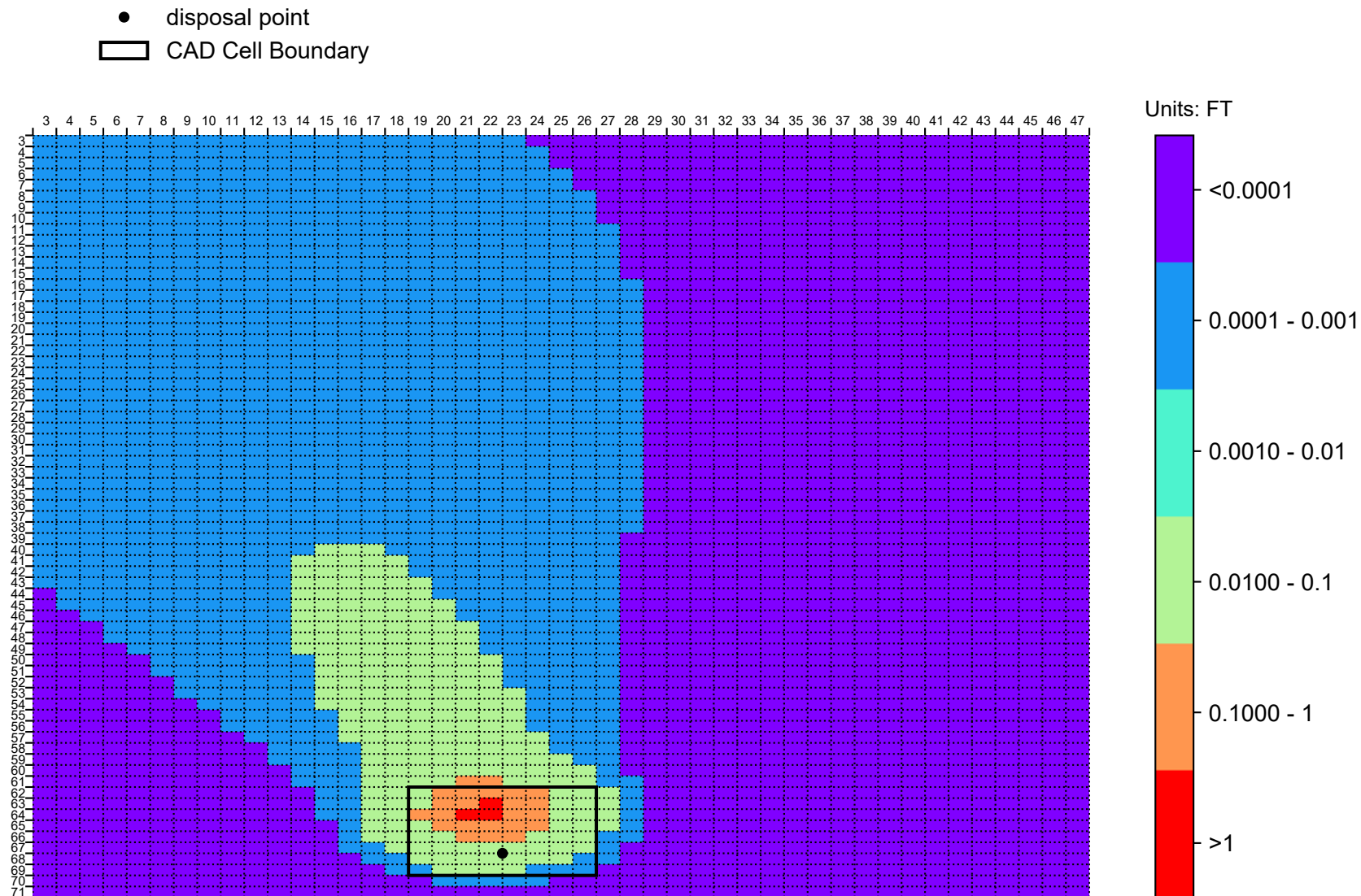


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_4.duo

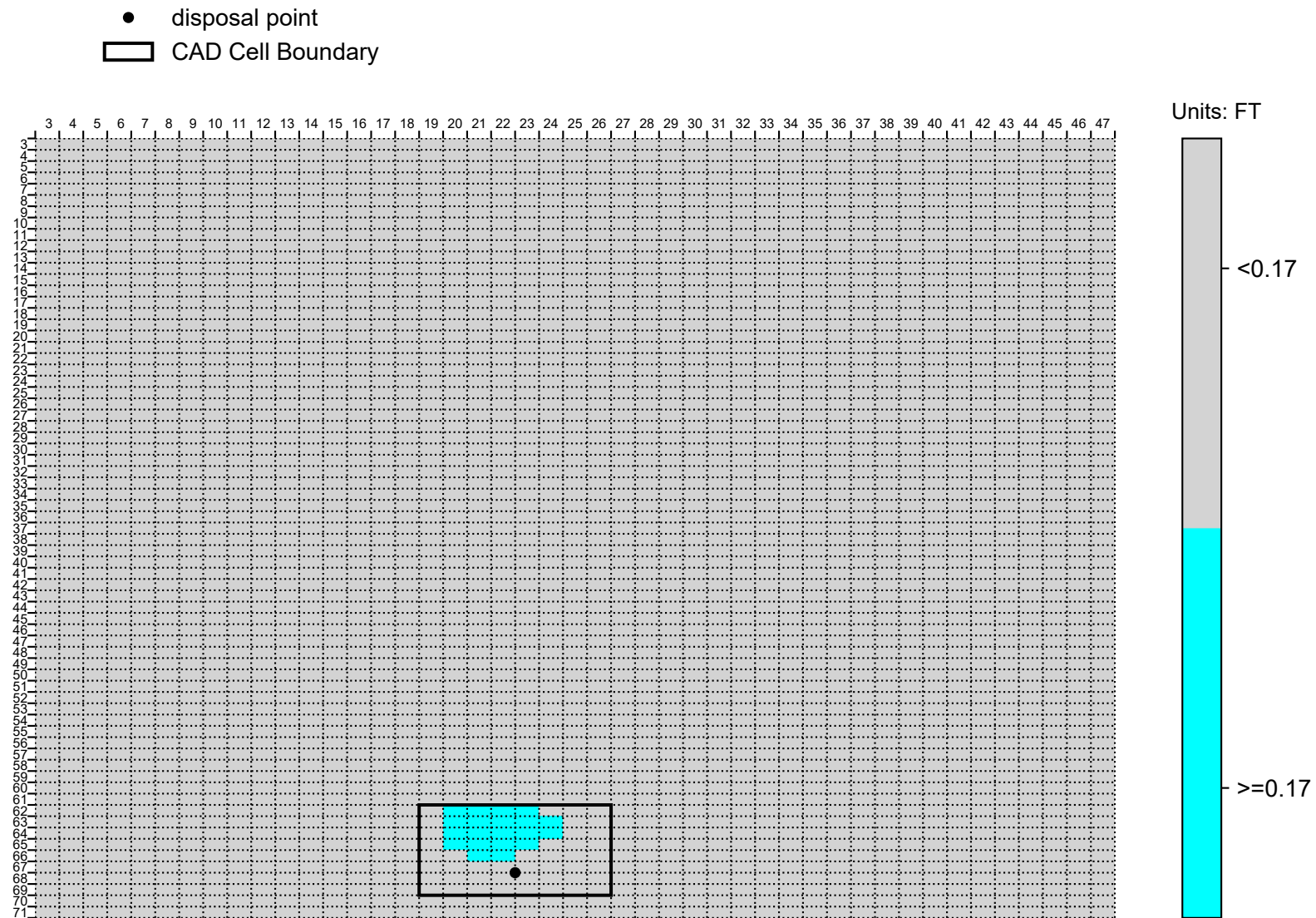
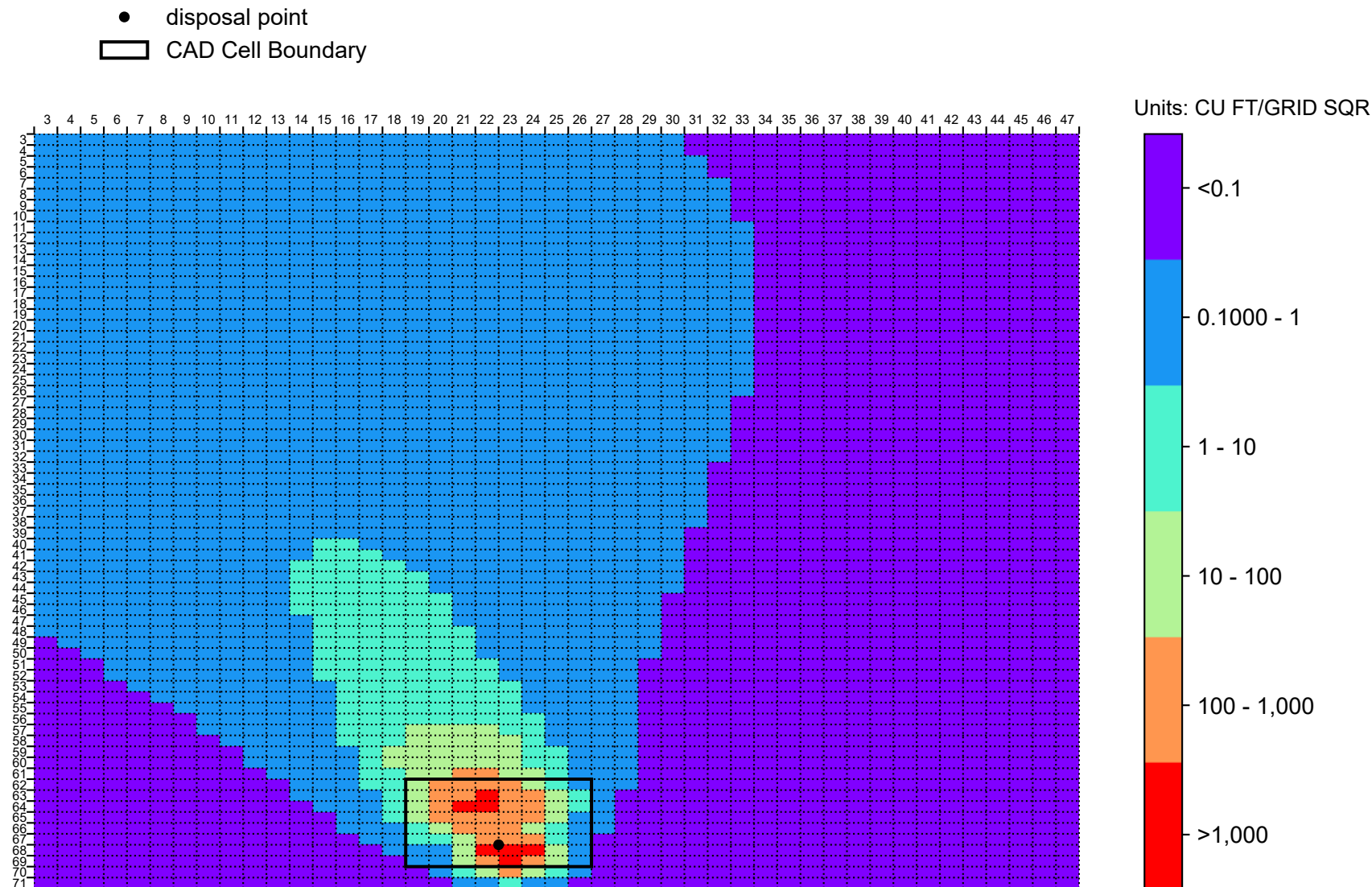


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_4.duo



Total Accumulated Material on STFATE model grid (cu/yd) = 907.50
 Total placed (cu/yd) = 2000.00
 Total solids placed (cu/yd) = 910.00
 Total Lost (cu/yd) = 2.50
 Accumulated Material in a 5x5 grid centered on the disposal point (cu/yd) = 359.48

Total Accumulated Material WITHIN Boundary (cu/yd) = 835.23
 Total Lost (cu/yd) = 74.77
 Percent Material Outside Boundary (%) = 8.20
 f value = 0.455

Figure 1

Plot of TOTAL ACCUMULATED SOLID VOLUME ON BOTTOM (CU FT/GRID SQR)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_5C.duo



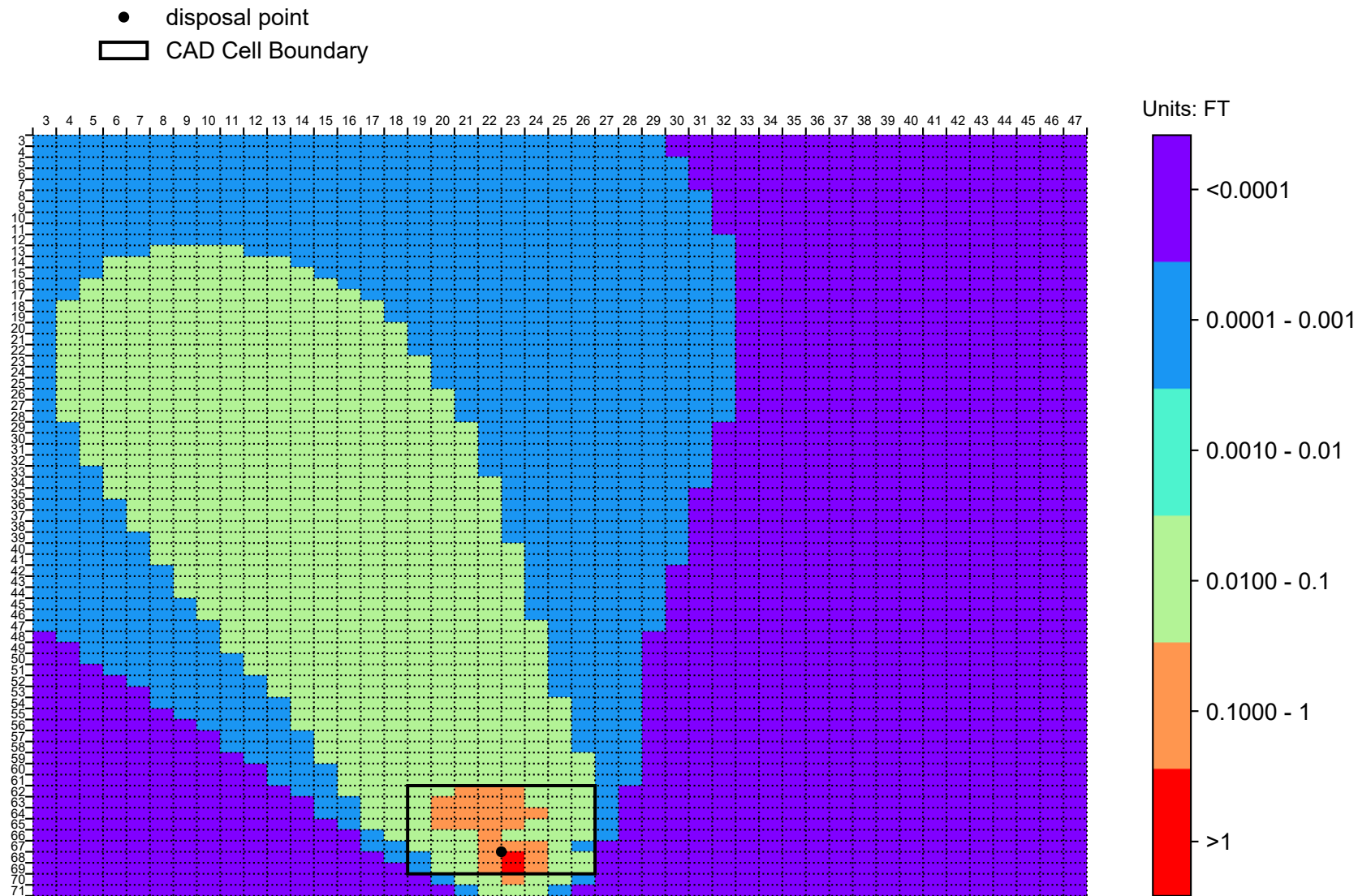


Figure 2

Plot of TOTAL THICKNESS (FT) OF NEW MATERIAL ON BOTTOM

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_5C.duo

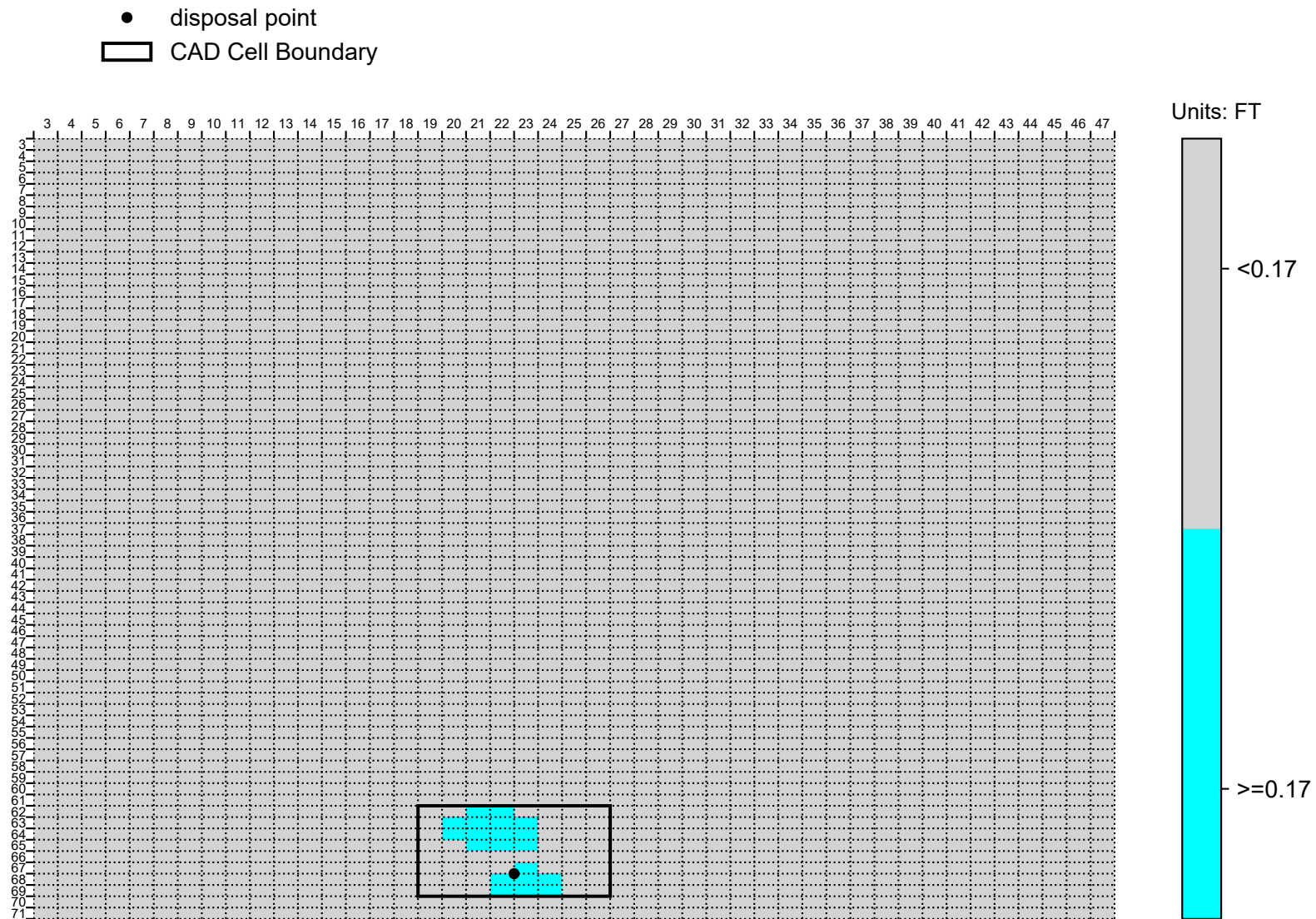


Figure 3

Plot of Deposit Thicknesses Greater than 2 Inches (0.17 ft)

Disposal point Y at [67,22]. Results are adjusted to include multiplier.

Source: LNBCAD_YFNP_5C.duo

Appendix H

Operations, Management, and Monitoring Plan

DRAFT

November 24, 2020
Draft Basis of Design Report
Sediment Dredging and Confined Aquatic Disposal, Lower Newport Bay



Appendix H: Operations, Management, and Monitoring Plan

Prepared for City of Newport Beach

November 24, 2020

Draft Basis of Design Report

Sediment Dredging and Confined Aquatic Disposal, Lower Newport Bay

Appendix H: Operations, Management, and Monitoring Plan

Prepared for

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ABBREVIATIONS

BODR	Basis of Design Report
BMP	best management practice
CAD	confined aquatic disposal
CCC	California Coastal Commission
CEQA	California Environmental Quality Act
CFR	Code of Federal Regulations
City	City of Newport Beach
CWA	Clean Water Act
cy	cubic yard
DGPS	differential global positioning system
DMMT	Dredged Material Management Team
EFH	Essential Fish Habitat
ESA	Endangered Species Act
GPS	global positioning system
NEPA	National Environmental Policy Act
NOAA	National Oceanic Atmospheric Administration
OMMP	Operations, Management, and Monitoring Plan
PCB	polychlorinated biphenyl
RGP 54	Regional General Permit 54
RWQCB	California Regional Water Quality Control Board
T&D	Transportation and Disposal
TBT	tributyltin
TSS	total suspended solid
USACE	U.S. Army Corps of Engineers
USCG	U.S. Coast Guard
USEPA	U.S. Environmental Protection Agency
USFWS	U.S. Fish and Wildlife Service
WDR	Waste Discharge Requirement

1 Project Overview

The City of Newport (City) and the U.S. Army Corps of Engineers (USACE) are responsible for maintaining authorized navigation depths in different parts of Lower Newport Bay Federal Channels (herein referred to as Federal Channels). Combined, approximately 106,900 cubic yards (cy) of material unsuitable for open ocean disposal requires dredging from the Federal Channels by the City and USACE. Working closely with the agencies and the USACE, the City has elected to design a confined aquatic disposal (CAD) facility within the Federal Channels (between Lido Isle and Bay Island) to chemically isolate this material (Figure H-1). This Operations, Management, and Monitoring Plan (OMMP) has been developed to present the City's planned approach for managing the site as a disposal facility for use by the City and USACE during a phased dredging project. Included in this document are the following elements:

- Overview of the OMMP objectives and establishment and proposed CAD project
- Discussion of associated regulatory permits needed for creation and operation of the disposal facility
- Planned operation and communication process for site use
- Presentation of an environmental monitoring program
- Proposed annual reporting details
- Discussion of contingency plans to address unexpected construction issues or long-term stability should they become a concern

2 OMMP Objectives

The primary objective of the City's CAD facility OMMP is to describe the plan for managing the CAD facility as a disposal site for sediments unsuitable for open ocean disposal during a phased, multi-user project conducted by the City and USACE. This document discusses the administrative steps and physical process of placing the material into the CAD facility, covering (or capping) it with clean material to prevent the release of contaminants, and the details of an ongoing and long-term monitoring program to monitor for potential environmental impacts associated with the project.

The purpose of the OMMP is to provide the construction and monitoring framework through which the City and USACE will conduct the disposal of their dredged material. The OMMP describes the conditions for use of the CAD facility; for example, the OMMP requires that specific, identified best management practices (BMPs) are employed during disposal and capping activities (see Sections 6.3 and 6.4), and that the City employ short- and long-term monitoring activities (see Section 7).

The CAD facility would be managed by the City, under the terms and conditions of the OMMP and would be permitted by the regulatory and resource agencies as an approved disposal location for a phased, multi-user project. In this way, the disposal site would be permitted for use, the conditions for use would be known in advance of dredging, and the City would be responsible for ensuring that the framework established by this OMMP is followed. Documentation of the regulatory agency decision-making process and environmental analyses that leads to approval of the CAD facility as an acceptable disposal alternative is currently under way. Results from the City's Environmental Impact Report, currently being conducted in compliance with the California Environmental Quality Act (CEQA), and agency permits and special conditions will augment this OMMP as appropriate.

3 Establishment of the OMMP

3.1 Legal Authority and Responsible Party

The City is financially responsible for constructing the CAD facility. Following completion, the City will assume responsibility for the long-term management of the CAD facility, which includes the following components:

- Pre- and post-disposal monitoring of the CAD facility
- On-site monitoring of all disposal and capping operations within the CAD facility including the disposal and capping operations for sediments within Lower Newport Bay but outside the Federal Channels that are not suitable for open ocean disposal under the City's Regional General Permit 54 (RGP 54) program
- Design of the final isolation cap placed on the surface of the CAD facility at the conclusion of all disposal operations
- Preparation of monitoring reports for the regulatory agencies that document compliance with this OMMP

Specific staff and departments responsible for these management operations include the following:

- Dave Webb, Public Works Director, City of Newport Beach
- Chris Miller, Public Works Manager, City of Newport Beach
- Adam Gale, Managing Planner, Anchor QEA, LLC
- Steve Cappellino, Principal Scientist, Anchor QEA, LLC
- Michael Whelan, Principal Engineer, Anchor QEA, LLC

3.2 Modifications of the OMMP

This OMMP has been developed as a "working document" and may require modification during the operation and monitoring phases of the CAD facility development. Final modification of the plan is at the discretion of the City, in consultation and consensus with the USACE, U.S. Environmental Protection Agency (USEPA), California Coastal Commission (CCC), and California Regional Water Quality Control Board (RWQCB).

If modifications to the OMMP are required, addenda sheets will be issued to each party that is involved. The addenda sheets will clearly identify the addendum number, date of the revision, and where the addenda sheet is to be placed in the OMMP. Additionally, the plan identification number for each plan holder will be shown. These sheets can be inserted into the plan (via a 3-ring binder) in the appropriate section. A list of the names of all of plan holders and their plan identification numbers will be compiled and maintained. This list will be used to ensure that all addenda are distributed to every plan holder. All addenda will be distributed with return receipt requests to ensure that all plan holders receive all addenda.

4 CAD Facility Description

The proposed project entails creation of a CAD facility within the Federal Channels (Figure H-1) as a solution for sediments dredged from within and outside the Federal Channels that are unsuitable for open ocean disposal. Specifically, the project involves excavating a CAD facility between Lido Isle and Bay Island to accommodate the total volume of sediment previously determined to be unsuitable for open ocean disposal under the Federal Channels maintenance dredging program as well as additional capacity for sediments outside the Federal Channels that are not permitted under the City's RGP 54 permit.

Bay deposits excavated to create the CAD facility will be dredged and disposed with a bottom-dump barge at an open ocean disposal site (e.g., LA-3). Clean sand that is dredged to create the CAD facility would be disposed of with bottom-dump barges at a predefined nearshore placement area in Newport Beach, located immediately north of the Entrance Channel. Subsequently, sediments unsuitable for open ocean disposal from the Federal Channels (Main Channel 1, Main Channel 2, Turning Basin, and Newport Channel 1) would be dredged using mechanical equipment and placed within the CAD facility using a bottom-dump barge.

These sediments would then be covered with an interim cover containment layer of clean sediments dredged from the Federal Channels that is suitable for open ocean disposal (e.g., Newport Channel 3), as part of USACE's maintenance dredging program. The clean interim cover containment layer will be 1 foot thick. The City will provide public and private entities opportunities prior to and after the placement of the interim cover containment layer to place additional sediments from outside the Federal Channels. The CAD facility has been designed to accommodate an additional 50,000 cy of capacity for this material. If the final elevation for this layer is achieved prior the completion of the negotiated time period of disposal, the City will close the CAD facility for disposal and place a 3-foot-thick, clean final cap to chemically isolate the underlying sediments from burrowing organisms and biota residing in the overlying water column under long-term scenarios. If 50,000 cy of material from public and private participants is not achievable within the negotiated time period of disposal, the City will close the CAD facility for disposal and place a 3-foot-thick, clean final cap, thus leaving the final elevation of the CAD facility lower than originally designed.

Since the final cap will be placed after completion of the Federal Channels maintenance dredging program, sourcing of this layer will need to be finalized by the City. For modelling purposes, the Entrance Channel, Newport Channel 2, Newport Channel 3 was used due to its low chemical properties and higher sand content, making it ideal candidates for the final cap for the CAD facility. Also, shoaling is most prevalent within the Entrance Channel, which makes it good candidate for additional maintenance dredging in the future. If the City elects to source the final cap from another location, the City should meet or exceed the material properties of the Entrance Channel, Newport

Channel 2, and Newport Channel 3 to closely match the chemical isolation results described in Appendix D of the Draft Basis and Design Report (Draft BODR).

Since the CAD facility is located within the Federal Channels, the top of slope for the CAD will range between -15 to -17 feet mean lower low water (MLLW) depending on whether the selected contractor elects to dredge the full allowable overdredge. Regardless, the CAD facility has been designed to accommodate the possibility of dredging the Bay Island area deeper in the future to match the authorized depth in the adjacent Main Channel 3 (-20 feet MLLW). Thus, the final elevation of the final cap is designed to a -22 feet MLLW elevation to accommodate for future deepening to -20 feet MLLW and 2 feet of allowable overdredge. The bottom of the CAD is designed to -45 feet MLLW plus 1 foot of allowable overdredge. Further details on dimensions and estimated volumes are included in the Draft BODR. It is anticipated that most of this material will be suitable for nearshore placement, whereas the top 2 feet of material may require disposal at an open ocean disposal site (e.g., LA-3). Testing of the sediments during dredging may be required to determine suitability.

Geotechnical investigations near the proposed CAD facility location (see Appendix F of the Draft BODR) were used to conduct geotechnical analysis on the CAD facility. Additional sediment cores conducted within the CAD facility (see Appendix F of the Draft BODR) provided additional evidence on the extent of bay deposits within the location of the CAD facility. Subsurface materials in the CAD location largely consist of soft clayey silt underlain by poorly graded to fine dense sand. Figure H-2 shows a typical cross section through the CAD facility.

5 Permitting Requirements

This section discusses applicable state and federal permits required for construction, operation, and management of the Lower Newport Bay CAD facility. The anticipated regulatory framework for disposal of dredged material in the CAD facility includes multiple permits obtained by the City to authorize construction and operation of the CAD facility.

5.1 Activities Requiring Permits for Disposal

Regulations governing dredging and discharge of marine sediments, and subsequent capping include the following:

- National Environmental Policy Act (NEPA)
- CEQA
- Clean Water Act (CWA) Section 404 and Rivers and Harbors Act Section 10 under the jurisdiction of the USACE
- Coastal Development Permit under the jurisdiction of the CCC
- CWA Section 401 and Porter-Cologne Waste Discharge Requirements (WDRs) under the jurisdiction of the RWQCB
- Endangered Species Act (ESA) consultations for federally listed species under the authority of the U.S. Fish and Wildlife Service (USFWS) and National Oceanic Atmospheric Administration (NOAA) Fisheries
- Magnuson-Stevens Fishery Conservation and Management Act consultations for Essential Fish Habitat (EFH) under the jurisdiction of NOAA Fisheries
- Surface Lease Agreement under the jurisdiction of the State Lands Commission

The City anticipates obtaining all necessary regulatory permits to construct and operate the CAD facility as a multi-user, multiphase project disposal facility for sediments unsuitable for open ocean disposal from within and outside the Federal Channels in Lower Newport Bay. Expected authorizations include WDRs from the RWQCB and a Federal Consistency Determination from the CCC. The City will also request a standard individual permit from the USACE Regulatory program for discharges of dredged material into the CAD facility and nearshore placement in Newport Beach, California, and work in navigable waters. The City will prepare permit applications to the USACE, RWQCB, and CCC to obtain permission to dredge the material and to use the CAD facility as a disposal site. The Federal Channels maintenance dredging program would prepare analogous environmental documents for their maintenance dredging and disposal within the CAD facility.

5.2 Permit Application Process

As described above, the City will obtain all necessary permits to construct and operate the CAD facility. The City will also obtain all permits to dredge and transport material unsuitable for open

ocean disposal within the Federal Channels to the CAD facility. Individual permits will be required during the second phase of the project for dredged material outside the Federal Channels.

The proposed dredging, CAD facility construction, and site management activities must demonstrate compliance with the requirements of NEPA, CEQA, ESA, and CWA Section 404. The USACE and other permitting agencies will require the results of the physical and chemical testing of the dredged material as well as the most recent bathymetric survey of the CAD facility.

The regulatory and permitting agencies will likely require the City to employ designated BMPs and operational controls and conduct short-term monitoring during placement within the CAD facility of sediments unsuitable for open ocean disposal (within the Federal Channels and outside the Federal Channels) and during capping operations. Therefore, the City will likely be required to comply with one or more operational and/or institutional controls (e.g., BMPs) to minimize water quality impacts to Lower Newport Bay.

6 OMMP Communications Plan and Operating Requirements

This section addresses the operational conditions set forth for disposal and capping procedures at the CAD facility. The CAD facility will be designed with enough capacity for the unsuitable material dredged within the Federal Channels, 50,000 cy of material dredged within Lower Newport Bay but outside the Federal Channels, a 1-foot-thick interim cover containment layer, and a 3-foot-thick final cap (see Draft BODR for additional details). Furthermore, CAD facility construction and placement of material within the CAD facility will be restricted by an evaluation of whether the activities constitute the Least Environmentally Damaging Practicable Alternative according to the USEPA 404(b)(1) guidelines.

6.1 Communication Plan

6.1.1 *Pre-Disposal Planning*

The two parties proposing to use the CAD facility (City and USACE) have conducted detailed coordination throughout the project development phase and developed the technical requirements for all pre- and post-construction activities at the site. Bulk physical and sediment chemistry analyses in accordance with state and USACE permit requirements have been performed by the City on candidate material within the Federal Channels. Based on these detailed analyses, a determination of sediment suitability with the Dredged Material Management Team (DMMT) in August 2019 has concluded material in Main Channel 1, Main Channel 2, Turning Basin, and Newport Channel 1 is not suitable for open ocean disposal and therefore suitable for placement in the CAD facility (Figure H-3). Engineering design for the CAD facility including disposal and capping elements are at approximately 30% complete at this time and are thus sufficiently developed for the agency permit application process.

A pre-project planning meeting will be held at least 1 week prior to initiation of construction and disposal operations to discuss the schedule and logistics of the planned activities. Specific topics of discussion for the pre-project planning meeting include the following:

- Identify points of contact for all parties involved in the project including emergency contact numbers for the City, USACE, and City Representatives
- Review the construction specifications and anticipated project schedule
- Review the environmental monitoring requirements for the project, if applicable, and contact numbers for field sampling staff
- Review health and safety requirements and communication between field contractors
- Discuss reporting requirements for the project

6.2 Disposal and Capping Operations

6.2.1 *Schedule*

A conceptual schedule for CAD facility construction, dredged material placement and subsequent capping operations for the facility has been developed (Figure H-4).

6.2.2 *Navigation and Safety Requirements*

The users of the CAD facility must exercise every precaution to prevent accidents and injury to themselves or others when operating within the boundaries of the facility. This requirement extends to all persons entering and working around the CAD facility including, but not limited to, tugboat operators and crew, dredging vessel crew, sampling and surveying crew, and USACE and City field staff.

Vessels transporting material for discharge, including cap material, shall utilize global positioning system (GPS) and automated disposal barge tracking system. The City and USACE will be required to adhere to applicable provisions of the following regulations with regard to navigation, navigational/maritime safety, and worker occupational health and safety:

- U.S. Coast Guard (USCG) requirements, consistent with the office of the Captain of Lower Newport Bay
- 33 United States Code – Navigation and Navigable Waters, including Chapter 34, “Inland Navigation Rules”
- 33 Code of Federal Regulations (CFR) – Navigation and Navigable Waters
- 46 CFR – Shipping
- 29 CFR 1926 – Safety and Health Regulations for Construction
- Other applicable federal, state, and/or local regulations

6.3 Disposal Operations

The City will ensure that dredging contractors maintain contact with the City throughout disposal operations via telephone, radio, and face-to-face conversations. During specific disposal events, environmental monitoring will be performed to identify the levels of total suspended solids (TSS) and chemical contaminants in the water surrounding the CAD facility. Based on the results of environmental monitoring, the City may amend this document to require modification of the disposal operations. Pre- and post-construction monitoring requirements are described in Section 7.

Differential Global Positioning Systems (DGPS) will be employed by all contractors who have authorization to dispose of dredged materials in the CAD facility. If floating debris are expected, the contractors must provide a boat capable of collecting and transporting debris. The City and USACE are responsible for either removing debris from dredged material at dredge sites in their areas of

responsibility or collecting all floating debris after disposal to ensure floating debris are not observed in or around the CAD facility location. If floating debris are observed following disposal, it must be collected and disposed of by the contractors immediately following the disposal event.

A Transportation and Disposal (T&D) Log will be a fundamental component of recordkeeping for permit and disposal activities. The T&D Log will be used to identify basic disposal information and status including owner; equipment and permit information; tug and barge information; loading, transit, and weather information; and specific information about disposal and post-disposal operations. The T&D Log will be completed by the inspector, and a copy will be forwarded to the engineer via email within 24 hours of each day of disposal activities. This will be a component of both phases of the project, including the initial unsuitable material disposal from the Federal Channels and the subsequent disposal activities for material outside the Federal Channels that are not suitable for open ocean disposal under the City's existing RGP 54 program.

6.4 Capping Operations

Cap placement within the CAD facility shall occur via dump barge. Care must be taken to ensure that the material is released in a controlled manner and that the cap is placed as evenly as possible over the site.¹ Contractors barge tracking requirements and progress surveys will be required during the placement of sediments at the CAD facility.

¹ This BMP is recommended to allow for increased bearing capacity of the contaminant surface layer and to minimize the potential for mixing at the interface layer

7 Construction Monitoring and Post-Disposal Requirements

Monitoring of CAD facility's (Port of Hueneme, California and Long Beach, California) have demonstrated that sediments unsuitable for open ocean disposal could be placed into a CAD facility and capped with clean sediments without causing significant environmental impacts to the overlying water column or surrounding sediments. The methods and results of the recently completed 10-year monitoring conducted for the CAD facility at Port Hueneme are being finalized and should be available upon request prior to construction of the Lower Newport Bay CAD facility. Included in that study were field investigations conducted during disposal, immediately after capping, and consecutively for 10 years after construction. The construction monitoring and post-disposal requirements proposed for the Lower Newport Bay CAD facility have been informed by the lessons learned during the Port Hueneme CAD facility study.

7.1 Construction Monitoring

Using the results of the extensive field monitoring conducted at Port Hueneme as a general example of successful disposal and capping operations, construction monitoring for sediments unsuitable for open ocean disposal at the CAD facility will focus on the following two main objectives: 1) ensure that significant quantities of sediments are not deposited outside of the designated CAD facility; and 2) ensure that chemicals in the sediment remain fully isolated and do not affect resident aquatic organisms.

To achieve these objectives, the following field and laboratory parameters will be monitored during and immediately after construction:

- Field operations will be monitored and documented to ensure proper equipment placement prior to disposal and volumes/depths for all material placed into the CAD facility.
- Water column turbidity monitoring shall be conducted on a routine basis at reference and downcurrent locations to assess sediment transport during disposal operations.
- Water column samples will be collected periodically and analyzed for dissolved and particulate metals to monitor for chemical release and transport during disposal operations.
- During dredging, silt curtains may be required to reduce turbidity by isolating the active dredging site from the rest of Lower Newport Bay.
- A bathymetric survey of the CAD facility will be conducted prior to initiation of disposal operations to ensure that it has been constructed to meet the design specifications.
- A bathymetric survey of the CAD facility will be conducted after the sediments unsuitable for open ocean disposal have been placed within the CAD facility to ensure that the material has been placed evenly within the CAD facility.

- A bathymetric survey of the CAD facility will be conducted after the interim cover containment layer is constructed to ensure that the material has been placed evenly and at the proper depth within the CAD facility.
- Bathymetric surveys will be conducted periodically during the disposal operations for sediments unsuitable for open ocean disposal under the City's existing RGP 54 program to ensure that the material has been placed evenly within the CAD facility.
- A bathymetric survey of the CAD facility will be conducted after the final cap is constructed to ensure that the material has been placed evenly and at the proper depth within the CAD facility. If not, the contractor will be required to repair any irregularities.

7.1.1 *Water Quality Monitoring*

Water column monitoring will occur at set distances directly downcurrent of the disposal operations. The proposed downstream sampling distances for each operation will include at a minimum 150, 200, and 250 feet, and the nearest sample will be collected within 15 minutes of the disposal event.

At each station, continuous depth profiles will be collected a minimum of three times per week for light transmission, dissolved oxygen, and conventional field sampling measurements (i.e., salinity, temperature, and pH). Three sample depths (3 feet below the water surface, 1 foot above the bottom, and midway between these two points) will be monitored for TSS three times per week. Samples will be processed by the laboratory for a 7-day turnaround. Water column monitoring for dissolved metals, polychlorinated biphenyls (PCBs), DDT, and tributyltin (TBT) concurrent with the TSS samples will be conducted three times per week for the first 2 weeks of disposal operations, then weekly, thereafter, if no water quality exceedances are observed. Reference or upcurrent stations within Lower Newport Bay will also be sampled at similar depths and frequency for comparison. Figure H-5 depicts the conceptual locations for monitoring of the water column.

Water column monitoring at the dredging operations will be conducted at similar distances, depths and frequencies and be tested for the same chemical parameters. If no elevated chemicals are observed during the first 2 weeks of monitoring, sample frequency will be reduced to once per week.

7.1.2 *Construction Operations Monitoring*

Proposed monitoring procedures to meet the objectives related to cap design include the following:

- Recording tonnage/volume of sediment dredged and placed within the CAD facility
- Tracking location of sediment placement within the CAD facility
- Recording tonnage/volume of capping sediment dredged and placed within the CAD facility
- Completing progress bathymetric surveys to verify sediment placement location
- Tracking operational information such as dredge production rates, downtime, and barge discharge time

- Completing a bathymetric survey of the CAD facility after the interim cover containment layer and final cap have been placed over the CAD facility to ensure that the cap material has been placed evenly over the entire facility

7.2 Immediate Post-Construction Monitoring Description

Monitoring immediately after construction is completed is required to ensure that placement of the sediment is successful, which, in this case, is measured by achieving the desired minimum cap thickness over the entire CAD facility while minimizing the incidence of off-site transport of sediment outside of the CAD facility. These parameters will be measured using during- and post-construction bathymetry surveys and post-construction sediment coring of the cap layer. Each parameter is described in greater detail below.

7.2.1 *Bathymetric Surveys*

Bathymetric surveys will be conducted prior to initiation of disposal activities to establish the baseline conditions for the CAD facility and routinely during disposal operations to monitor successful placement of sediments into the CAD facility. A post-construction cap bathymetric survey is also required to quantify the final configuration and elevations of the capped site. This bathymetric survey will be conducted after the placement of the interim cover containment layer and after placement of the final cap. This information will help determine whether design criteria are met and provide a baseline for comparison to long-term bathymetric surveys of the CAD facility.

7.2.2 *Cap Coring*

Post-construction coring is required after the placement of the final clean sediment cap to provide information both on the physical characteristics of the final cap and the underlying sediment (i.e., final cap thickness, horizontal coverage, and extent of mixing between layers) and the chemical characteristics of the final cap once it has been placed. Core chemistry data will be collected to establish a baseline profile of chemicals in various layers of the final cap and in the underlying sediment. Final cap core chemistry information will also help to quantify the extent of mixing between the final cap and underlying sediment that occurred during placement.

This baseline chemistry profile will be compared to long-term monitoring core chemistry data to determine whether any chemicals are migrating from the underlying sediment into the final cap sediment. Because diffusion of chemicals through sediment is a time-dependent process, migration from underlying sediments will be observable first in the deepest layers of the final cap. If long-term monitoring reveals increases in chemicals only in surface layers of the final cap, it would be indicative of chemicals from sources outside the CAD facility being deposited on the final cap surface (rather than migration of chemicals from beneath the cap).

7.3 Long-Term Post-Construction Monitoring

Long-term monitoring after construction of the final clean sediment cap is completed is required to verify that the CAD facility has maintained its physical integrity and that the cap is maintaining its ability to sequester underlying contaminants. These parameters will be measured using periodic post-construction bathymetric surveys and sediment coring of the cap layer. Each parameter is described in greater detail below. The key elements addressed by the monitoring program included the following:

- Determining if the CAD facility cap has maintained its physical integrity
- Confirming that chemicals remain isolated below the cap surface

7.3.1 *Bathymetric Surveys*

Bathymetric surveys will be conducted 3, 6, and 12 months after completion of final cap construction to quantify the configuration and elevations of the capped site. Then, bathymetric surveys will be taken periodically and reported to the responsible state and federal regulatory agencies (CCC, RWCQB, USEPA, and USACE). If there is consensus among the regulatory agencies that the final cap is performing as predicted after 10 years of monitoring, the applicants may apply to the Executive Director of the CCC to narrow the focus or modify this aspect of the long-term monitoring program. This information will help determine whether design criteria continue to be met and quantify rates of erosion or deposition at the CAD facility.

7.3.2 *Cap Coring*

Twelve months after completion of final cap construction, sediment coring will be conducted to provide information on the physical characteristics of the final cap and underlying sediment (i.e., final cap thickness, horizontal coverage, and extent of mixing between layers) and the chemical characteristics of the final cap for comparison to baseline data collected immediately after final cap construction. Core chemistry data will be collected at a minimum of five locations distributed across the CAD facility to establish a profile of chemicals in various layers of the final cap and in the underlying sediment.

This chemistry data will be compared to the baseline chemistry data to determine whether any chemicals are migrating from the underlying sediment into the final cap sediment. Because diffusion of chemicals through sediment is a time-dependent process, migration from underlying sediments will be observable first in the deepest layers of the cap. As such, bulk chemistry and porewater samples will be taken within 1 foot of the interface between the underlying material and the final cap material to determine if there has been significant movement of contaminants. At least five samples will be taken 12 months after completion of the final cap and then every 5 years thereafter. A report will be submitted to the responsible state and federal regulatory agencies. If there is consensus among the regulatory agencies (CCC, RWCQB, USEPA, and USACE) that the final cap is performing as

predicted after the third round of samples, the applicants may apply to the Executive Director of the CCC to narrow the focus or modify this aspect of the long-term monitoring program. If long-term monitoring reveals increases in chemicals only in surface layers of the cap, it would be indicative of chemicals from sources outside the CAD facility being deposited on the final cap surface (rather than migration of chemicals from beneath the final cap).

7.3.3 Adaptive Management

After the first year of post-construction monitoring has been completed, an adaptive management plan will be developed based on an analysis of the data collected during the year. The long-term management plan will be developed based on the existing conditions of the site and current technological developments and will be designed to ensure long-term cap stability and isolation of contaminants. Monitoring requirements, such as timing of the events, will be determined at that time. At a minimum, however, long-term monitoring will include the following:

- Completing bathymetric surveys to rates of erosion and deposition
- Coring for chemistry in bulk sediments and porewater

The exact scope and frequency of the long-term monitoring program will be evaluated and developed after the first year of post-construction monitoring data are available and have been reviewed.

7.3.4 Environmental Monitoring Reports

The City will prepare and submit to the regulatory agencies an annual environmental monitoring report to document and discuss the results of all CAD facility monitoring activities conducted during the previous year. Sampling will be based on the calendar year, and reports will be completed by January 31 of the following year and will include a discussion of current and past monitoring data for the site, as well as proposed future monitoring planned for the site. Table H-1 includes a summary of the construction and post-construction monitoring requirements.

Table H-1
Summary of Construction and Post-Construction Monitoring

Matrix	Target Analytes	Frequency	Collection Technique
Surface Water – During Dredging (Outside Silt Curtain) and at Disposal Location	TSS, metals, PCBs, DDT, and TBT	Three times per week for first 2 weeks, then weekly if no elevated concentrations are observed	Grab samples
Bathymetry – During Disposal	—	As needed and at milestones during disposal of Main Channel 1, Main Channel 2, Turning Basin, and Newport Channel 1 sediments	Multi-beam sonar

Matrix	Target Analytes	Frequency	Collection Technique
Bathymetry – Immediate Post Construction	—	Immediately following construction (including both the layer of material unsuitable for open ocean disposal and the interim cover containment layer)	Multi-beam sonar
Bathymetry – During Disposal	—	As needed, and at milestones for sediments outside the Federal Channels (permissible and not permissible under the City's RGP 54 program)	Multi-beam sonar
Sediment Cores – Immediate Post Construction of the Final Cap	Metals, PCBs, DDT, and TBT	Immediately following construction of the final cap	Core samples
Bathymetry – Immediate Post Construction of the Final Cap	—	Immediately following construction of the final cap	Multi-beam sonar
Porewater – Long-Term Monitoring	Metals and PCBs	1 year post construction, then every 5 years	In situ sediment probes
Sediment Cores – Long-Term Monitoring	Metals, PCBs, DDT, and TBT	1 year post construction, then every 5 years	Core samples
Bathymetry Surveys – Long-Term Monitoring	—	3, 6, and 12 months post construction and then every 5 years	Multi-beam sonar

8 Contingency Plans

Environmental and maritime safety is of primary importance in the operation and management of the Lower Newport Bay CAD facility. This OMMP has been developed with these factors in mind. However, it is recognized that unforeseen events can occur. Sound plans of action are required to assure consistent and appropriate actions are taken to address such events.

8.1 Emergency Notification Procedures

The contractor's field safety plan shall include specific points of contact in the event of emergencies. During the pre-construction meeting, the contractor will be given 24-hour emergency numbers for the City, USACE, USEPA, USCG, and the Harbor Police Department.

8.2 Incidents and Unusual Occurrences

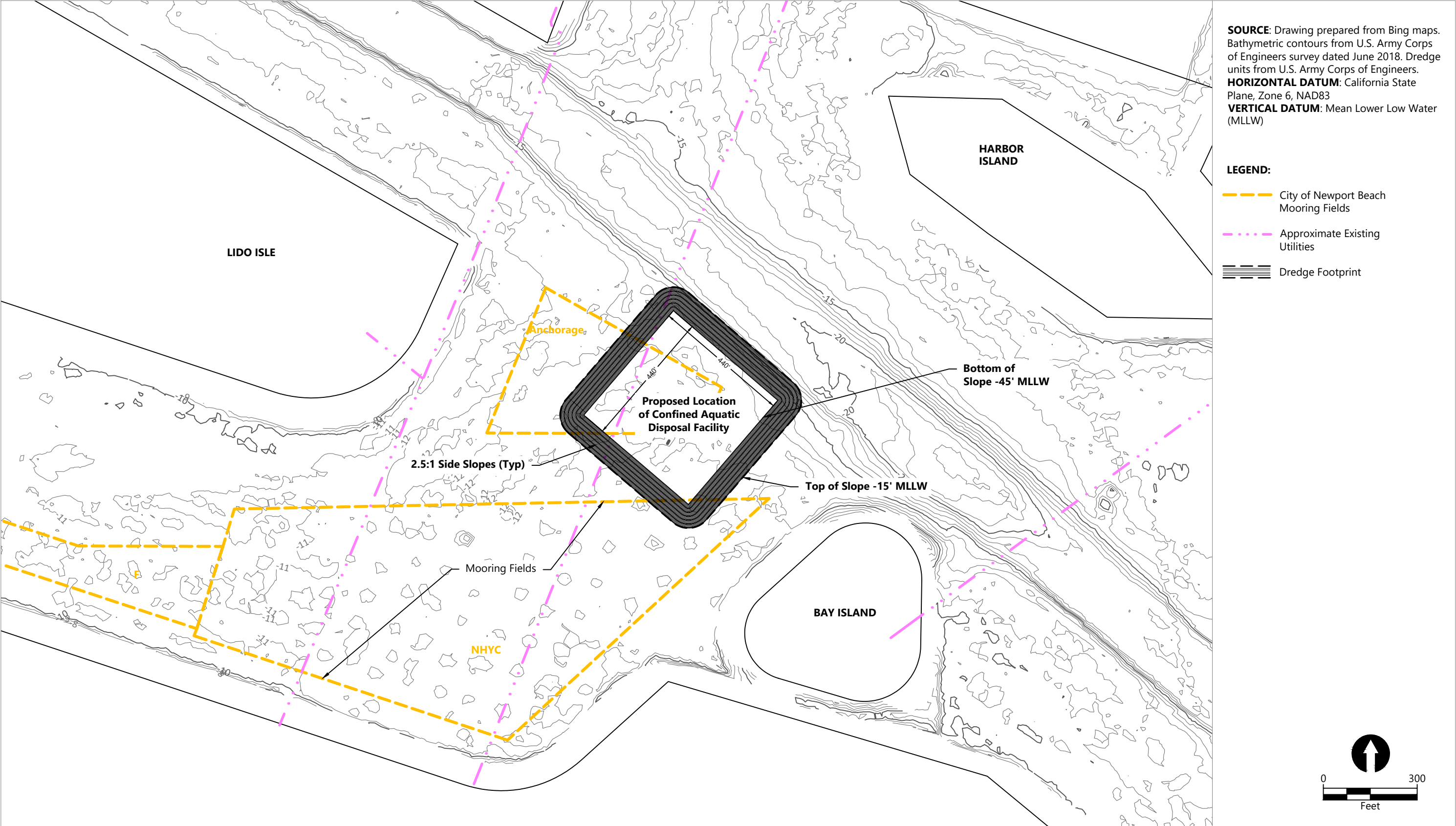
The City, which is responsible for the operation and management of the CAD facility, will work with the USACE and contractors to establish safe working conditions within and around the CAD facility. At the pre-construction meeting and in the agreements to be executed between the City and USACE addressing construction and operation of the CAD facility, it will be emphasized that the contractors, tugboat captain, and USACE-certified inspector are the first line of defense for assuring safety and compliance at the site. It will be emphasized that no activities should be started if the potential for problems appears possible and that any ongoing disposal activities should be ceased once the potential for problems arises. It is anticipated that most remedies will be precautionary (e.g., wait for better weather, repair dredging and disposal equipment, alter dredging and disposal equipment, alter dredging and disposal methods, coordinate conflicting activities among separate users of the Harbor).

If incidents or unusual occurrences do occur, the contractor will immediately cease the specific dredging and disposal activity and assess the situation. Remedies will be identified and provided to the City and, if necessary, the USACE and USCG for their concurrence. The contractor will be required to provide details on how the incident occurred and what immediate steps were taken to limit the extent of the impact. The contractor will be required to report on immediate actions and notifications made. The City will assess this information and evaluate the proposed remedy of the occurrence.

The engineer will perform environmental monitoring during all specified disposal activities. The results of this monitoring will be reported to the City and USACE. The City and USACE will evaluate these results and work together to determine whether operations are environmentally sound. The results of environmental monitoring may require operational methods to be modified to help meet the determined goals.

Any change in dredged material disposal techniques, methods, or equipment must receive prior approval from the City and USACE. Modifications to environmental permits may be required. If it becomes impractical to meet the criteria, considering the environmental and physical conditions within the site and equipment and methods available to the contractor, then engineering solutions may be considered and proposed. Modifications to the proposed actions and notifications described above will be made as lessons are learned in the operation and management of the site.

Figures

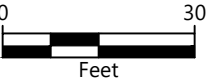
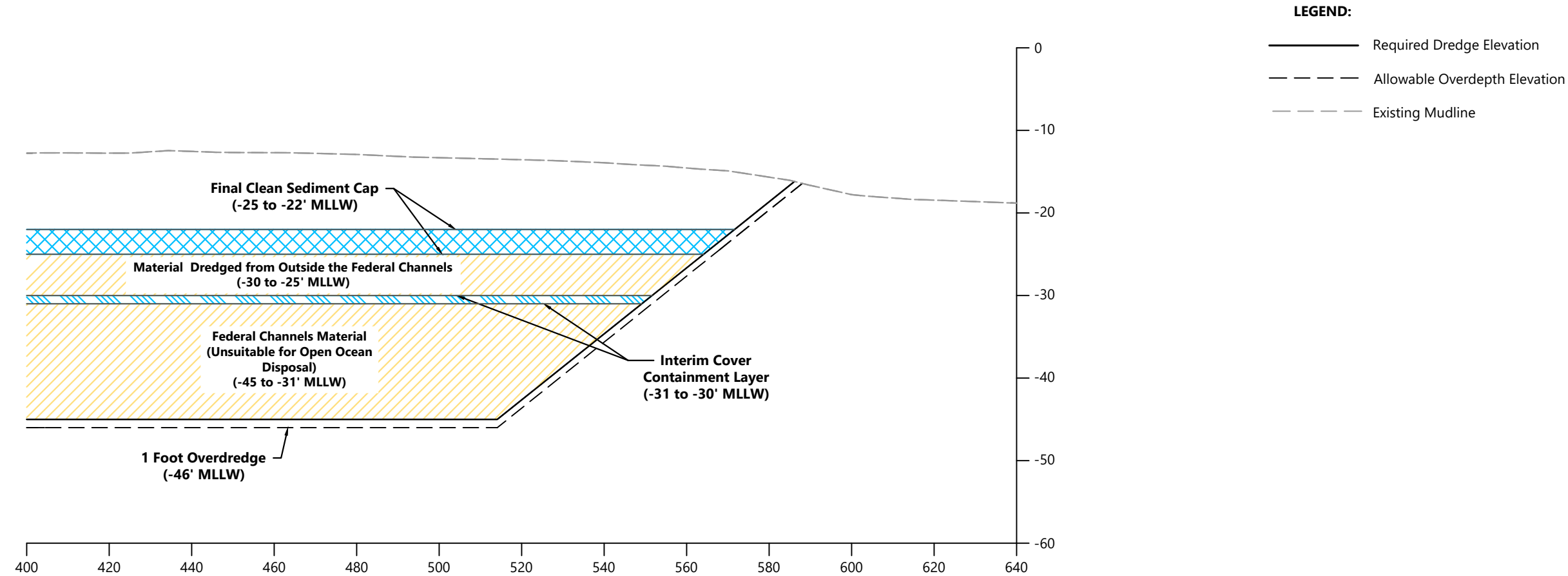


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Filepath: K:\Projects\0243-City of Newport Beach\Federal Channel\0243-RP-017 BODR BAY ISLAND CAD.dwg Figure H-1



Figure H-1
Plan View and Location of Proposed CAD Facility

SOURCE: Ariel from Bing Maps, 2018.
HORIZONTAL DATUM: California State Plane, Zone 6, North American Datum of 1983 (NAD83), U.S. Survey Feet
VERTICAL DATUM: Mean Lower Low Water (MLLW)





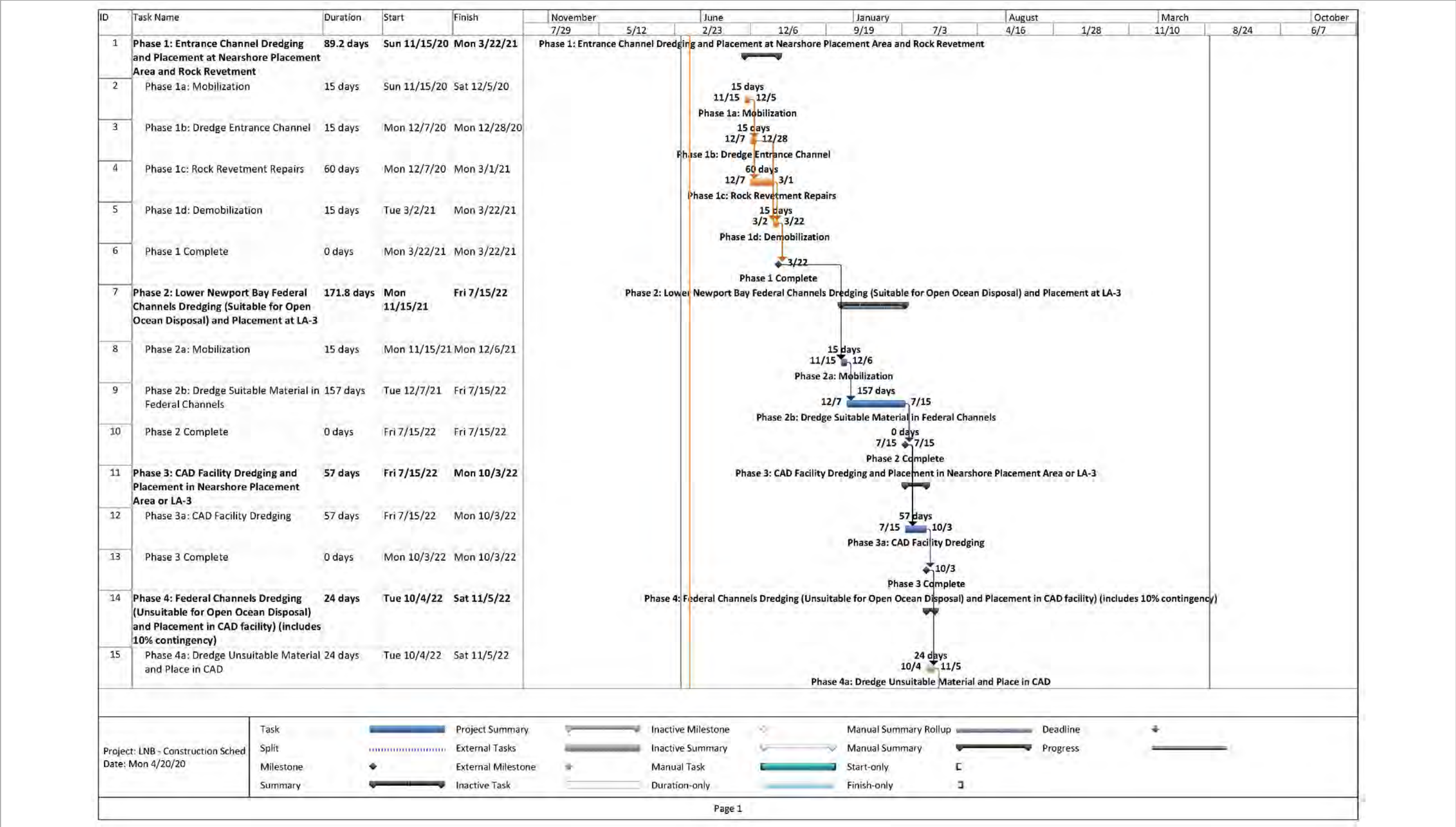
SOURCE: Drawing prepared from Bing maps. Bathymetric contours from U.S. Army Corps of Engineers survey dated June 2017. Dredge units from U.S. Army Corps of Engineers.
HORIZONTAL DATUM: California State Plane, Zone 6, NAD83
VERTICAL DATUM: Mean Lower Low Water (MLLW)

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Figure H-3
Federal Channels Maintenance Dredging Sediment Suitability Map

Appendix H Operations, Management, and Monitoring Plan
Draft Basis of Design Report Sediment Dredging and Confined Aquatic Disposal, Lower Newport Bay



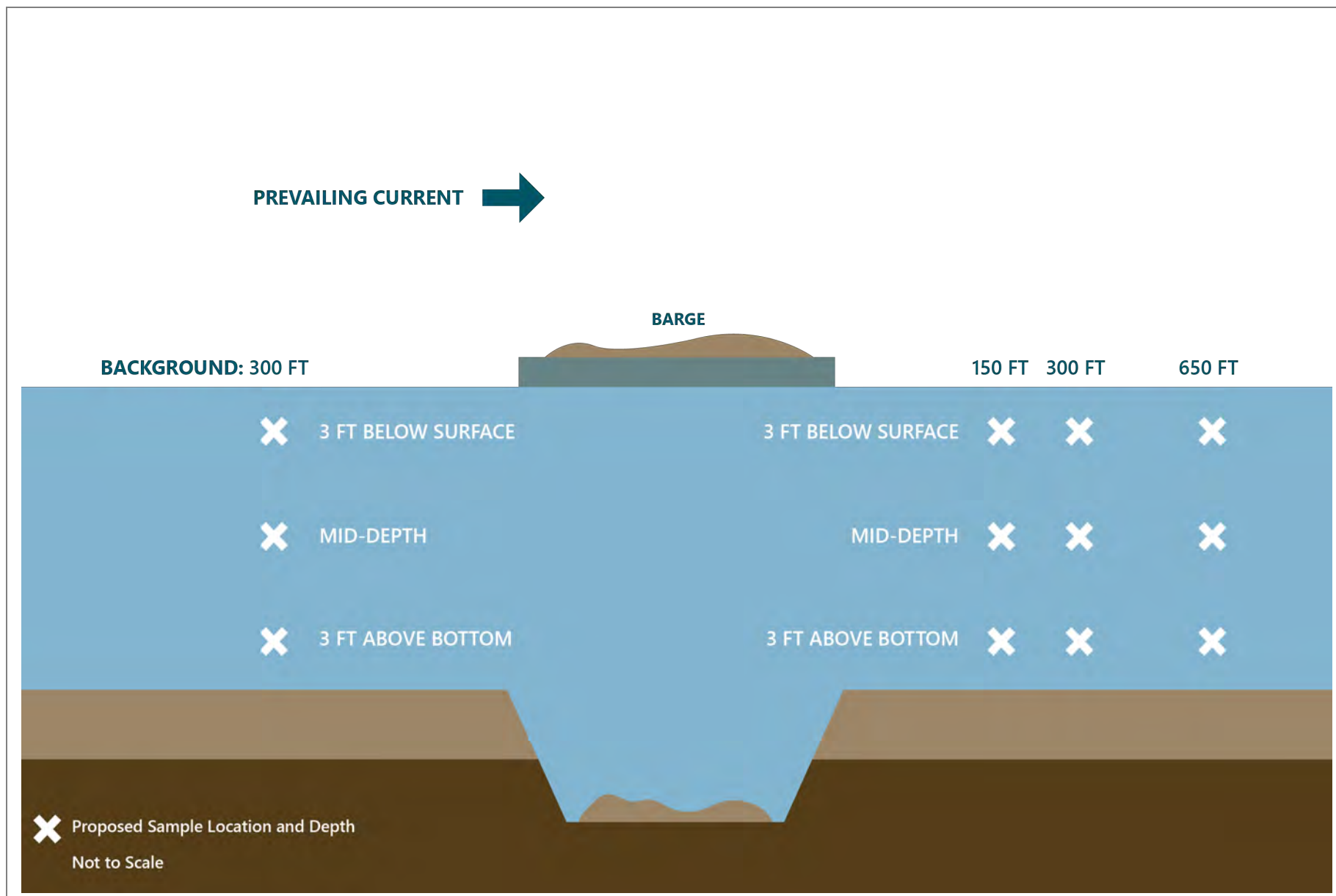


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Figure H-4
Construction Schedule

Appendix H Operations, Management, and Monitoring Plan
Draft Basis of Design Report Sediment Dredging and Confined Aquatic Disposal, Lower Newport Bay



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Figure H-5
Water Quality Monitoring Locations During Disposal

Appendix H Operations, Management, and Monitoring Plan
Draft Basis of Design Report Sediment Dredging and Confined Aquatic Disposal, Lower Newport Bay